

SURVEYOR'S NOTE
BOOK

B.
1931

(J. Eagon Wyer)

DIETZGEN
TRADE MARK

ENGINEERS'
FIELD BOOK
No. 400

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1 $\frac{1}{2}$ see inside of back cover.

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J. A. Mason
University Museum
33d + Spruce Sts
Philadelphia

Sight To. Azimuth. Vert. Ang. I. H.D. D.E.

Sight To.	Azimuth.	Vert. Ang.	I.	H.D.	D.E.
ΔD	$70^{\circ}45'$	$0^{\circ}10'$	0.421		
Inst. at ΔC . H.I. = 1.30 m.					
ΔD	$31^{\circ}38'$	$7^{\circ}05'$	0.412	40.894	5.9
1	$83^{\circ}10'$	$8^{\circ}04'$	0.125		
ΔC	$110^{\circ}43'$	$12^{\circ}55'$	0.224		
Instrument at ΔB . H.I. 1.48					
15		$24^{\circ}40'$	0.176		
14	$278^{\circ}13'$	$37^{\circ}04'$	0.540		
12	$106^{\circ}03'$	$0^{\circ}07'$	0.120		
11	$113^{\circ}57'$	$-2^{\circ}51'$	0.360		
10	$122^{\circ}10'$	$-4^{\circ}00'$	0.159		
9	$339^{\circ}12'$	$12^{\circ}36'$	0.206		
8	$198^{\circ}11'$	$0^{\circ}45'$	0.162		
7	$208^{\circ}41'$	$6^{\circ}08'$	0.190		
6	$220^{\circ}36'$	$14^{\circ}56'$	0.228		
5	$290^{\circ}16'$	$26^{\circ}28'$	0.122		
4	$304^{\circ}06'$	$17^{\circ}20'$	0.110	10.126	
3	$317^{\circ}43'$	$0^{\circ}06'$	0.096	9.926	-
ΔD	$14^{\circ}53'$	$5^{\circ}14'$	0.670	66.764	+6.11.
2			0.258	25.326	-
1			0.850	85.326	-
ΔB	$33^{\circ}36'$	$0^{\circ}55'$	0.974	97.70	+1.56
Instrument at ΔA . H.I. 1.33.					

Elev. Mag. Bear.

$S 35^{\circ} 00' W$.

$N 35^{\circ} 35' W$.

$N 33^{\circ} 35' E$.

Bottom of 2nd Wall.

Junction of Pyramids with Terrace.
 Top of Left Pyramid. on
 End of Small remaining Peak
 mound rising off to of wall.

Top of Bank.

Corner of 2nd wall.

Top of Bank on Plaza Level.
 end of 1st wall.

Top of 2nd wall. here appears to
 run into Hill.
 Top of 2nd wall.

Base of 2nd wall.

Constant to be added to
 Stadia Int. (I) = 0.326 metres.

Sta.	Hor. Ang.	Vert. Ang.	Mag. B.	I.	H. D.
π at $\square A$		H. I. = 1.29 m.			27.5
$\square B$	33° 53'	0° 39'	N 33° 35' E	0.975	97.826
$\square D$	15° 09'	5° 13'		0.671	66.907
0.1	33° 53'	0° 30'		0.850	85.326
2	33° 53'	0° 42'		0.673	67.626
3	33° 53'	0° 21'		0.506	50.926
0.4	33° 53'	-0° 33'		0.250	25.326
5	193° 42'	-0° 40'		0.153	15.626
6	202° 03'	2° 01'		0.200	20.076
7	167° 30''	-3° 44'		0.120	11.824
8	121° 53'	-3° 14'		0.162	16.000
9	114° 10'	-3° 03'		0.360	36.223
10	311° 16'	8° 20'		0.082	8.34
11	302° 06'	17° 33'		0.110	10.29
12	292° 20'	26° 24'		0.131	10.05
13	278° 14'	24° 29'		0.181	15.22
0. I	278° 30'	36° 54'		0.531	34.20
14	347° 48'	6° 31'		0.201	20.16
15	339° 41'	12° 22'		0.205	19.826
16	209° 34'	8° 29'		0.233	23.300
17	220° 34'	13° 56'		0.223	21.50
18	211° 37'	10° 49'		0.322	31.37

π at $\square B$ & B.S. (0°) on $\square A$.	H. I. = 1.32
D 31° 37' 6° 57'	0.409 40 m
C 110° 44' 12° 35' N 35° 45' W	0.223 21.4

April-16-1931.

