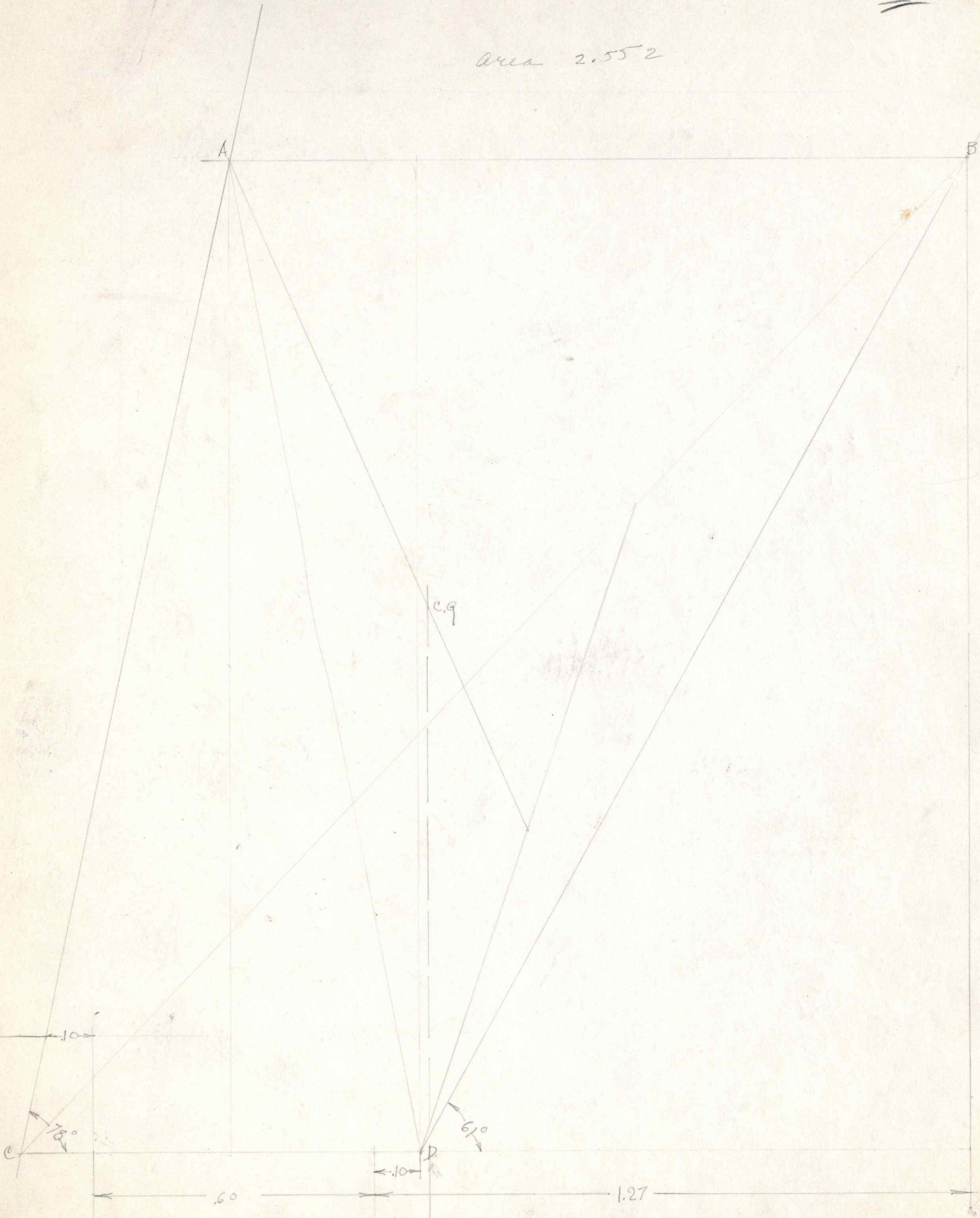
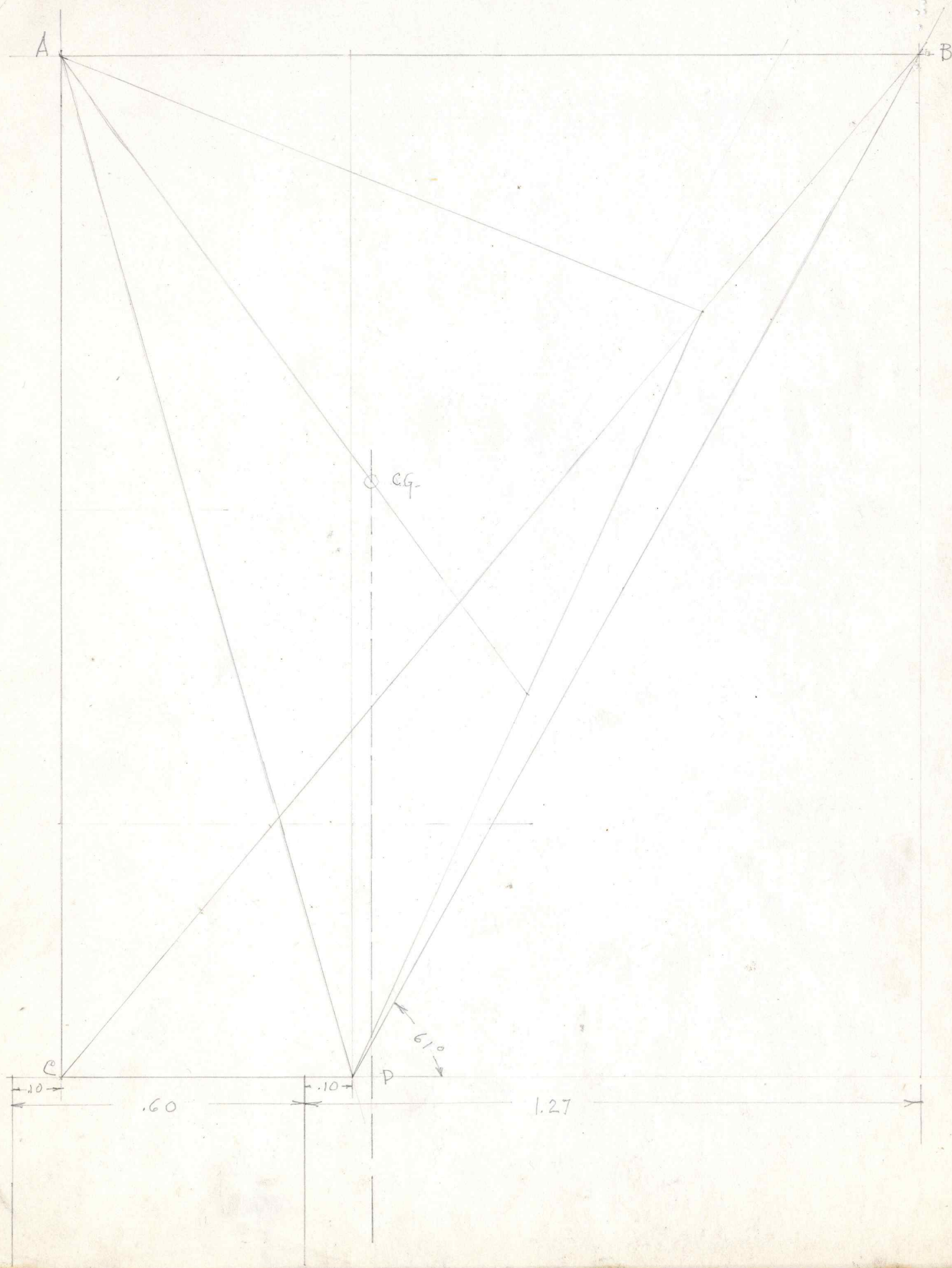


