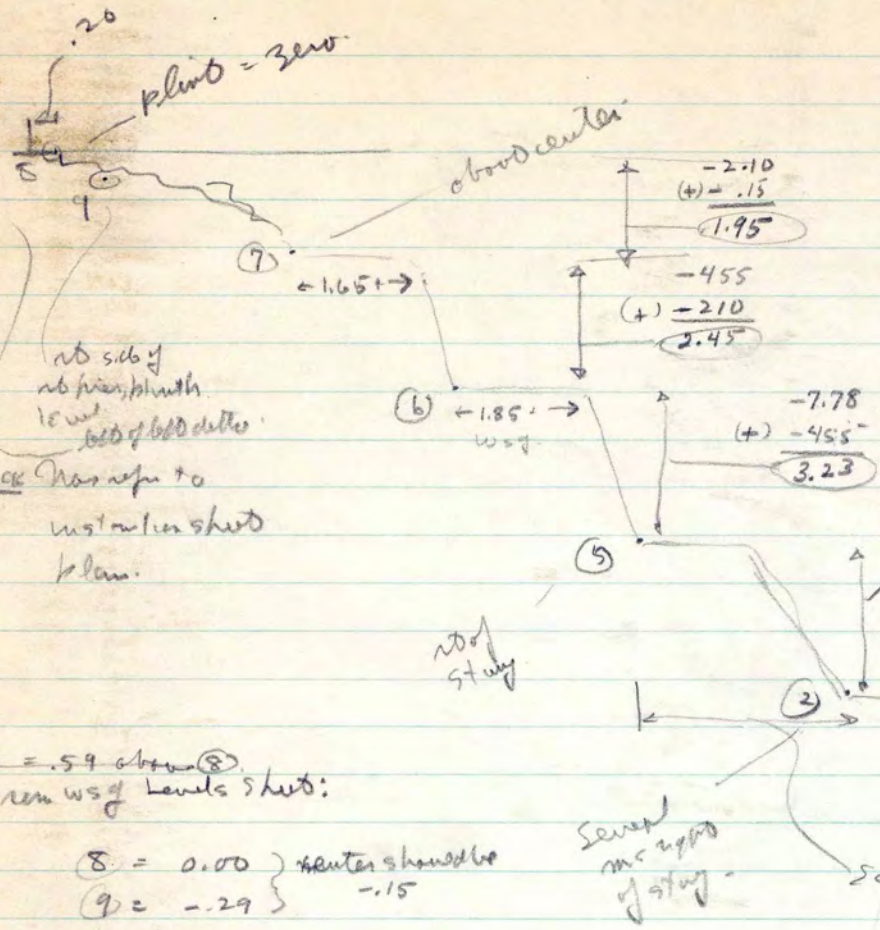


B-12

Average figures for record

Heights: 1st 3.25
2nd 3.25
3rd 2.45
Bld. Plat 1.95

Tenace widths.
1.65 to stdg
1.85
1.70 (scaled)
2 | 3.50 | 1.75

See note to check
and see - this may
be up to .30 too
little, handle the
reverse

1.75
1.75
80
80
62
5.72

wsg scales
6.50
5.72
3 | 17.18 | 29 to each
- 11.03 | 6
+ - 7.78 | 18
3.25

Tenace?
- No. - just
as likely
about. as
tenaces is
wrong, which
would account for
some of this.

hi = .59 above (8).
From wsg Levels Sheet:

(8) = 0.00 } centers should be
(9) = -.29 } -.15

(7) = -2.105

(6) = -4.55

(5) = -7.78

(4) = -10.89 (top of both slabs, center).

(3) -10.84 (" " " " end of slab)

(2) -11.03

3.25
3.23
2.45
8.93
+ 1.95
10.88
.15 - taken off for center
10.73 = reading

2.50
1.70
.80 rise/run

256
x 2
5.00
+ 62 slope of 3rd
5.62

Slabs, 1st tenace, top.
(Fairly good, more to test.

1939 LS

Section through crest

hi = .70 above sill in tumble.

Pt. ② road dam .95

③ " " 2.75 (Top of lowest Bld Pl. stone)

④ " 3.47 (Pavement?) of Bldg. plan and near right corner

hi .05 above bound ④

⑤ road d. 3.17 (pavement)

hi .50 above bound ④.

⑥ Bound on stone ch.

road dam 3.93 ±

hi road .52 above bound ⑥

⑦ road d. 1.76

⑧ " 2.00 (Stake is in bed rock)

⑨ " 2.39 } same hi.