Mag. Bear. taken at 8.30 a.m. Distance Chpd. 97.

Vertical Ang. taken with Rod on Ground.

Vert. Ang. taken with Rod on grd.

} Top of Bank. - faces with rock.

Hub on Top of Pyramid.

} Corners of Terraces.

April-17-1931.

Sight To.	Hor. Ang.	Ver. Ang.	Mag. B.	I.
19.	145° 59'	1° 53'		0.145 14.8
20.	72° 09'	9° 15'		0.100 10.3
21.	37° 35'	5° 57'		0.171 17.2
22	43° 15'	10° 16'		0.208 20.1
25	82° 57'	16° 50'		0.145 14.3
24	84° 19'	8° 09'		0.124 12.0
23	130° 55'	8° 24'		0.171 16.9
□ B1	180° 46'	-0° 41'	N34° 35' E	0.661 66.1
□ B2	268° 03'	-0° 50'	S61° 50' E	0.705 70.5
26	161° 14'			27.60
27	180° 39'			26.47
28	197° 28'			27.70
29	212° 25'			31.63
○ 1	0° 00'	-1° 33'		0.125 12.5
30	16° 16'	3° 21'		0.270 27.0
31	268° 03'	0° 15'		0.353 35.3
32		-0° 39'		0.560 56.0
π at □ C & B.S (0°) on □ B				H.I = 1.35
□ B	0° 00'	-12° 40'		0.225
□ D	70° 45'	0° 10'	S35° 30' N	0.421
○ H	135° 03'	34° 05'		0.414
33	341° 44'			4.05
34	348° 14'			2.50
35	32° 14'			5.50
36	50° 51'			4.60

} Top line of Retaining wall of 1st Terrace.	
} Top line of Retng Wall of 2 nd Terrace.	
Base of 2nd Retng Wall.	
Dist: measured with tape.	
"	" " " (0.263 Stadia I.)
"	" " " "
"	" " " "
26, 27, 28, 29. Ends of Mnds of Ball Court. W.G.	
Center of Stone Stairway.	
Check sight for Dist & Elev.	
Stake with nail near Summit of Pyramid.	
Tape dist	14.03
" " "	} Base Well Stela # 8
" " "	} " " " # 7.

37	59°33'	2.70
38	9°04'	5.15
39	41°11'	7.93
40	51°16'	7.83
41	53°18'	12.17
42	59°40'	11.50
43	56°23'	14.17
44	62°39'	13.96
45	56°41'	15.56
46	56°53'	17.25
47	63°49'	19.03
48	67°38'	18.70
50	67°45'	20.80
49	64°06'	21.08

51	67°47'	-0°16'	0.0425
52	33°27'	-16°26'	0.0385
53	358°43'	-3°50'	0.0225
54	33°37'	+2°30'	0.0610
55	39°07'	-3°33'	0.0560
56	43°18'	-2°00'	0.0785
57	58°47'	-2°08'	0.1020
58	55°53'	-2°25'	0.1280
59	61°14'	-50°00'	0.1515
60	66°54'	+53°00'	0.1910
61	4°01'	-7°43'	0.0345
62	78°13'	+3°41'	0.1720

Tape Dist.	2.70	} North end Plinth for Stela
"	"	
"	"	} Base well Stela #6
"	"	
"	"	} Base well Stela #5
"	"	
"	"	} Base well Stela #4
"	"	
"	"	" #3
"	"	" #2
"	"	" #1

H.I. = 100 m. April-18. Level of floor at rear of Plinth

" well #8.

" Curb #8.

" " #7 (top of Plinth).

" Well #7

" " #6

" " #5

" " #4.

" " #3

" Curb #2.

" between #8 & #7.

63	122° 19'	+18° 00'	0.1340
66	117° 24'	+10° 33'	0.0940
64	190° 50'	-0° 26'	0.0475
65	226° 36'	-18° 05'	0.1215
66	70° 12'	+1° 09'	0.2220

π at □ D. with B.S. (0°) on C □ H.I. = 1.00m.