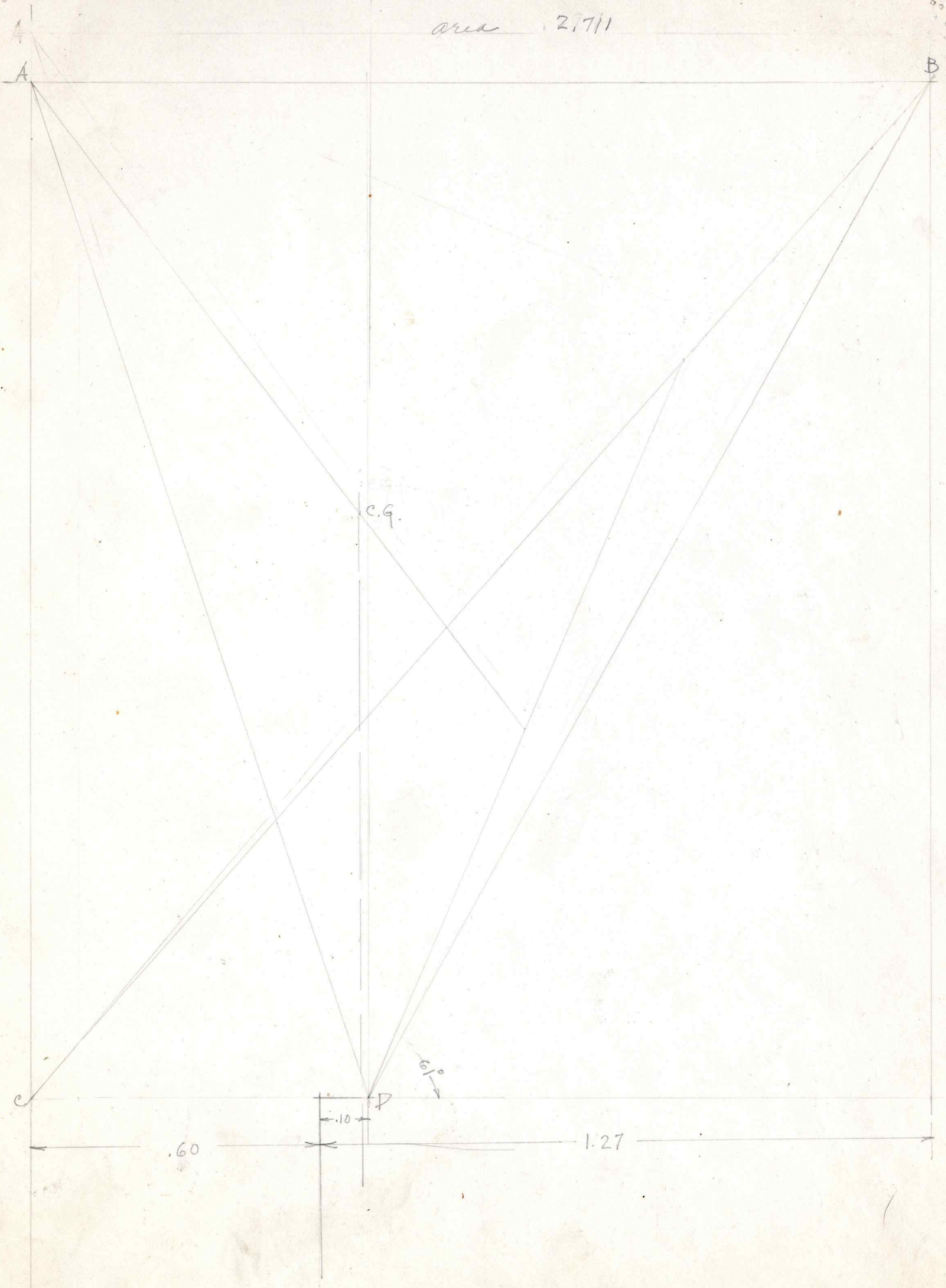
area 2.552



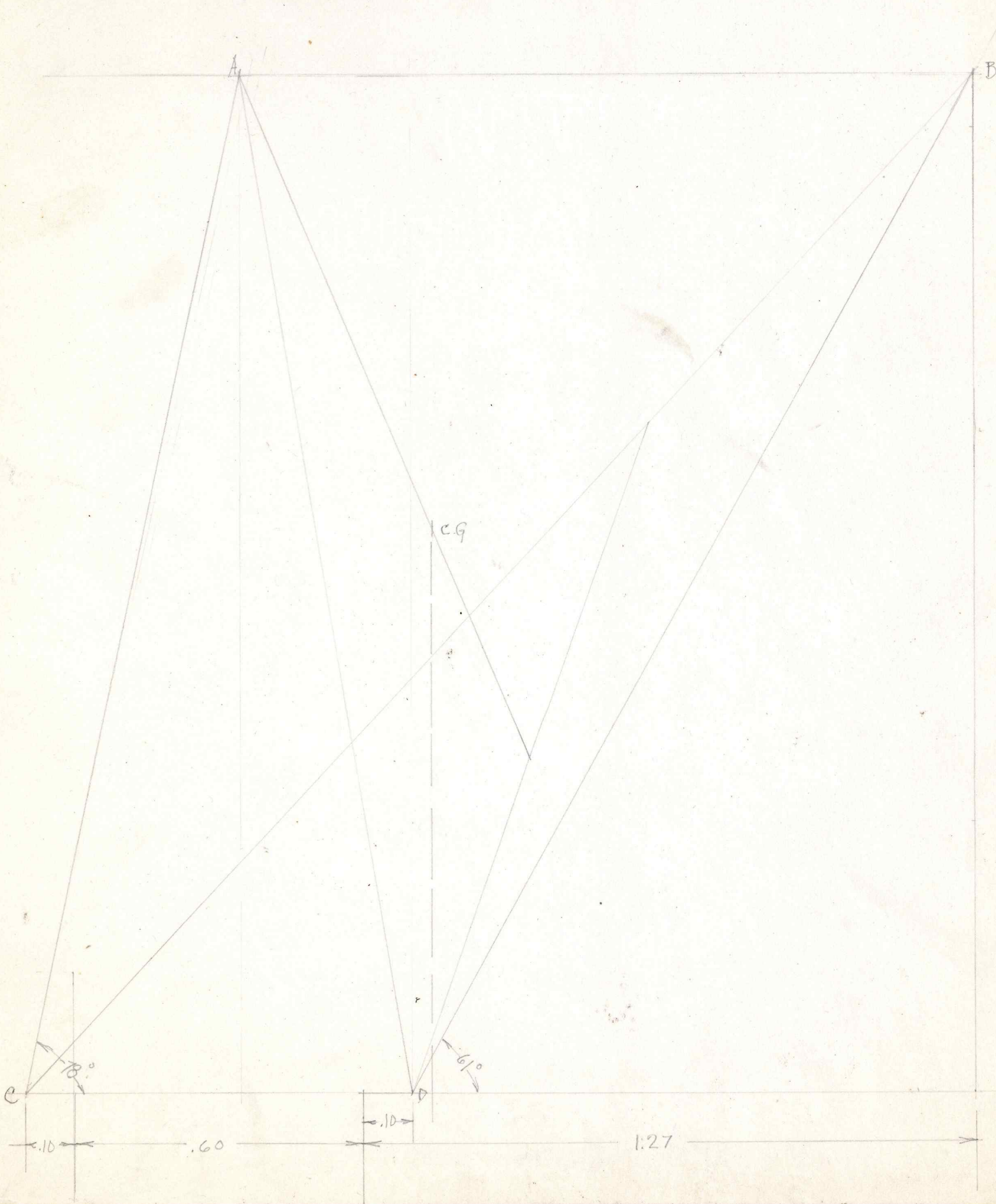
2.429 = area



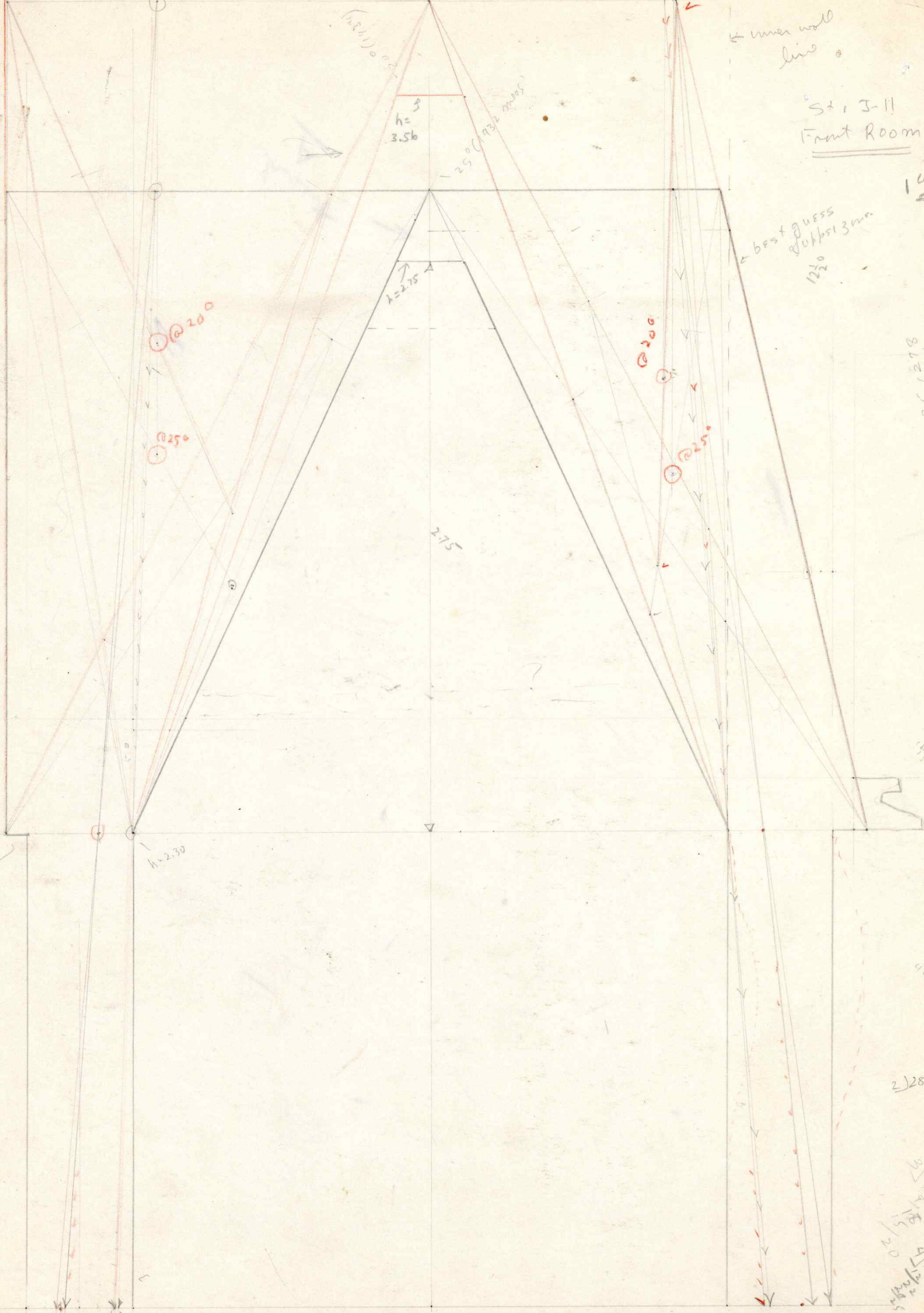
area 2.711



2.446 = area







inner wall line

St. J-11  
Front Room

1434

best guess  
of h=1.3m  
1220

3) 8.35 (2.78)  
2.78  
2.78/2.78

2.78  
2.78  
2.78/2.78

2.78  
2.78  
2.78/2.78

2) 288 (144)  
144  
288/144

1.08  
1.08  
1.08/1.08

4.14 (3)  
3  
4.14/3

1.15  
1.15  
1.15/1.15

1.72  
2.78  
1.72/2.78

1.72  
2.78  
1.72/2.78

2.78 (2.9)  
2.9  
2.78/2.9

1.44

2.00  
2.00

(h=3.56)

h=3.56

2.50 (932 mm)

l=2.75

2.75

200

250

200

250

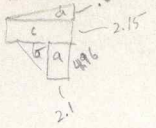
h=2.30

l=1.01

200

2.00  
2.00

Weight of 1/2 mid vault:



a	4.96	c	5.4	d	5.4
b	2.1		2.15		1.62
	4.96		270		54
	992		105		116.10
a	10.416				
b	7.066				
c	11.610				
d	1.62				
	36.712				
	x 2				
	61.424				

J-29 - coming 1931 & 1934 data  
 1934 Reconstruction  
 Rear (light) room

Load on 2 walls:

Outer: 4.14 | 27.60 | 6.66 per unit.

Medial: 4.2 | 61.424 | 14.62

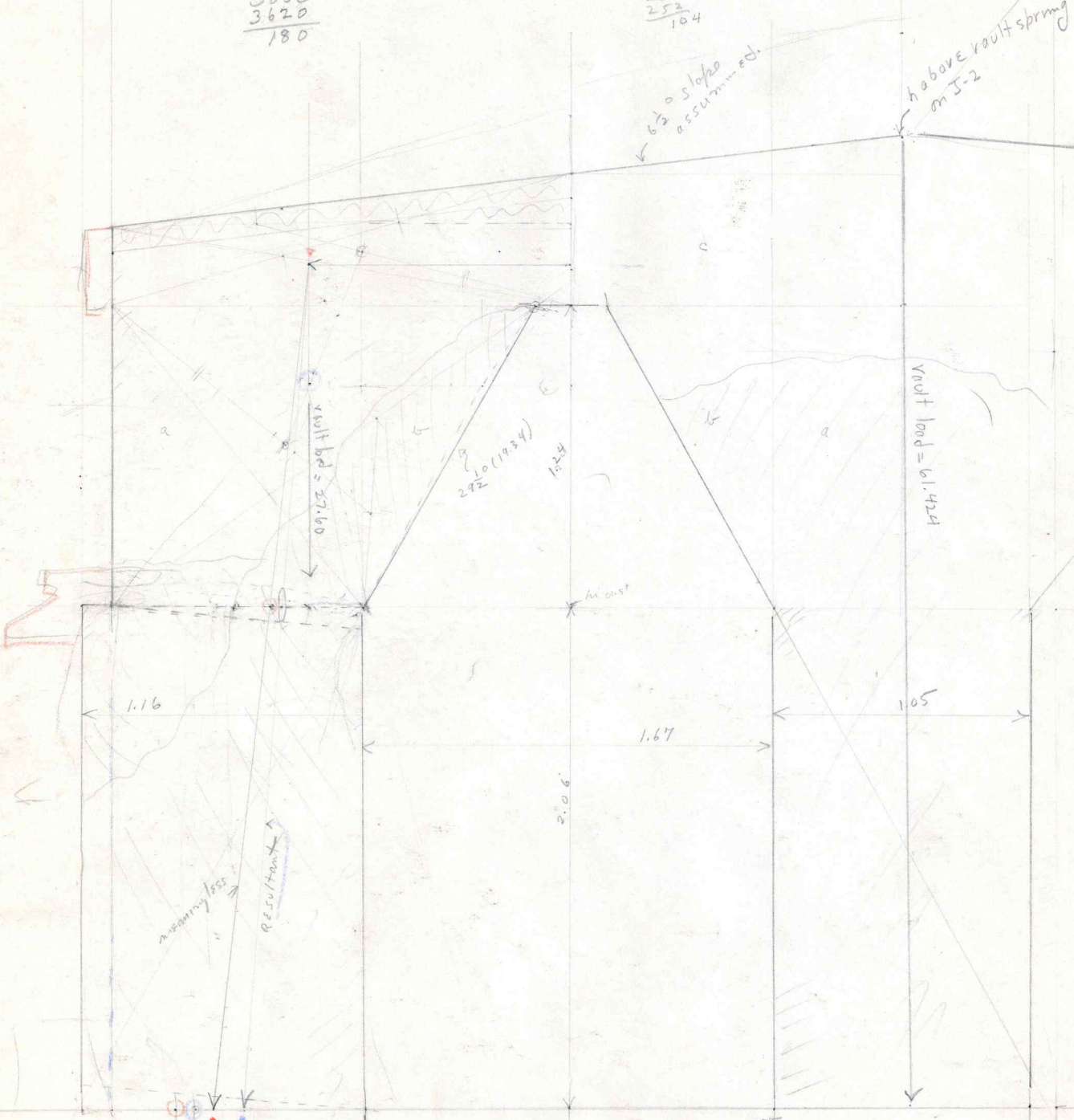
14.62 | 6.66 | 1.458  
 5848  
 8120  
 731.0

1.98  
 4  
 7.76

$Vh = \frac{1.24}{496}$

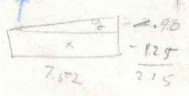
Resultant is: 2.15 in above.

4.54 | 2.650 | 1.58.9a.  
 2270  
 3800  
 3620  
 180



3 | 47 | 235

W on W Roof:



x 7.52 y = 7.52  
 1.25 - .90  
 3760  
 1504  
 752  
 24000  
 3.384  
 12.784

Vault: a 4.96 b 4.96  
 4.14 2.85  
 1984 2450  
 496 3968  
 1984 992  
 205344 7.0665  
 7.0665 2 | 41330