⑩ " 2.28 }

⑪ road d. 2.71

⑫ " " 2.73

⑬ " " 3.87

hi 1.25 above bd. ⑪

14 road d. 1.30 } on bed rock-wall on this

15 " " 1.40 }

Cost, 77¢ under 1.30 + Mag. 3.15 + road 3.93 (pavement) 5.08 - pavement 2.60 Concrete - Pavement 2.73 Tarvia

& See WSG Survey Plan

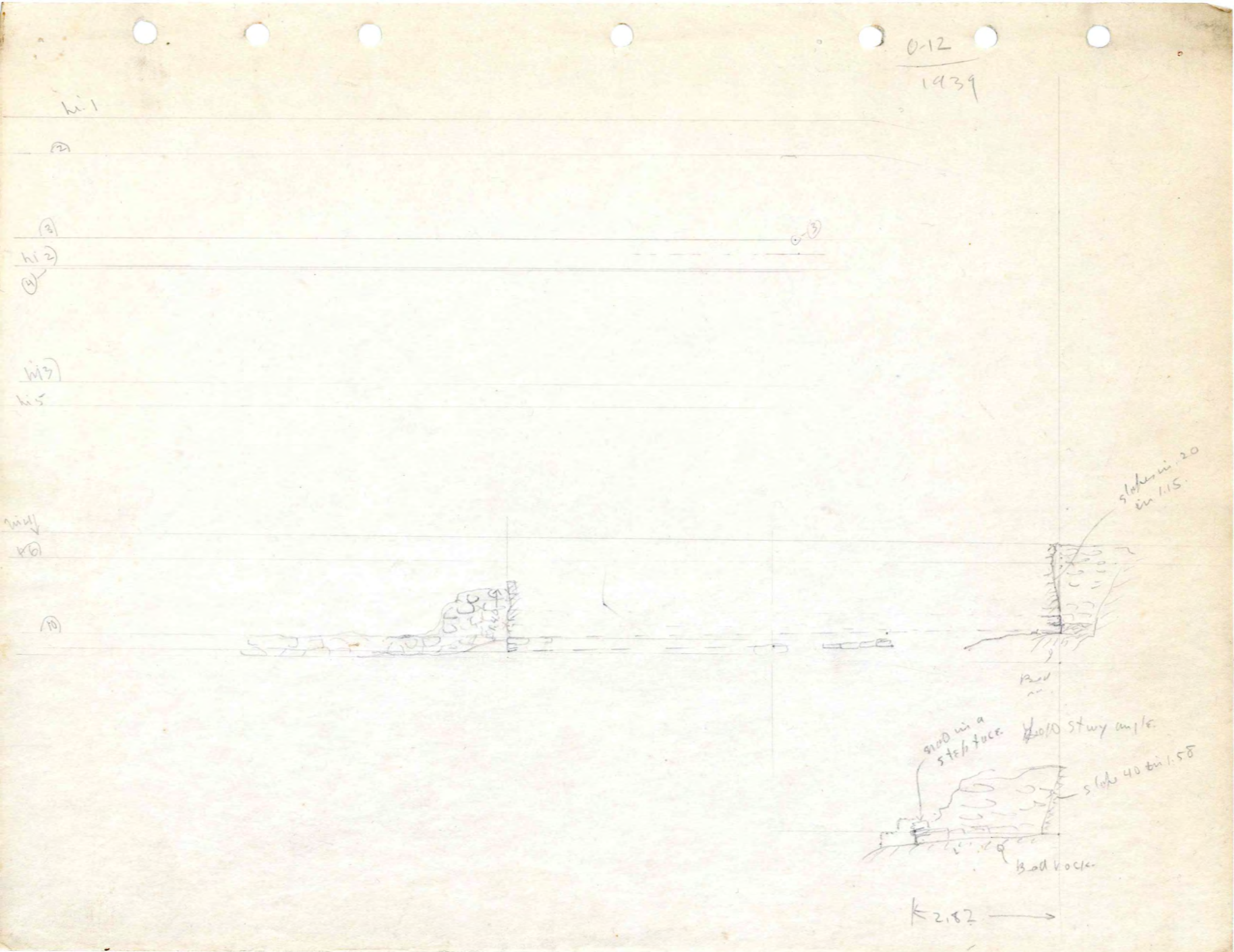
0-12

Many 5' sets 5-10

Corner of stone, squaring up with main lines

0-12

1939


hi 1
(2)
(3)
hi 2)
(4)
hi 3)
hi 5
(6)
(10)
slope in 20 in 1.15
Bed
good in a strb face
1:0.10 stwy angle
slope 40 in 1.58
Bed Rock
K 2.82

hi 1

(2)

(3)

hi 2

(4)