□ C 0° 00' -0° 06' 0.4220

□ B 30° 11' -6° 57' 0.4120

□ A 159° 48' -5° 10' 0.6700

□ E 259° 46' +22° 11' N65° 45' W 0.2040

d. 16.9
e = 7.69

Ck sight to B □

" " " A □ Int. Ang. B-D-A = 129° 37'

Sight to. Hor. Ang. Vert Ang. M.B. I. H.D. D.E.

⊥ @ "I" □	B.S on "A" □	H.I. 1.25
A 0°00'	-37°00'	0.530
1. 358°35'	-43°28'	0.193
2. 358°45'	-40°23'	0.1515
3. 329°03'	-39°25'	0.132
4. 332°09'	-42°02'	0.096
0 5. 52°45'	-29°50'	0.438
6. 99°47'	+3°09'	0.072
7. 133°20'	+17°13'	0.083

(Target on rod at 0.85)

Middle Hair @ 1.10.

— H.I., 1.32,

Sight To.	Hor. Ang.	Vert. Ang.	Mag. B.	I.	H.D.
π @ "B" \square .		H.I.	1.365		
2	90° 00'	-3° 24'		0.075	7.826
4		+15° 06'		0.159	15.1
5		+23° 22'		0.197	16.9
6	99° 50'	+23° 27'		0.215	18.42

π @ "D" \square .	B.S. on "A".	H.I.	I.	H.D.
1.	46° 29'	-2° 50'	0.062	6.2
F.	90° 00'	+27° 09'	0.300	26.2
7	86° 26'	+27° 04'	0.278	22.3
8	86° 16'	+25° 57'	0.239	19.5
9	86° 53'	+23° 21'	0.211	18.2
10	91° 12'	+14° 20'	0.162	15.14
11	124° 53'	+7° 14'	0.121	12.28

π @ "D" \square .	B.S. on "A".	H.I.	I.	H.D.
12	90° 35'	+22° 18'	0.214	19.78
13	87° 57'	+23° 30'	0.228	20.9
14	79° 56'	+22° 08'	0.212	19.6
15	86° 17'	+26° 15'	0.234	21.2

π @ "B" \square .	B.S. on "A".	H.I.	I.	H.D.
D.	180° 00'	1° 12'	0.199	19.9
16	85° 46'	21° 26'	0.215	18.95
17	84° 38'	23° 33'	0.224	19.0

12.40
1.27
10.43
16.2

16.106
1.14

0.269
4.0
1.269

D.E.	Pyramid # 27.	B.S. I.S. F.S.	
-	462.	1.269.	1 20.000
+	4.080	(-0.563) 1.832.	2
	7.27	1.269.	1
	8.00 ^{1.95}	(+1.076) 1.193	3
	.36		
	13.4	Top level.	
	11.4		
	9.50		
	7.78		
	3.96		
	1.55	Lower Terrace.	
	8.15	Front edge of face wall at Bottom.	
	9.18	Top of edge of vert. low wall	
	9.34	front lower edge of wall under stairs	
	20.35	top (9) + (12).	
	.43		
	7.42	Lower front edge bottom Vert.	
	8.30	Top	

				H.D
18	86°55'	25°25'	0.246	20.3
19	88°03'	28°07'	0.275	21.6

⊥ @ F.□ B.S on " D"□ H.I. - 1.38.

G	90°00'	-0°42'	0.265	26.8
20	91°19'	-0°57'	0.256	25.6
21.	91°22'	-1°00'	0.252	25.2
22	90°04'	-1°05'	0.202	20.5
23	90°19'	-0°40'	0.185	18.8
24	91°11'	+0°17'	0.165	16.8
25	88°13'	+2°56'	0.165	16.8
26.	87°55'	+1°39'	0.165	16.8
27	86°57'	+1°16'	0.162 ⁵	16.55
28	86°22'	+0°25'	0.161 ⁵	16.45
29	85°38'	-0°50'	0.160	16.3
30	85°34'	-2°00'	0.160	16.3
31.	90°35'	-1°05'	0.134	13.9
32	87°56'	-1°58'	0.210	21.3
33	83°43'	-2°43'	0.200	20.3

D.I.E		
9.7		Midway up 2. better face.
11.42		Top edge.
.33		
.43		Top of small rise.)
^{44.5}	Centre hair on 1.50.	Base of steps & } ± continuation of Base of Plinth.
^{38.8}	Centre hair on 1.50.	Outer edge - level of floor outside staircase.
.22		Middle wall at end of Stair.
.086		Inner wall.
.86		Top Tread of Stairs.
.485		" " "
.366		" " "
.12		1st " " "
*.237		1st " " "
*.57		Floor level.
*.258		Level behind & below Staircase at base of wall.
.73		Top edge & level of inner wall.
.96		Top edge of outer wall at junct with main staircase.