Roof W =

3 | 615 | 205 | 545 | 181

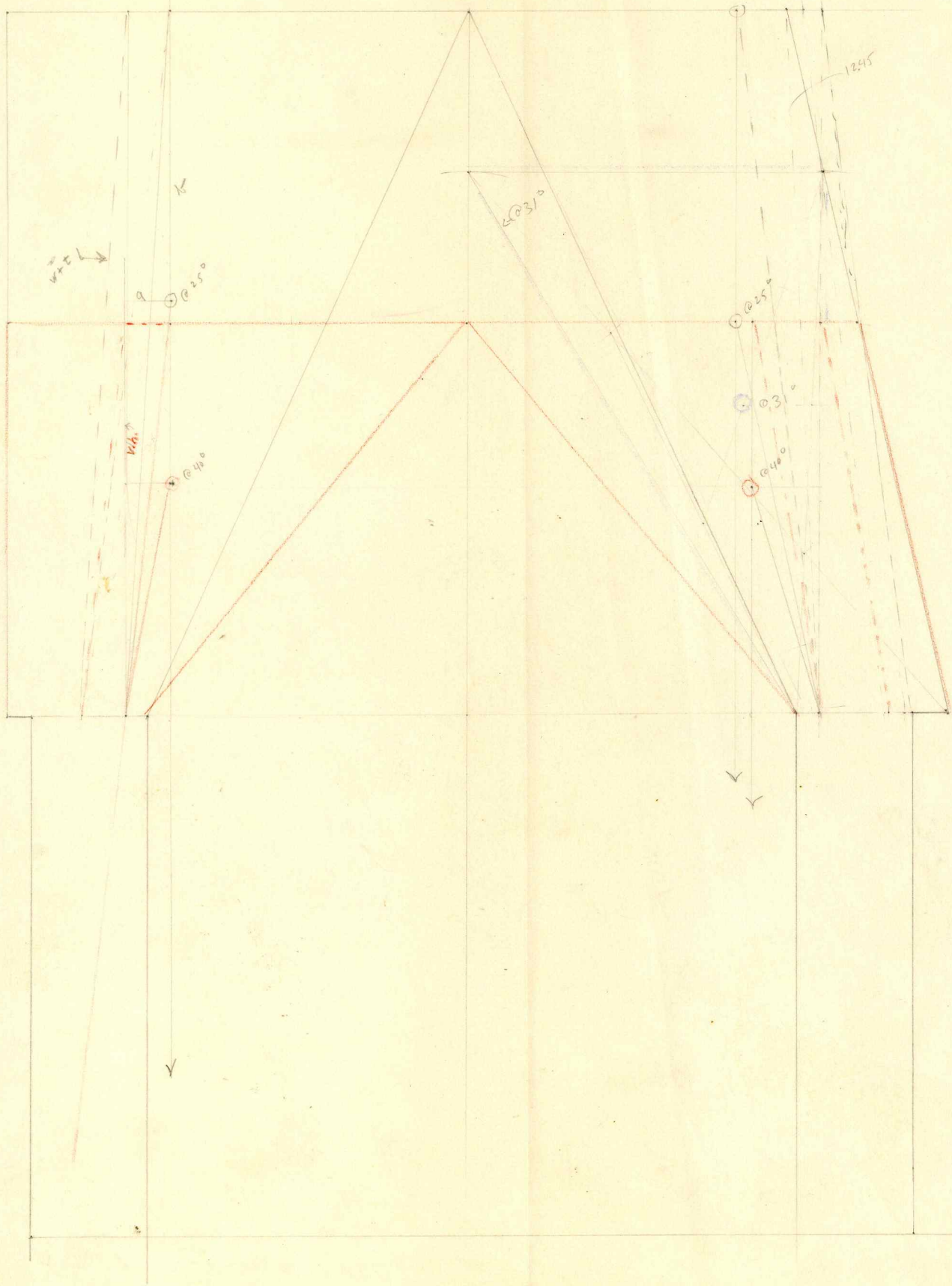
$VW = 27.6009$

3 | 535 | 170  
 2.06  
 4  
 824

3 | 1.11 | 1387  
 326  
 24  
 20  
 3866  
 15464

Moment

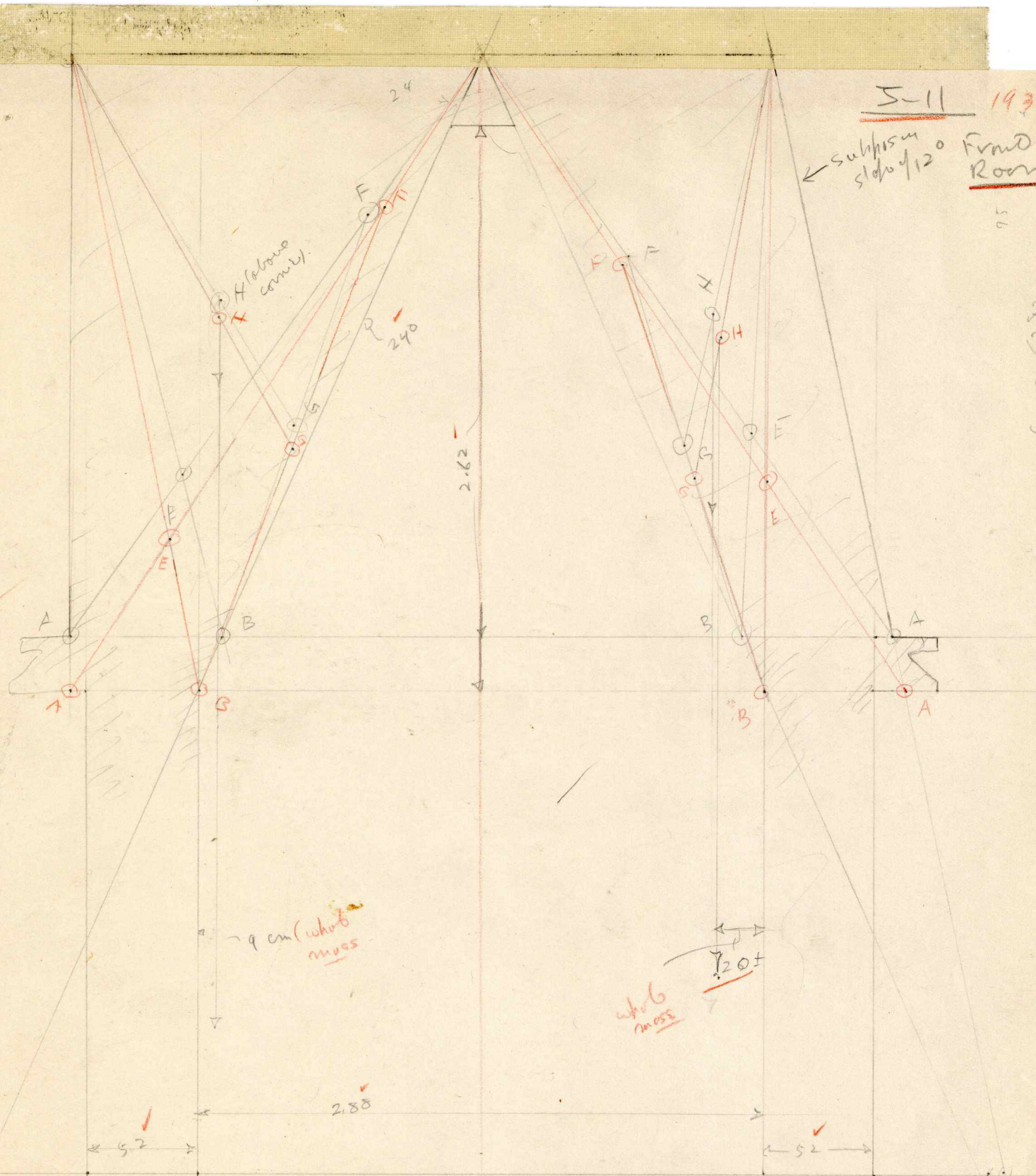
5-11 Front Row



3658 211

S-11 1933

Subsidiary slope of 12° from Room



Parabola rear vault section applied to narrow front wall.

Hypothetic 12° slope applied to front wall.

$$\begin{array}{r} 3 \overline{) 81} \quad (27) \\ \underline{6} \\ 21 \end{array}$$

wall h = 2.88 ±

$$\begin{array}{r} 2.88 \\ \times 3 \\ \hline 8.64 \\ 9.20 \end{array}$$

8.4

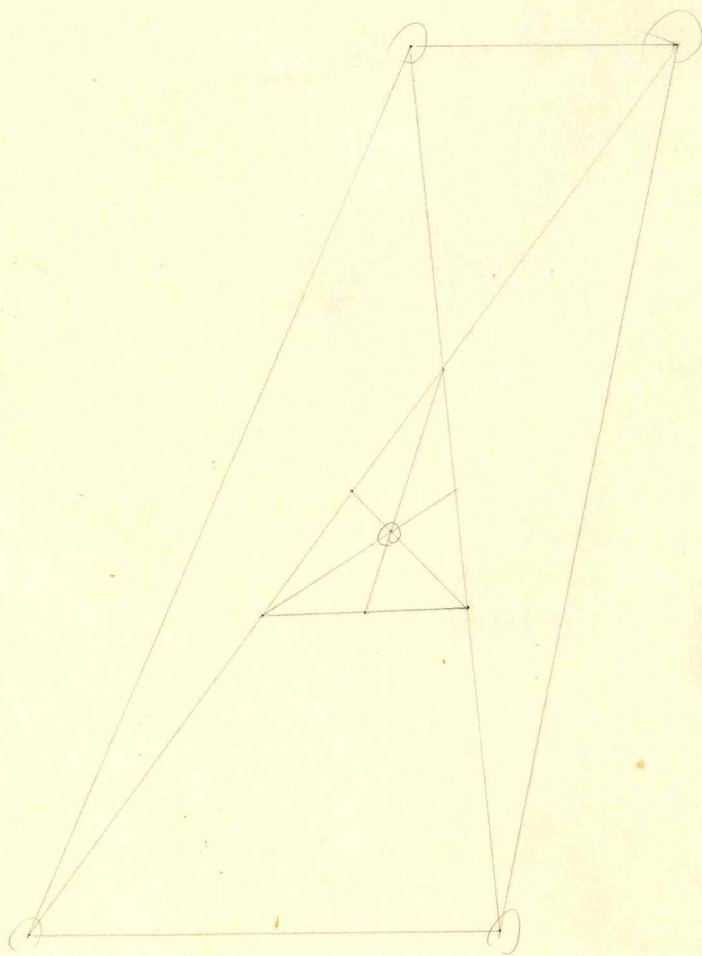
$$\begin{array}{r} 29 \quad (22) \\ \times 3 \\ \hline 87 \\ 87 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 3 \overline{) 845} \quad (281) \\ \underline{6} \\ 245 \\ \underline{24} \\ 25 \end{array}$$

$$\begin{array}{r} 2.62 \\ \times 4 \\ \hline 10.48 \end{array}$$

$$\begin{array}{r} 2.88 \\ \times 4 \\ \hline 11.52 \\ 3.7 \\ \times 5 \\ \hline 18.5 \\ 5.2 \\ \times 4 \\ \hline 20.8 \\ 2.62 \\ \times 5 \\ \hline 13.10 \\ 2.62 \end{array}$$

4.105 (2.82)

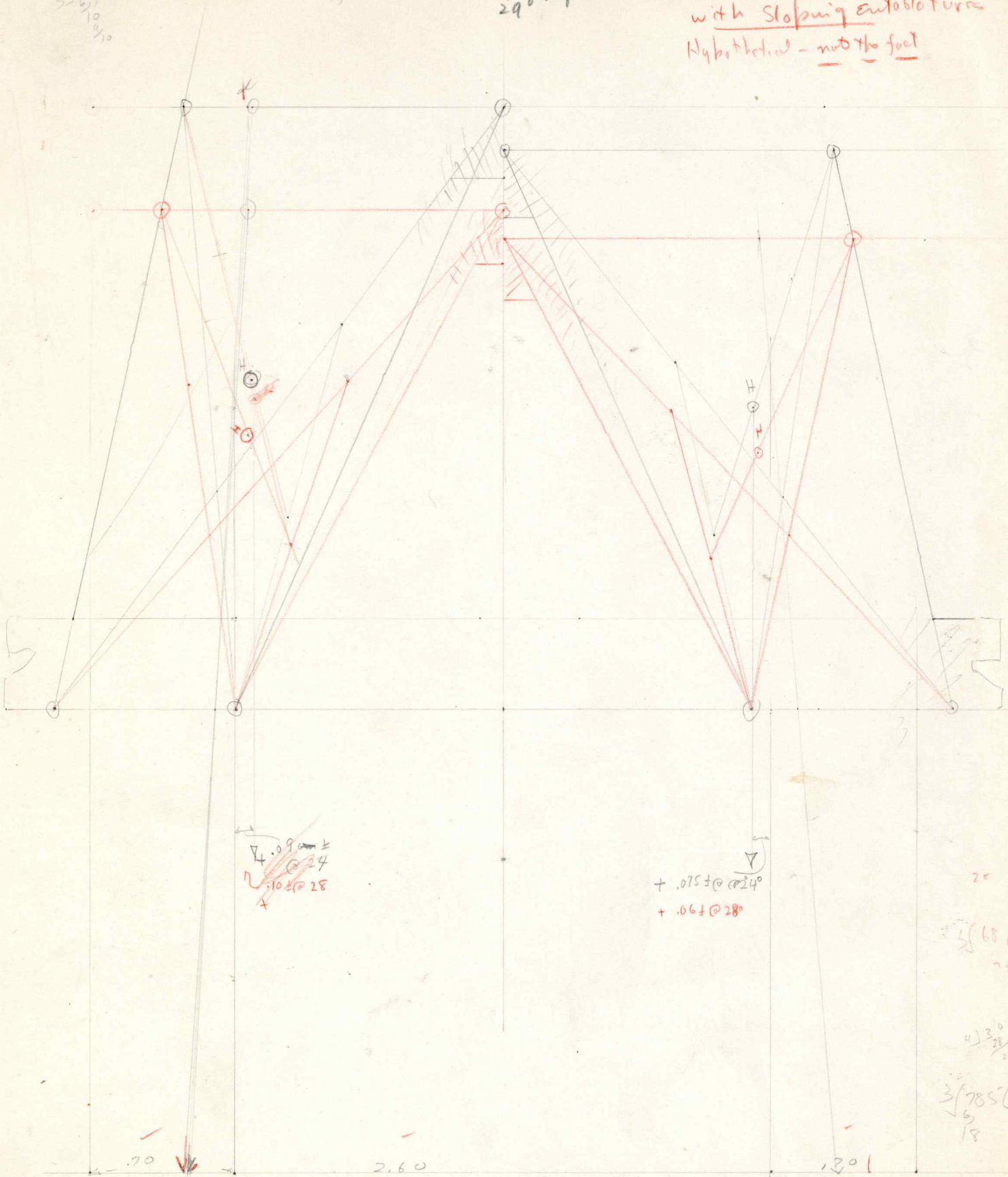


3/7  
3/10  
3/10  
3/10

3/25  
22  
21/15

24°  
29° slope

5-11-Real Room  
- Vault Reconstructed  
with Sloping entablature  
Hypothetical - not the fact



3/755  
3/15

3/875  
22

3/68  
22

4/30  
28

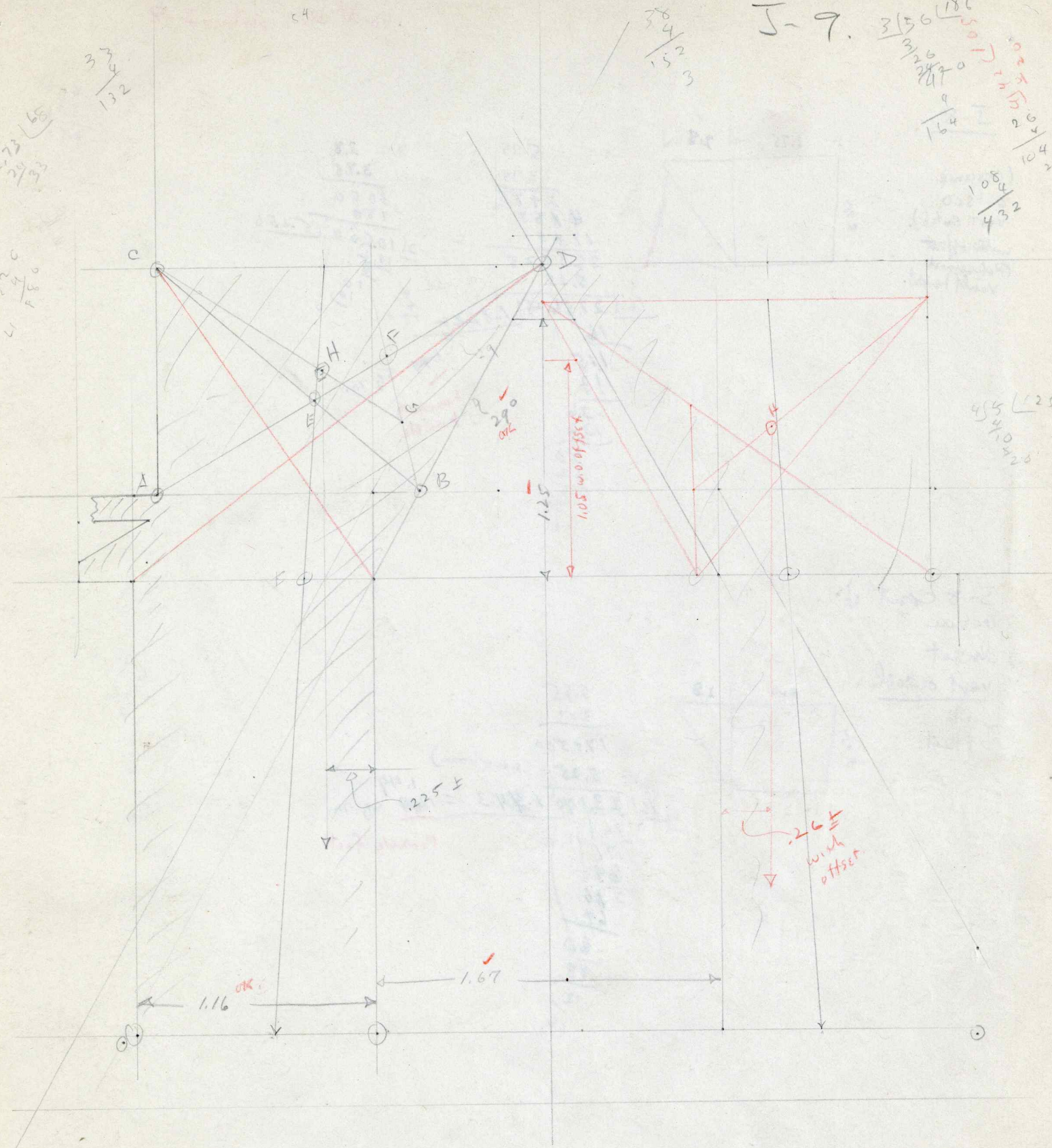
3/785  
18

J-9.  $\frac{3156}{164} = 19.2439$   
 $\frac{108}{432} = 0.25$   
 $\frac{102}{104} = 0.9712$   
 $\frac{102}{104} = 0.9712$

$\frac{22}{93} = 0.2365$   
 $\frac{33}{132} = 0.25$

$\frac{22}{93} = 0.2365$   
 $\frac{22}{93} = 0.2365$

$\frac{45}{104} = 0.4288$   
 $\frac{45}{104} = 0.4288$



Probable true section of rear room (using slope of 29° from front room).  
 no offset (occurs at other points).

$\frac{1.67}{2} = 0.835$   
 $\frac{668}{2} = 334$

$\frac{1.16}{4} = 0.29$   
 $\frac{4.62}{4} = 1.155$

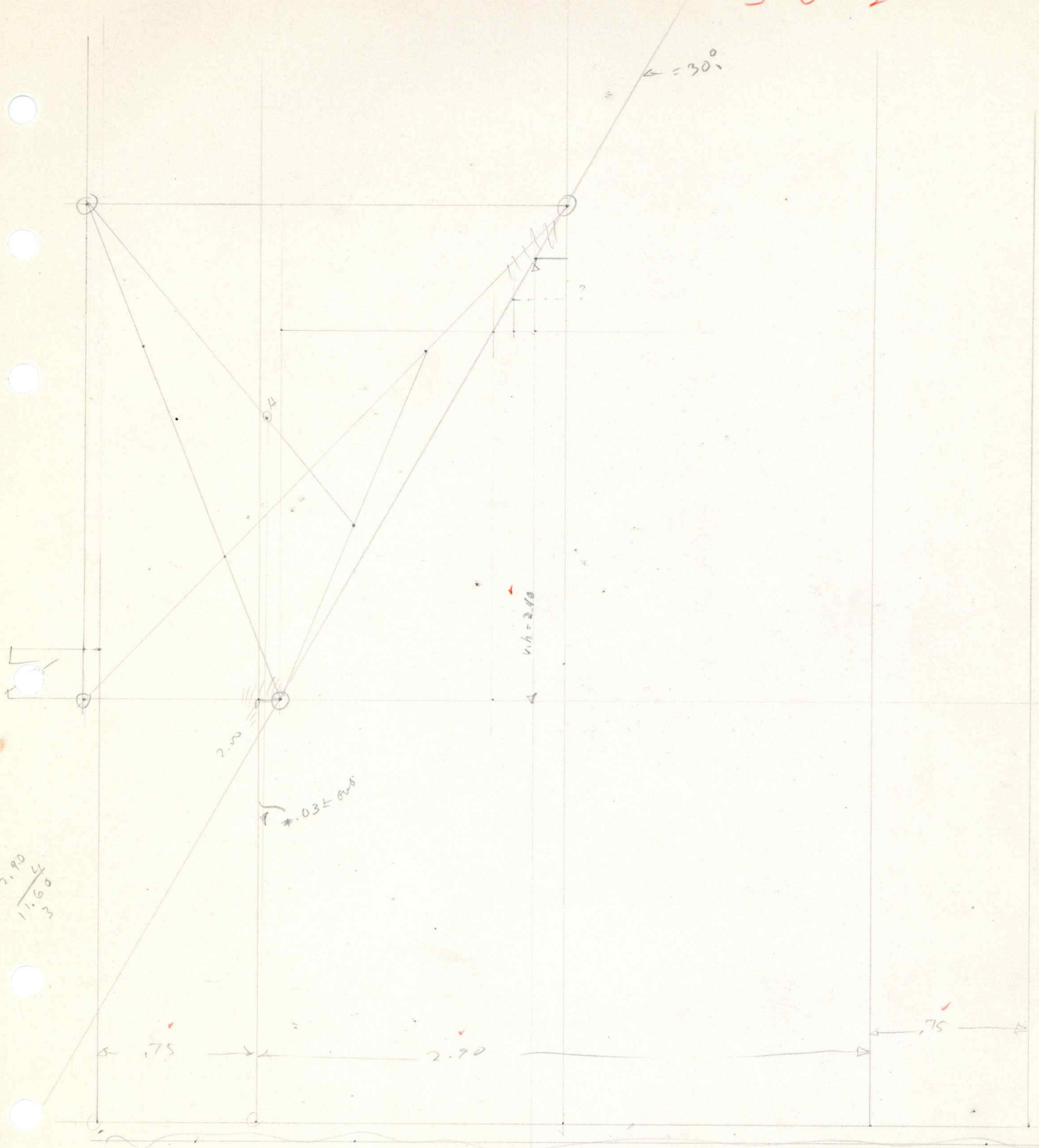
$\frac{105}{25} = 4.2$   
 $\frac{105}{25} = 4.2$

$\frac{419}{104} = 4.0288$   
 $\frac{419}{104} = 4.0288$

$\frac{105}{25} = 4.2$   
 $\frac{105}{25} = 4.2$



5-6-21



$$\frac{2.10}{1.60} = 1.3125$$

$$\frac{2.10}{1.470} = 1.435$$

$$\frac{3(29)(26)}{18} = 416.67$$

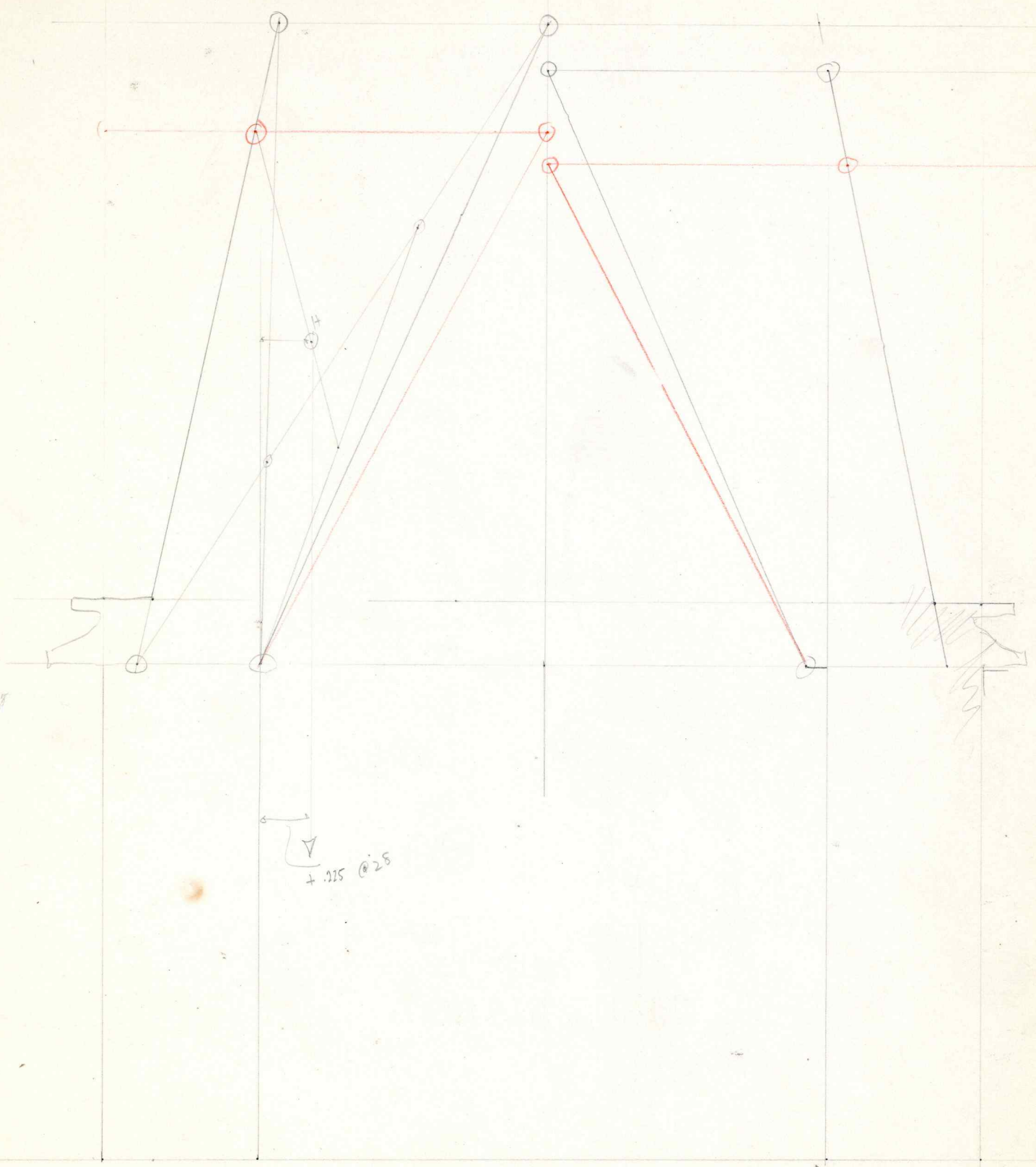
$$\frac{1.63}{.32} = 5.09$$

$$\frac{21}{8.4} = 2.5$$

$$\frac{2(115)(3.5)}{18} = 44.44$$



Hypothetical  
 vauld Reconst. of I-11  
 using I-2 upper zone.