34 $84^{\circ}30' - 1^{\circ}49'$ 0.129 13.2

35 $84^{\circ}24' - 0^{\circ}10'$ 0.121 12.4

.419
.036

Flow level in part of stairs.
1st. floor on edge.

B.S.	I.S.	F.S.	Rise	Direct fall.	levelling R.L.
0.156					2.558
	0.072.		0.084		2.642
	0.127.			0.055	2.587
	0.608.			0.481	2.106
2.714		2.714		2.106.	0.006
	0.269.		2.445		2.445
	0.015		0.254		2.699
	0.215			0.200	2.499
	0.305			0.090	2.409
	-0.050		0.		
		1.027		0.722	1.687

Sta.	Hor. Ang.	I.	$\frac{3.4}{2}$	D.E.
□ F.	- 9° 26'	0.034		1.65
1	+ 15° 56'	0.045		1.27
2	+ 15° 44'	0.055		1.52
3	+ 18° 24'	0.047		1.50
4	+ 19° 26'	0.099		3.20
5	+ 17° 19'	0.084		2.46
6	+ 13° 23'	0.054		1.285
7	+ 17° 27'	0.100		2.04
8	+ 17° 9'	0.062		1.935
9	+ 19° 39'	0.131		4.23
10	+ 26° 57'	0.166		6.82

levelling with Transit. Edifice on Pyr. # 27.

- Corner of Base of Edifice Sta. 1.
- Floor level at entrance S.E. corner Sta. 2.
- Level of edge of Terrace C. Sta. 3.
- " " " " B. Sta. 4.
- X Top of Stake □ "F"
- Edge of Terrace "C" in front of 2nd entrance S.E.
- Floor level entrance #2 S.E. right hand corner
- Terrace "C" centre of Pillar to right of Main entrance
- ledge + 0.050 above line of sight
- Edge of Terrace "B" in line with left corner of double wall.

B.S. on □ F.

- Edge of Terrace to 2nd opening
- Floor at entrance
- Floor level against wall
- Top of ledge
- Point 2.65 from front of building - base against 2nd floor
- Edge of Terrace C. main entrance
- 2nd floor level middle entrance
- Floor level centre hall
- Raised floor level of middle Rooms.
- Point on left hand front wall of rear room -
- lowest floor level of rear room 3.40 below this point
- second floor level of rear room 3.00 below same point

Sta	Hor Ang	I	DE
□ G -	4° 12'	0.198	

□ G -	22° 04'	0.060	
11 +	21° 22'	0.074	
12 +	24° 42'	0.095	
13 +	16° 56'	0.078	
14 +	17° 46'	0.072	

□ G -	8° 51'	0.143	
15 -	9° 00'	0.019	
16 +	23° 22'	0.047	
16 +	17° 47'	0.038	
17 +	15° 51'	0.078	
18 +	16° 43'	0.085	
19 +	15° 14'	0.085	
20 +	20° 02'	0.097	
21 +	7° 33'	0.099	

B.S. on. □ G.

Top of ledge N.W. end.

Top of battered wall SE end of rear end room N.W.

Floor level of end room N.W. end, inside partition wall

Floor level of end room.

B.S. on. □ G.

Corner (N°) of ledge on lower part of Plinth.

N° Corner of Building on ledge above Terrace. c. ?

Level of Terrace.

1st. Step at rear of Building.

2nd - - - - -

Corner of Terrace. at rear ..

Ledge on Top of battered rear wall.

Lower platform or Terrace at rear.

$$\begin{array}{r} 1.25 \\ .40 \\ \hline 0.85 \\ 4.25 \\ .326 \\ \hline 4.576 \end{array}$$

4.595

$$\begin{array}{r} 0875 \\ 775 \\ \hline 1.650 \end{array}$$

$$\begin{array}{r} 159.48 \\ 30.11 \\ \hline 129.37 \end{array}$$

$$\begin{array}{r} 1985 \\ 400 \\ \hline 2.385 \end{array}$$

$34 \times 1000 \times K = C$
 $34 \times 100 \times K = 0/10$

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