4/9 (22)  
 5  
 .10  
 200

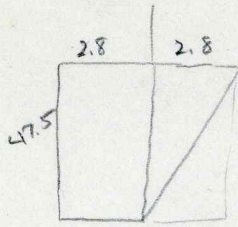
2/85 (42)

150

$$\frac{5.6}{2.8} \\ \frac{2.8}{2.8}$$

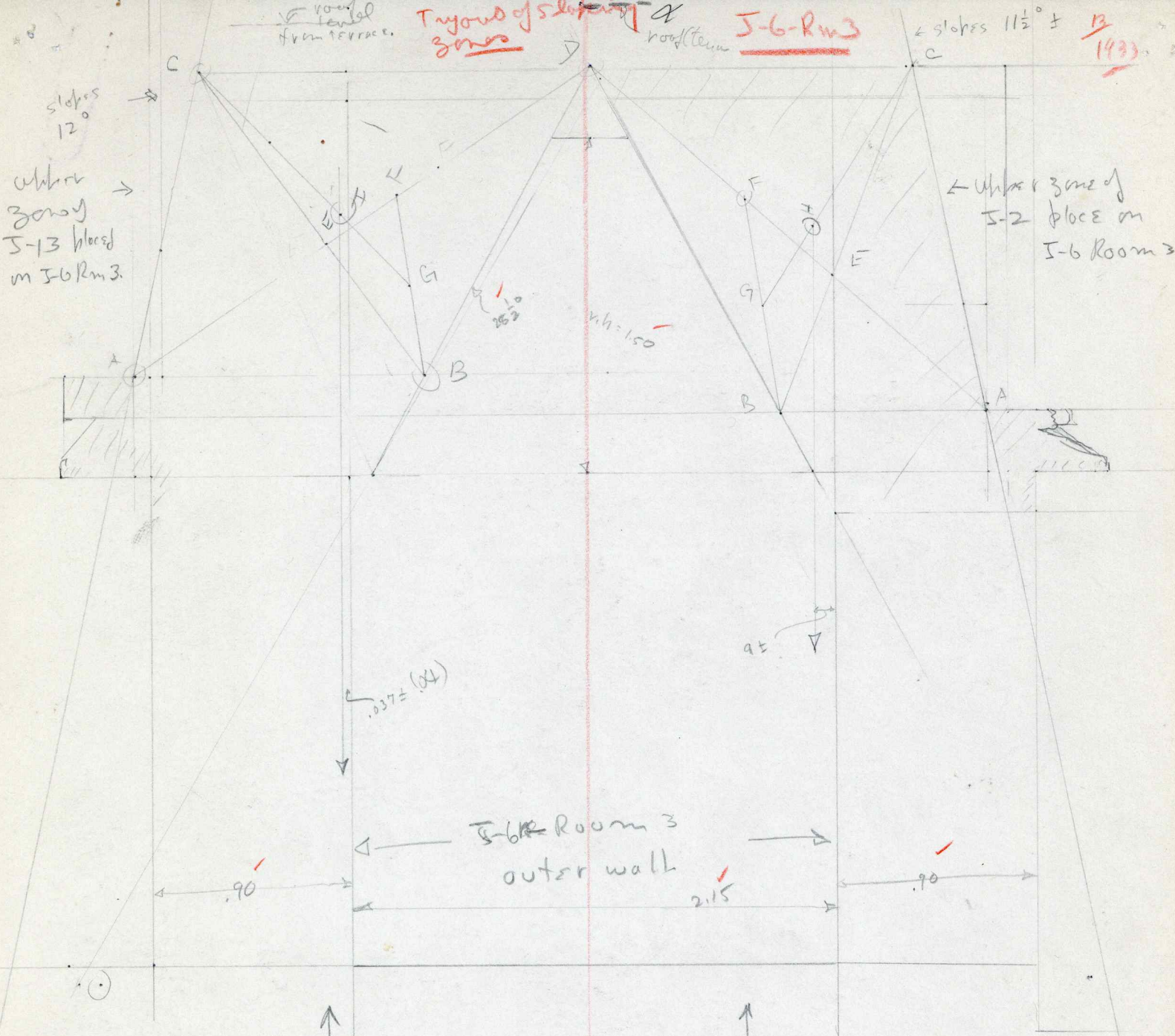
Room 6 of J-2

offset,  
height observed.  
slope 31°.  
(and see vert.  
other zone - close  
to stress point).



$\begin{array}{r} 2.8 \\ \hline 4.75 \\ 3800 \\ \hline 750 \\ \hline 13300 \\ \hline 6.650 \end{array}$	$\begin{array}{r} 2.8 \\ \hline 4.75 \\ \hline 2 \overline{) 13.30} \quad \underline{6.65} \\ 13 \\ \hline 13 \\ \hline 13 \\ \hline 16 \end{array}$
$\begin{array}{r} 16 \overline{) 199.50} \\ \underline{16} \\ 39 \\ \underline{32} \\ 75 \\ \underline{64} \\ 110 \\ \underline{96} \\ 14 \\ \hline 16 \end{array}$	$\begin{array}{r} 1.246 \\ \hline \approx 1.2558 \text{ meters.} \end{array}$

2.8  
4



The upper zone section (outside) of I-13 could have been applied to I-6-Rm 3 without net thrust on the walls.

The upper zone of I-2 (outside section) could have been applied to I-6-Rm 3 with very slight thrust on outer walls.

Handwritten calculations and notes:

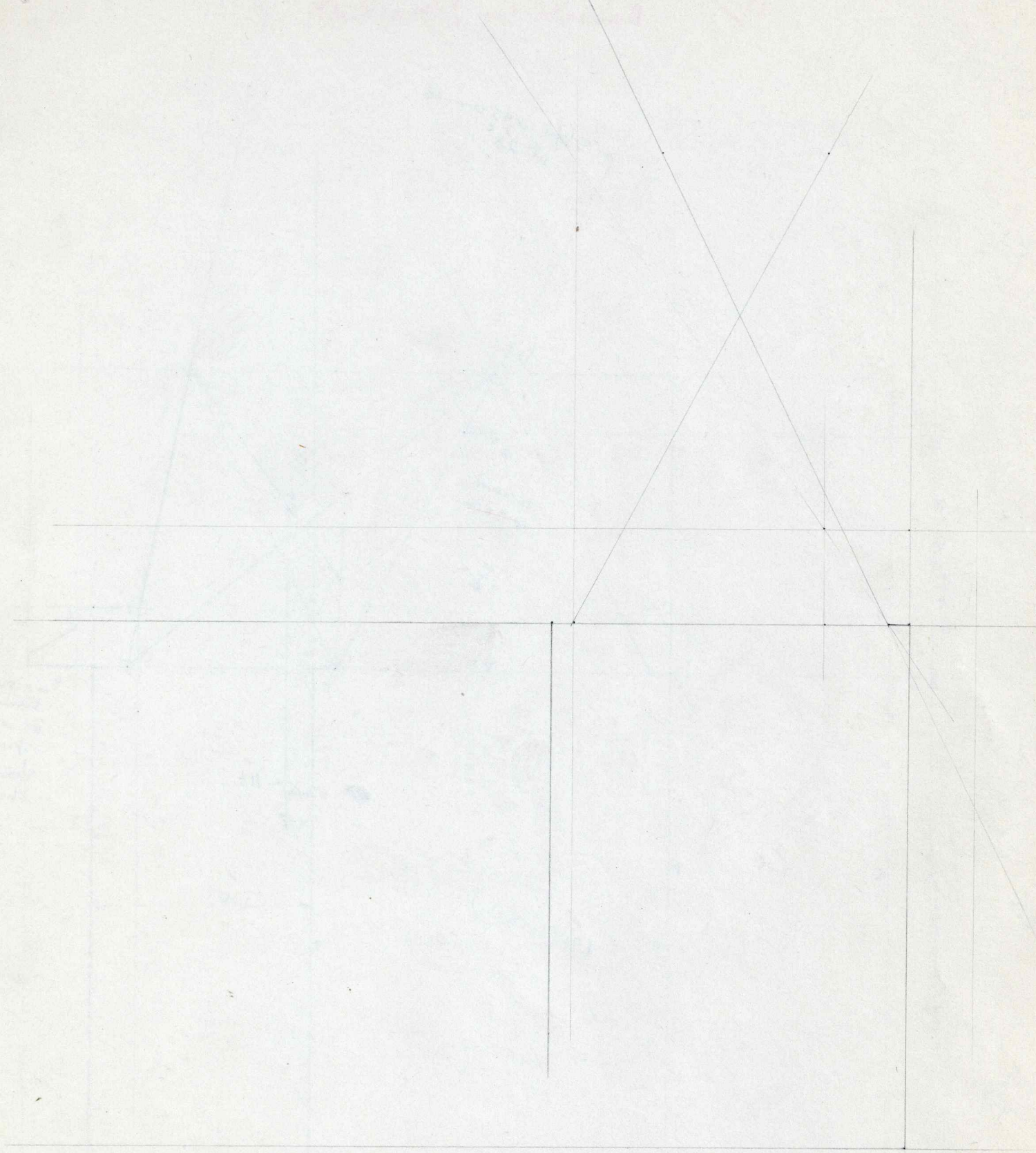
- $2.15 \times 8.00 = 17.2$
- $2.15 + 1.12 + 2.00 = 4.28$
- $4.28 \times 4 = 17.12$
- $4 \overline{) 235} \begin{matrix} 58 \\ 20 \\ 35 \\ 32 \end{matrix}$
- $4 \overline{) 15} \begin{matrix} 3 \\ 12 \end{matrix}$
- $4 \overline{) 35} \begin{matrix} 8 \\ 40 \end{matrix}$
- $4 \overline{) 665} \begin{matrix} 166 \\ 40 \end{matrix}$
- $4 \overline{) 95} \begin{matrix} 23 \\ 71 \\ 5 \end{matrix}$
- $4 \overline{) 595} \begin{matrix} 148 \\ 19 \\ 20 \end{matrix}$
- $5 \overline{) 176} \begin{matrix} 35 \\ 23 \\ 20 \\ 26 \\ 42 \\ 12 \end{matrix}$
- $5 \overline{) 36} \begin{matrix} 7 \\ 18 \end{matrix}$
- $5 \overline{) 38} \begin{matrix} 7 \\ 4 \\ 15 \end{matrix}$
- $5 \overline{) 42} \begin{matrix} 8 \\ 20 \end{matrix}$
- $5 \overline{) 21} \begin{matrix} 4 \\ 11 \end{matrix}$
- $10 \overline{) 26} \begin{matrix} 2 \\ 11 \end{matrix}$
- $10 \overline{) 28} \begin{matrix} 2 \\ 18 \end{matrix}$
- $10 \overline{) 112} \begin{matrix} 11 \\ 2 \end{matrix}$
- $10 \overline{) 117} \begin{matrix} 11 \\ 7 \end{matrix}$



S11-5-2

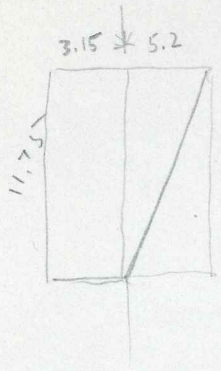
← 260

170  
5/8



Vault weights - J-11  
Rest Room.

J-11 -  
 maxm, as  
 measured  
 (24°, no offset).

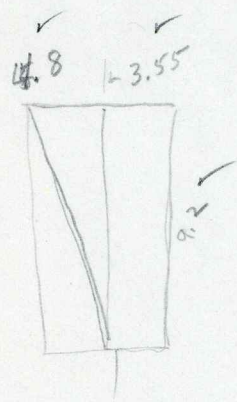


3.15	5.2
11.75	11.75
5875	2350
1175	5875
3425	2   61.100   39550
360125	5
30.55	11
	10
	0

16   66.5625   4.1601	meters - max
64	acc to measurements.
25	
16	
76	
96	
25	

J-11 -  
 minm



4.8	3.55
9.2	9.2
96	710
432	3195
2   44.16   22.08	32660
	2208
	54740

16   54.244   3.39	<del>sq. m.</del>
48	
62	
48	
144	
144	

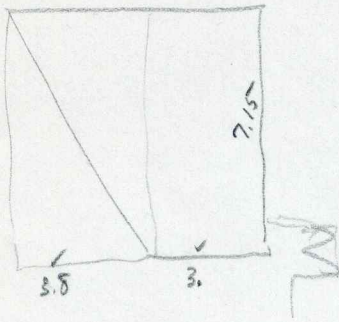
Minimum, with  
 offset,  
 @ 28°

16   54.74   3.42
48
67
64
34
32

J-6-Room 1.

Inset



$$\frac{3}{3.8} = \frac{1}{1.27}$$

$$\begin{array}{r} 7.15 \\ \underline{3.} \\ 21.450 \\ \underline{13.585} \\ 7.865 \end{array} \quad \begin{array}{r} 7.15 \\ \underline{3.8} \\ 5720 \\ \underline{2145} \\ 27170 \end{array} \quad \begin{array}{r} 13585 \\ \underline{2} \\ 27170 \end{array}$$

$$\begin{array}{r} 16 \overline{) 35.035} \\ \underline{32} \\ 30 \\ \underline{16} \\ 143 \\ \underline{128} \\ 155 \\ \underline{144} \\ 11 \end{array} \quad \begin{array}{r} 2.188 \\ \underline{2} \\ 2.19 \end{array}$$

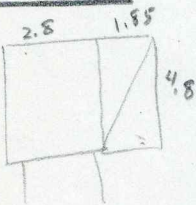
add offset.

$$\begin{array}{r} 7.15 \\ \underline{.7} \\ 5.005 \\ 3 \end{array}$$

$$\begin{array}{r} 35.035 \\ \underline{5.005} \\ 16 \overline{) 40.040} \\ \underline{32} \\ 80 \\ \underline{80} \\ 48 \\ \underline{32} \\ 16 \end{array} \quad \begin{array}{r} 2.502 \\ \underline{2.5} \\ 2.50 \end{array}$$

I-2-Room 6

a outset



$$\frac{4.65}{2.8} = \frac{1}{1.65}$$

$$\begin{array}{r} 4.8 \\ \underline{2.8} \\ 384 \\ \underline{96} \\ 1344 \\ \underline{444} \end{array}$$

$$\begin{array}{r} 4.8 \\ \underline{1.85} \\ 240 \\ \underline{384} \\ 48 \end{array} \quad \begin{array}{r} 8.880 \\ \underline{2} \\ 4.44 \end{array}$$

$$\begin{array}{r} 16 \overline{) 17.880} \\ \underline{16} \\ 18 \\ \underline{16} \\ 28 \\ \underline{16} \\ 120 \\ \underline{112} \\ 8 \end{array} \quad \begin{array}{r} 1.117 \\ \underline{1.1} \\ 1.12 \end{array} = 1.12 \text{ meters. (outset)}$$

± inset-subtract

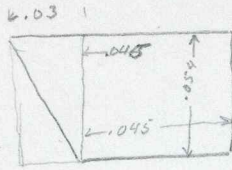
$$\begin{array}{r} 4.8 \\ \underline{.7} \\ 3.36 \end{array}$$

$$\begin{array}{r} 17.880 \\ \underline{3.36} \\ 16 \overline{) 14.520} \\ \underline{144} \\ 120 \\ \underline{112} \\ 8 \end{array} \quad \begin{array}{r} 1.107 \\ \underline{1.1} \\ 1.10 \end{array} = 1.10 \text{ meters.}$$



Vaults - Weight Calculations.  
Excluding mouldings - assuming offset.

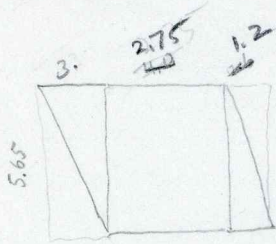
J-9 (trans Sinter.)  
 (inset).



$$\begin{array}{r}
 \text{cms} \\
 2.045 \\
 \times 2.045 \\
 \hline
 180 \\
 225 \\
 \hline
 2430 \text{ cms.} \\
 8.1
 \end{array}$$

$$\begin{array}{r}
 16 \overline{) 32.4} \quad 2.025 \text{ sq. meters.} \\
 \underline{32} \\
 40 \\
 \underline{32} \\
 80 \\
 \underline{80} \\
 0
 \end{array}$$

J-2



~~$$\begin{array}{r}
 4.1 \\
 5.65 \\
 \hline
 22.60 \\
 8.47 \\
 1.695 \\
 \hline
 14 \overline{) 32.765} \\
 \underline{32} \\
 76 \\
 \underline{64} \\
 125 \\
 \underline{112} \\
 13
 \end{array}$$~~

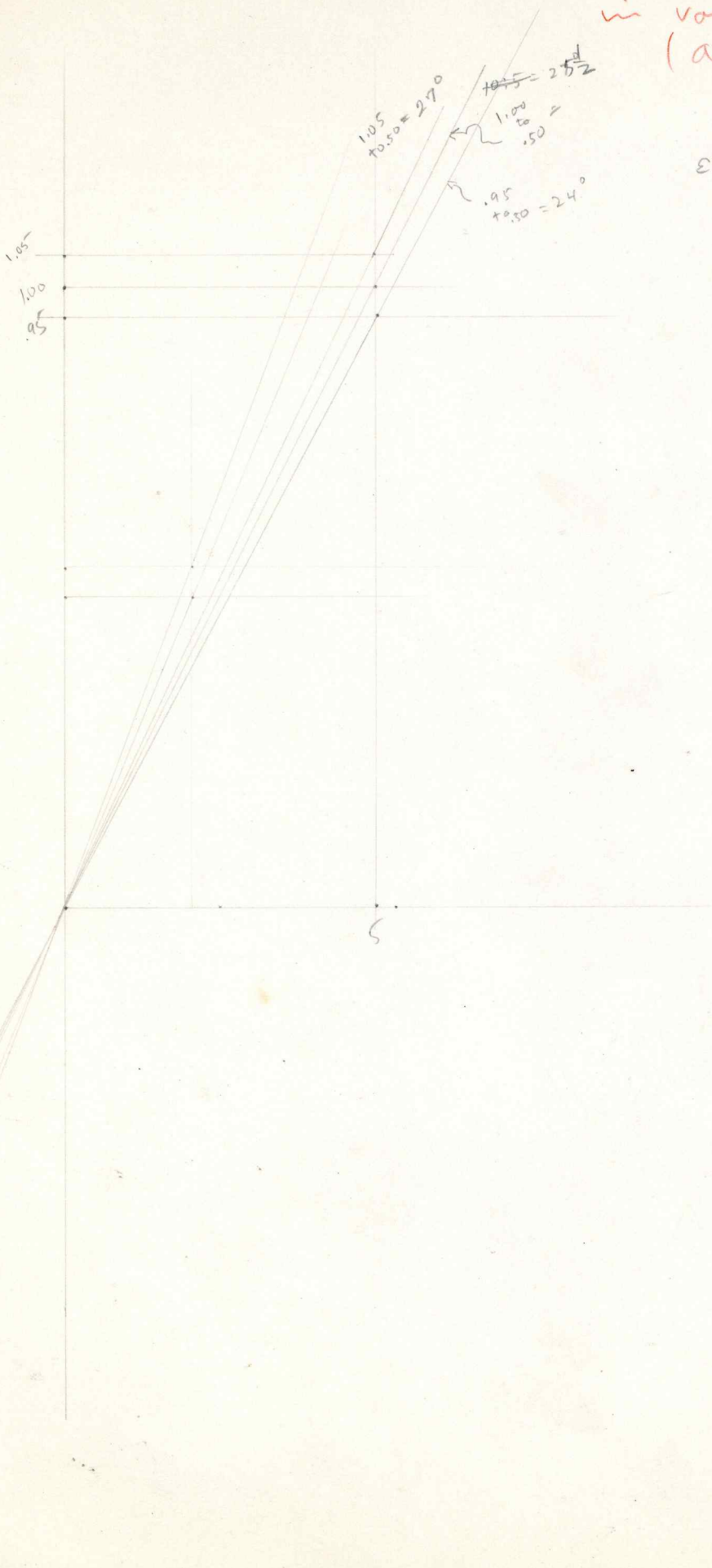
$$\begin{array}{r}
 5.65 \\
 3. \\
 \hline
 2 \overline{) 16.95} \quad 8.475
 \end{array}$$

$$\begin{array}{r}
 5.65 \\
 2.75 \\
 \hline
 2825 \\
 3955 \\
 1130 \\
 \hline
 185375 \\
 8.475 \\
 3.391 \\
 \hline
 16 \overline{) 27.4025}
 \end{array}$$

$$\begin{array}{r}
 5.65 \\
 1.2 \\
 \hline
 1130 \\
 565 \\
 \hline
 2 \overline{) 6.780} \quad 3.39
 \end{array}$$

$$\begin{array}{r}
 16 \overline{) 27.4025} \quad 1.7370 = 1.74 \text{ sq. meters.} \\
 \underline{16} \\
 114 \\
 \underline{112} \\
 60 \\
 \underline{48} \\
 122 \\
 \underline{112} \\
 105
 \end{array}$$

Test for error  
in vault measure.  
(angles).

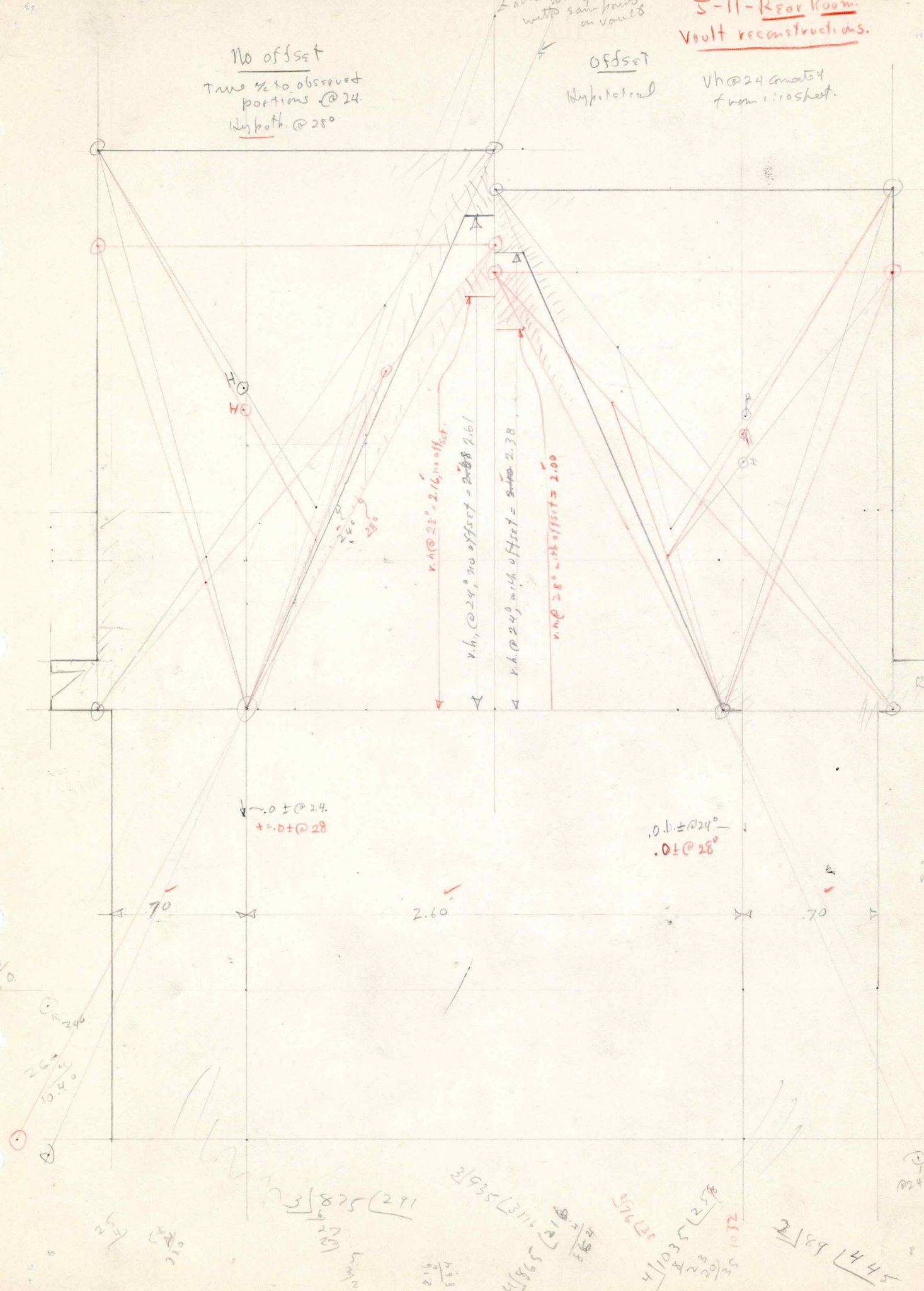


5-11-Rear Room  
Vault reconstructions.

No offset  
True 1/2 to observed  
portions @ 24.  
Hypoth. @ 28°

offset  
Hypothetical

Vh @ 24 cm to 54  
from 1:10 sheet.



v.h. @ 28° = 2.16, no offset.  
v.h. @ 24°, no offset = 2.11  
v.h. @ 24°, with offset = 2.38  
v.h. @ 28° with offset = 2.00

.0 ± @ 24.  
± .0 ± @ 28

.0 ± @ 24°  
.0 ± @ 28°

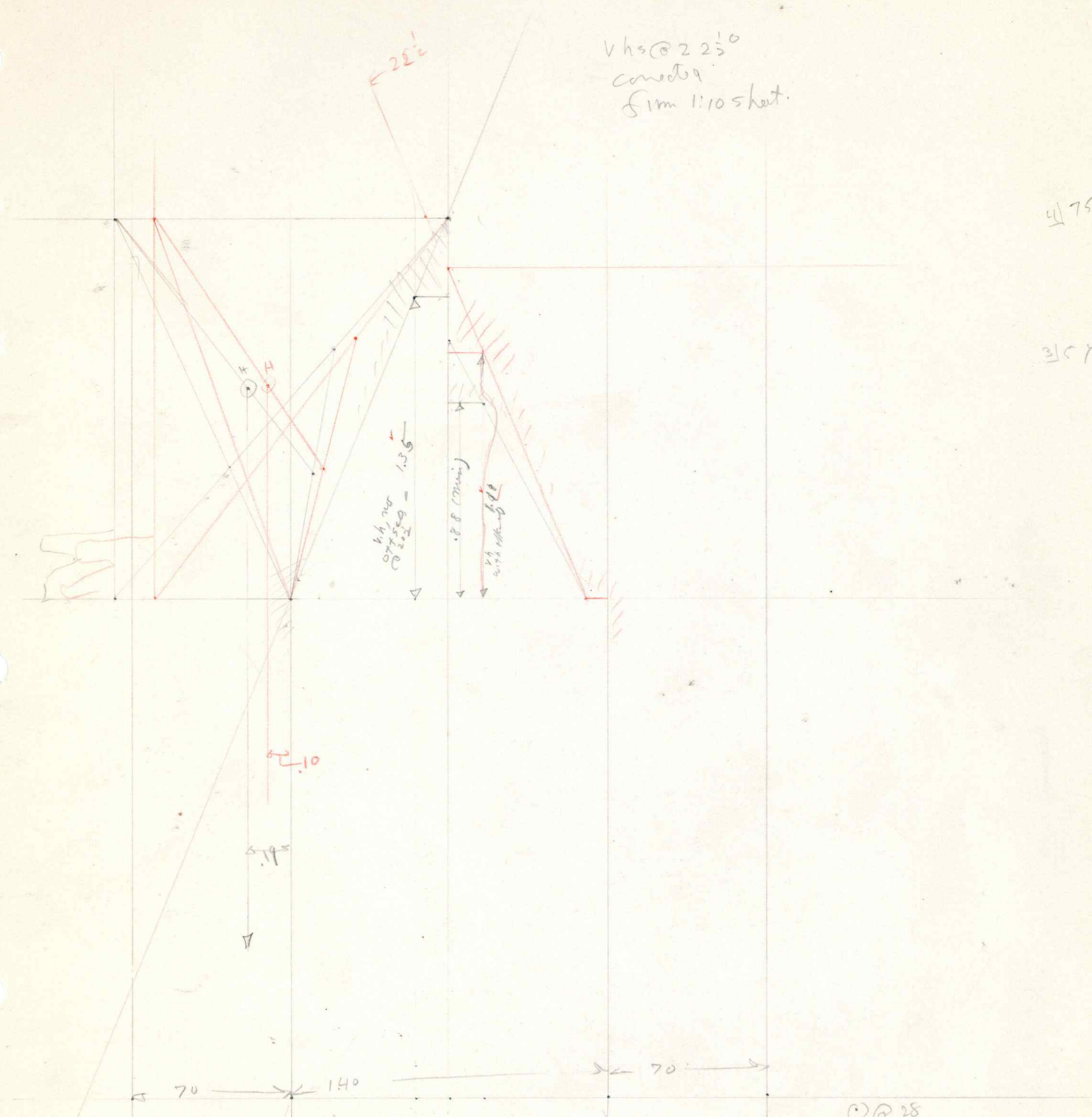
260  
1040  
246

3525 (283  
25  
1101  
24  
25

25  
220  
3 | 875 (291  
27  
10  
2  
216  
554  
5 | 965 (311  
21  
2  
562  
4 | 1035 (258  
23  
20  
35  
1032  
2 | 89 (445

5-23

Vhs @ 22 1/2°  
conductor  
firm 1:10 sheet.



4175 119  
3157 117

223  
592  
22 1/2°

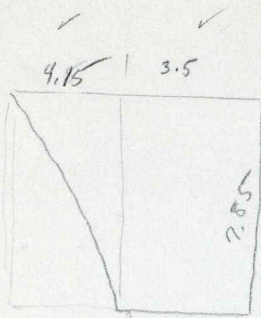
136  
4  
544

435 109  
436  
140  
56  
4535 135  
31535 1175  
23  
15

4135 187  
32  
30  
22

⊙ @ 28

I-22



with off set,  
out set vert  
Entabl.

$$\begin{array}{r}
 3.5 \\
 \hline
 7.85 \\
 3925. \\
 \hline
 2355 \\
 \hline
 27475 \\
 \hline
 16.232 \\
 \hline
 43707
 \end{array}$$

$$\begin{array}{r}
 4.5 \\
 \hline
 7.85 \\
 3725 \\
 \hline
 3170 \\
 \hline
 2) 3.3250 \\
 \hline
 6.65 \\
 \hline
 17.662
 \end{array}$$

$$\begin{array}{r}
 4.15 \\
 \hline
 7.85 \\
 2085 \\
 \hline
 3320 \\
 \hline
 2905 \\
 \hline
 2) 325775 \\
 \hline
 65155 \\
 \hline
 12 \\
 \hline
 13 \\
 \hline
 5 \\
 \hline
 4 \\
 \hline
 17 \\
 \hline
 16 \\
 \hline
 17
 \end{array}$$

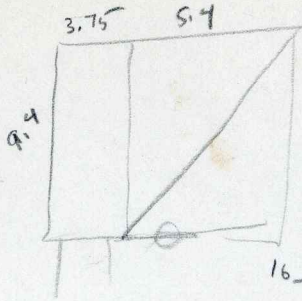
$6.28+ = 16.23$

$$\begin{array}{r}
 16 \ 4370 \ 2.73 \\
 \hline
 32 \\
 \hline
 117 \\
 \hline
 128 \\
 \hline
 50 \\
 \hline
 48 \\
 \hline
 2
 \end{array}$$

about min. for  
no thrust.

5-6-2nd

(Good seed,  
for stability).



3.75	5.4
9.40	9.4
15000	216
33750	486
362500	
25.38	

16 | 68,630  
 48 |  
 126 |  
 112 |  
 143 |  
 128 |  
 156 |  
 144 |

2 | 50.76 | 25.38 58 mt  
 2 | 50.76 | 25.38  
 3.589 = 3.59 58 mt

8.5  
~~8.5~~  
 8.5  
 3.75  
 12.25

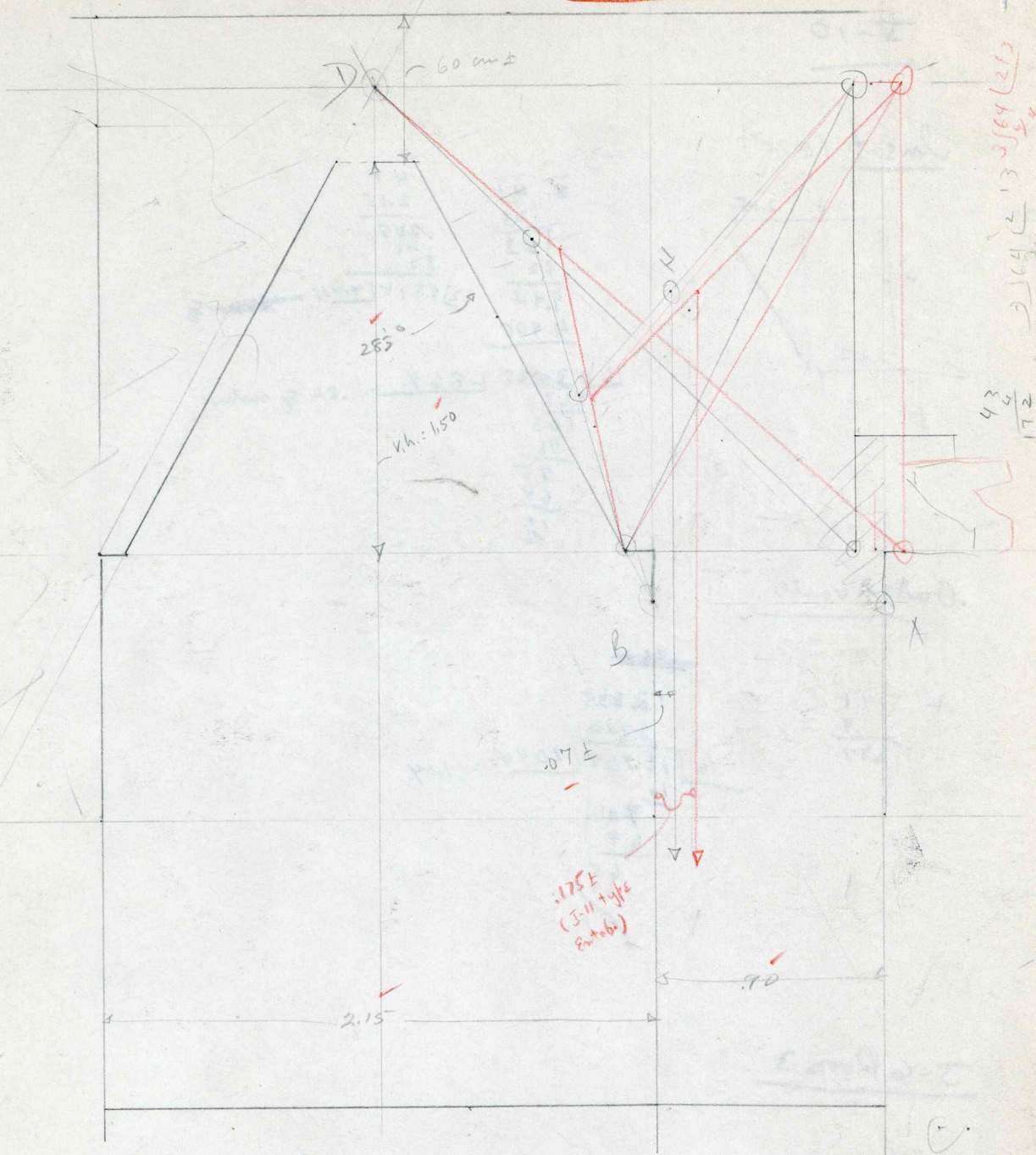
3.75  
 5.4  
 9.15

Vert Zone

5-6 - Rim 3

A

69  
23  
Add  
9200



5-6 Room 3

Reconstructed vault

H = center of gravity.

with soap envelope

$$4 \overline{) 2360}$$

$$\begin{array}{r} 2.16 \\ 8 \overline{) 17.28} \\ \underline{16} \\ 128 \\ \underline{128} \\ 0 \end{array}$$

$$\begin{array}{r} 2.15 \\ 8 \overline{) 17.2} \\ \underline{16} \\ 120 \\ \underline{120} \\ 2 \end{array}$$

$$\begin{array}{r} 1.67 \\ 4 \overline{) 6.68} \\ \underline{6} \\ 108 \\ \underline{108} \\ 0 \end{array}$$

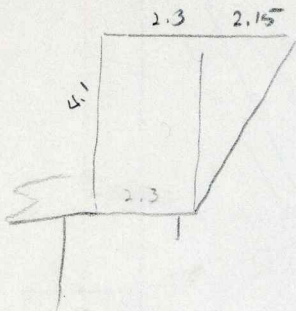
1000  
1000  
1000

1000  
1000  
1000

5-10

Inset (@28°)

$$\begin{array}{r} 4.45 \\ 2.3 \\ \hline 2.15 \end{array}$$



$$\begin{array}{r} 4.1 \\ 2.3 \\ \hline 1.23 \\ 82 \\ \hline 9.43 \\ 4.405 \end{array}$$

$$\begin{array}{r} 4.1 \\ 2.15 \\ \hline 2.05 \\ 41 \\ 82 \\ \hline 2) 8.815 \end{array} \quad \begin{array}{r} 4.405 \\ \hline 1.864 \end{array}$$

$$\begin{array}{r} 16 \overline{) 13.835} \\ \underline{128} \\ 103 \\ \underline{96} \\ 75 \\ \underline{64} \\ 11 \\ \underline{16} \end{array} \quad 1.864 = .86 \text{ of meter}$$

Outset would

$$\begin{array}{r} + 4.1 \\ .7 \\ \hline 2.87 \end{array}$$

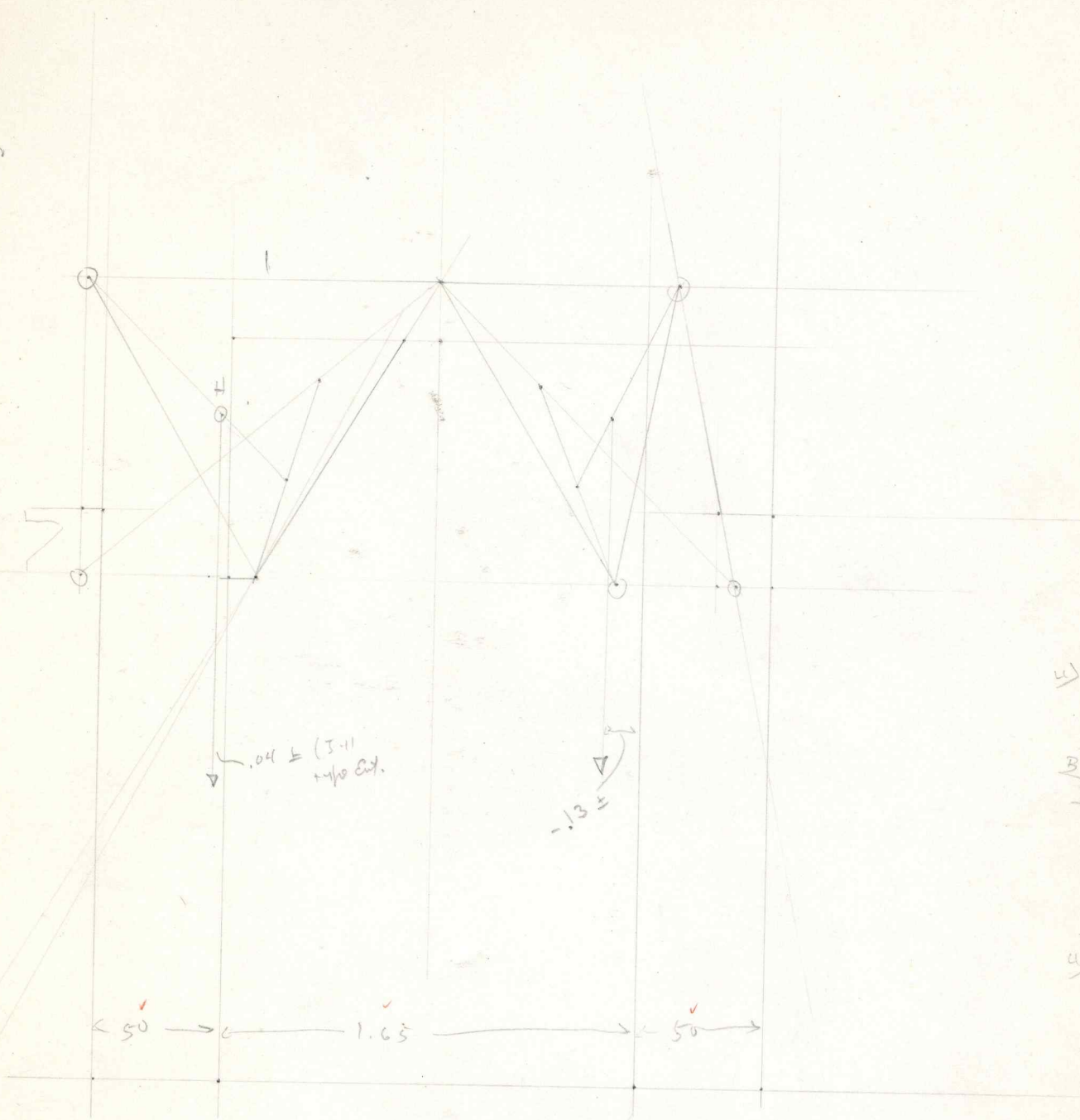
~~8.64~~

$$\begin{array}{r} 13.835 \\ 2.870 \\ \hline 16 \overline{) 16.705} \\ \underline{16} \\ 70 \\ \underline{64} \\ 65 \\ \underline{64} \\ 1 \end{array} \quad 1.044 = 1.04$$

5-6 Room 3

Room 6 of 5-2

45  
300



56

.04 ± (3-11 + 1/10 Ext.)

-.13 ±

← 50 →    ← 1.65 →    ← 50 →

165  
660

4) .055 ← 4  
75  
10

3) 26 ← 866  
24  
20  
20

4) 660 ← 165  
26  
20

9 @ 11 1/2"

325  
31°

4) 125 ← 3.2  
10



J-6-Room 1

$$\begin{array}{r} 4 \overline{) 225} \ 56 \\ \underline{200} \\ 25 \end{array}$$

$$\begin{array}{r} 3 \overline{) 645} \ 215 \\ \underline{600} \\ 45 \end{array}$$

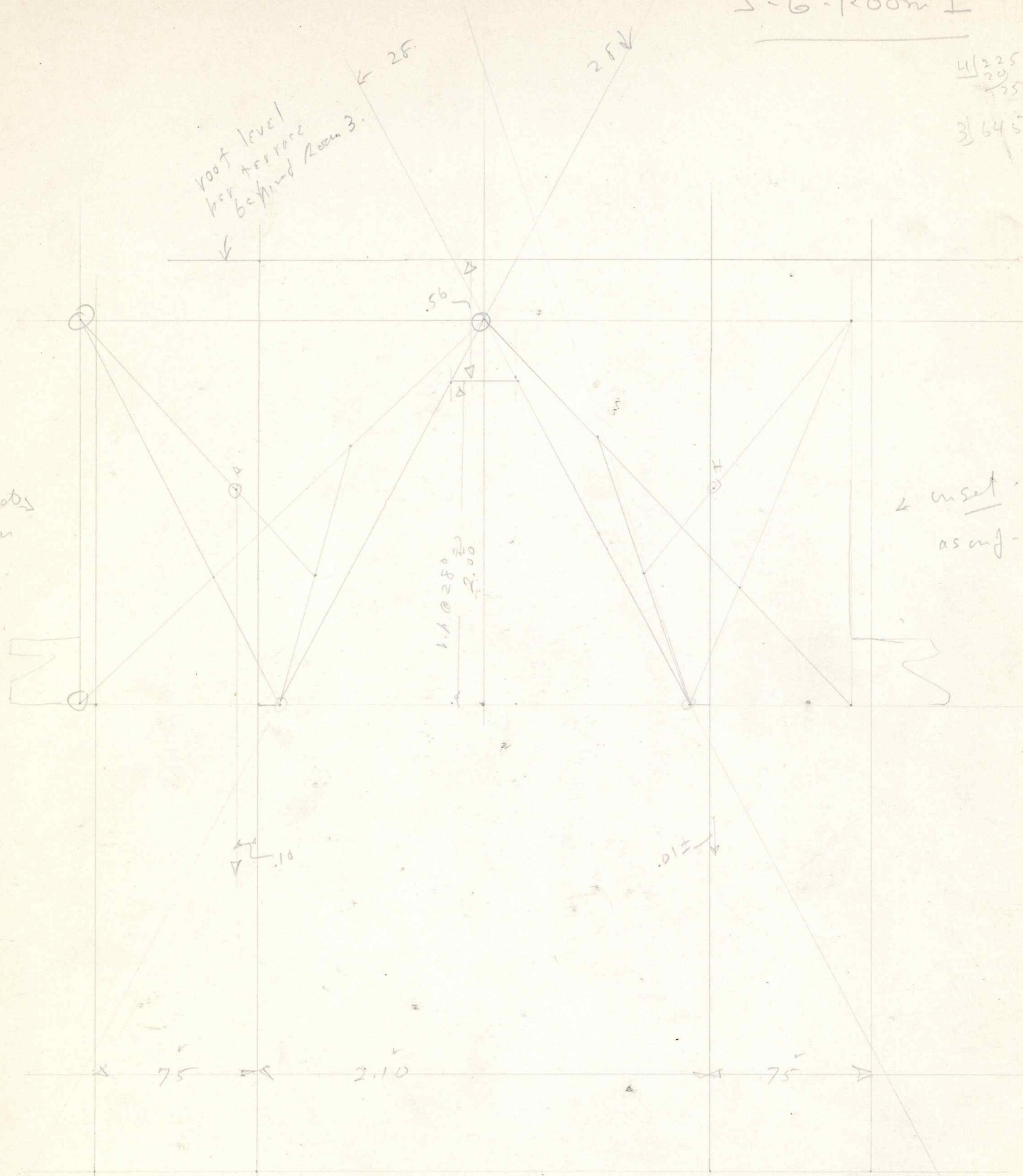
roof level  
 for terrace  
 behind Room 3.

outsets  
 as on  
 J-11.

inset  
 as on J-9.

$$\begin{array}{r} 217 \\ 5 \overline{) 65} \\ \underline{50} \\ 15 \end{array}$$

$$\begin{array}{r} 210 \\ 5 \overline{) 65} \\ \underline{50} \\ 15 \end{array}$$



O-223

O-224

$$\begin{array}{r} 4 \overline{) 29} \ 210 \\ \underline{200} \\ 90 \end{array}$$

$$\begin{array}{r} 4 \overline{) 300} \ 25 \\ \underline{280} \\ 20 \end{array}$$

← *truss height*

← *abbin voo height (4.20)*

*v.h. = 1.85 m. Not used (2.28)*

*v.h. = 1.69 m. offset (2.28)*

$$\begin{array}{r} 2.28 \\ 9 \\ \hline 1.3 \end{array}$$

0.05

0.50

70      2.28

70

4.225

0.025

0.025

$$\begin{array}{r} 1.85 \\ 740 \\ \hline 2 \end{array}$$

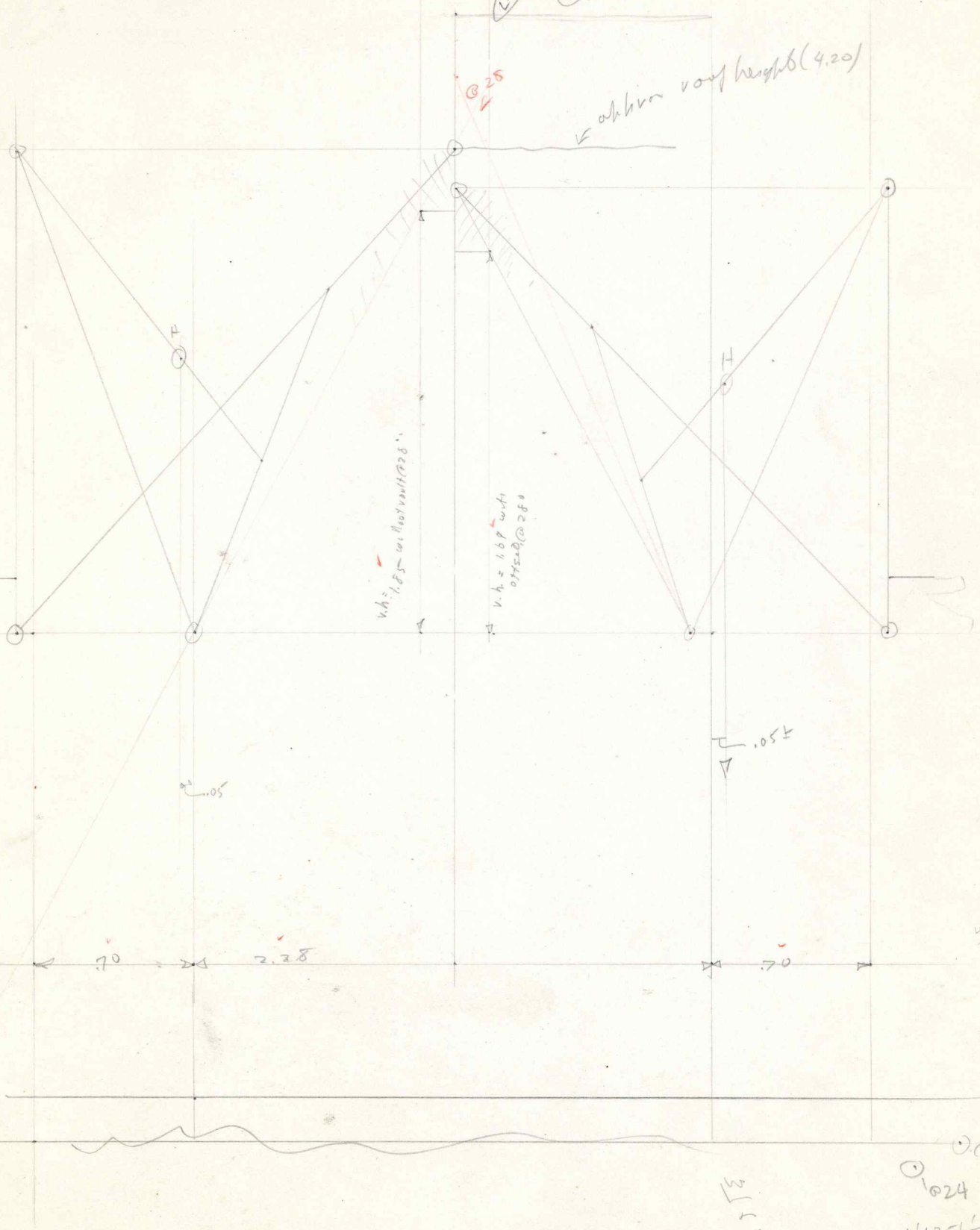
$$\begin{array}{r} 1.69 \\ 740 \\ \hline 2 \end{array}$$

$$\begin{array}{r} 1.69 \\ 676 \\ \hline 2 \end{array}$$

3/172 < 20

$$\begin{array}{r} 4.574 \\ 185 \\ \hline 2 \end{array}$$

$$\begin{array}{r} 4.675 \\ 169 \\ \hline 2 \end{array}$$



Str. I-13

1933

Reconstructed vault section - no thrust at 28° soffit, or greater.

slope = 12°

True outer section

66° off for 1 degree

J-2 outer section

assumed R.30

assumed R.25

assumed offset + height to moulding

assumed

.87

.19 ±

.35 ±

1.62

.55 ±

4/12 1/4

4/7 1/17

4/30

4/28

4/46

4/44

4/30

4/5 1/2

4/5 1/10

3/40 1/33

3/19 1/10

1.05 ±

4/26

3/50 1/66

3/20 1/18

3/20

4/75 1/35

4/41 1/35

4/13 1/32

12/10

4/62 1/150

2/2

2/25

4/12 1/105

20

4/12 1/105

20

4/12 1/105

20



219 22  
16

Sk I-8

3 | 52 | 102

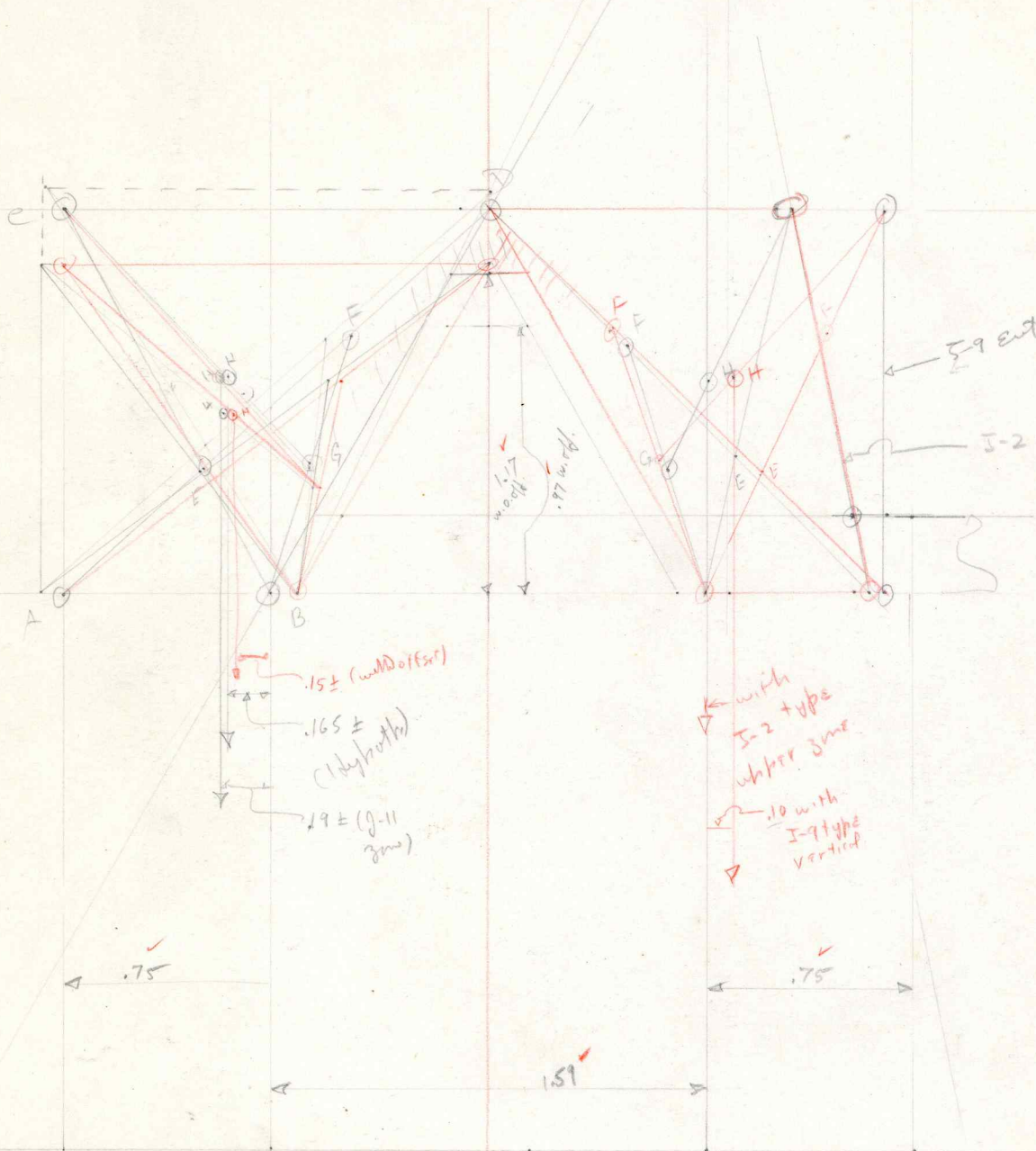
3  
22  
21/10 4 | 6 | 6  
20

38

2.03  
812

216 11  
812

216 11  
812



3 | 42 | 14  
12

117  
468

3 | 31

3 | 31 | 97  
30

3 | 2 | 13  
16

3 | 58 | 193

3  
29  
27  
10

117  
468

3 | 6 | 9  
19  
10

117  
468  
3 | 6 | 9  
315