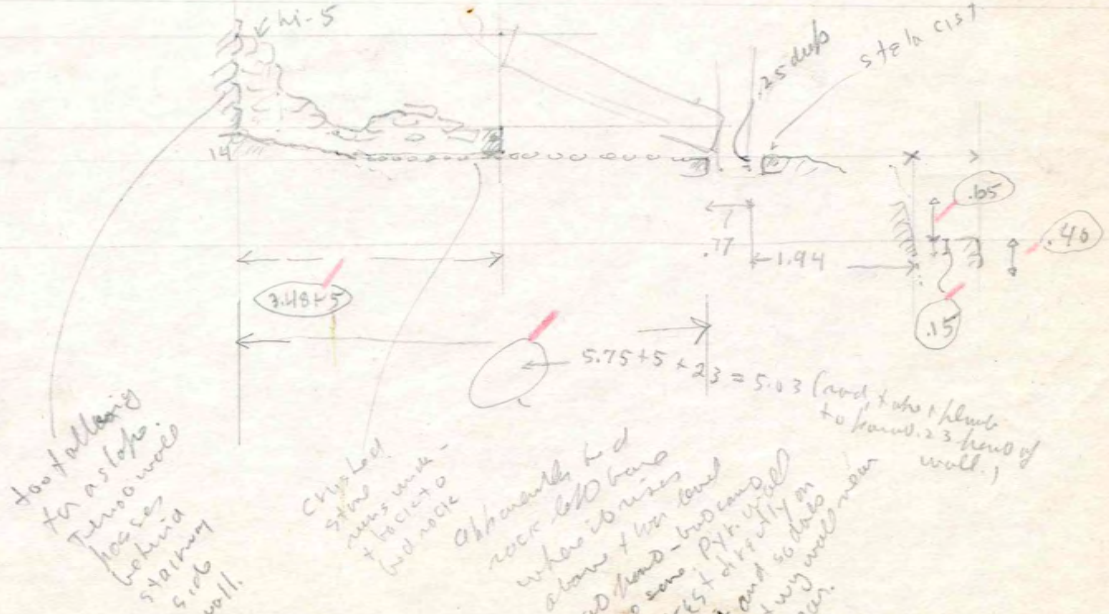
hi 3

(5)

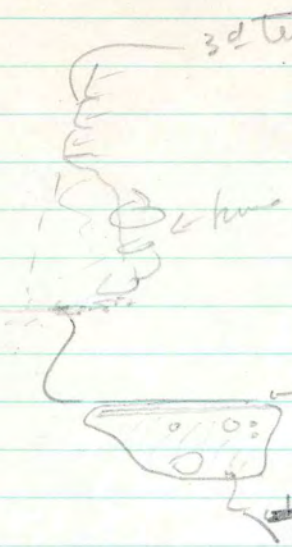
hi 4

(6)

(10)



B-13
June 24 (49)



light yellow matrix
very light cream chocolate } = f.p.
unsevd. type.
ID was poor ph-1.2 in basement

Fairly dry. No wash exhaust of
f Con could be found - probably
badly broken by weight of fill -
wash - a Bud layer of chicos, some
a less gray, ahead as I went further
in.

The general light ahead here probably results
from presence of bed rock (1.P sandstone)

W-S-g.
1940

0.12 Transit shots.

B-1	1 - 2 = 4.85 (+)		1 - 3 = 13.53 (+)		B1 - B3 - B2	15° 18'
B2	2 - 3 = 9.71 (+)					
B3	B3 - B1 - B2	31° 47	B3 - B2 - B1	132° 59		
1	1 - B1 - B2	177° 33	1 - B2 - B1	1° 04	1 - B3 - B2	23° 12
2	2 - B1 - B2	115° 05'	2 - B2 - B1	24° 08	2 - B3 - B2	28° 08
3	3 - B1 - B2	57° 57'	3 - B2 - B1	67° 23	3 - B3 - B2	17° 33
4	4 - B1 - B2	41° 17	4 - B2 - B1	119° 53	4 - B3 - B2	94° 15
5	5 - B1 - B2	96° 30	5 - B2 - B1	49° 22	5 - B3 - B2	44° 22
6	6 - B1 - B2	88° 01	6 - B2 - B1	69° 35	6 - B3 - B2	70° 42
7	7 - B1 - B2	87° 09	7 - B2 - B1	75° 13	7 - B3 - B2	85° 10
8	8 - B1 - B2	62° 36	8 - B2 - B1	72° 51	8 - B3 - B2	89° 39
9	9 - B1 - B2	102° 58	9 - B2 - B1	61° 11	9 - B3 - B2	75° 26
10	10 - B1 - B2	30° 05'	10 - B2 - B1	54° 45'	10 - B3 - B2 Away from pt.	1° 30
11	11 - B1 - B2	41° 27'	11 - B2 - B1	38° 14	11 - B3 - B2 to pt.	2° 08

Levels.

① hi above plinth below 8 read .59 (Taken as zero)

Batter above 6 = out .16 down .87

Batter above 5 = out .39 down .87

9 read down -0.88 from ① (Lowest stone)
+ .59
-.29 -.29

7 read down -2.695 from ① (bottom stone)
+ .59
-2.105

② hi above 7 read 2.105
.08
-2.025

6 to front of terrace 1.85 (+) and down about ~~.12'~~ cm. (Top course probably missing.)

7 to front of terrace 1.65 (+) and down .32'

6 read down -2.53 from ②
-2.025
-4.555

③ hi above 6 read -4.555
+0.32
-4.235

Face of stele above 11 = -3.87 from ④
-6.995
-10.865

.35 above top of cist.

5 read down -3.55 from ③
-4.235
-7.785

④ hi above 5 read 7.785
.79
-6.995

Plinth .20' deep in front of 8.

8 - 9 = 4.15 (+)

3 - 4 = 8.61 (+)

4 read down -6.995
-3.90 from ⑤ lowest stone
-10.895

3 read down -3.55 from ④ top of step.
-6.995
-10.945

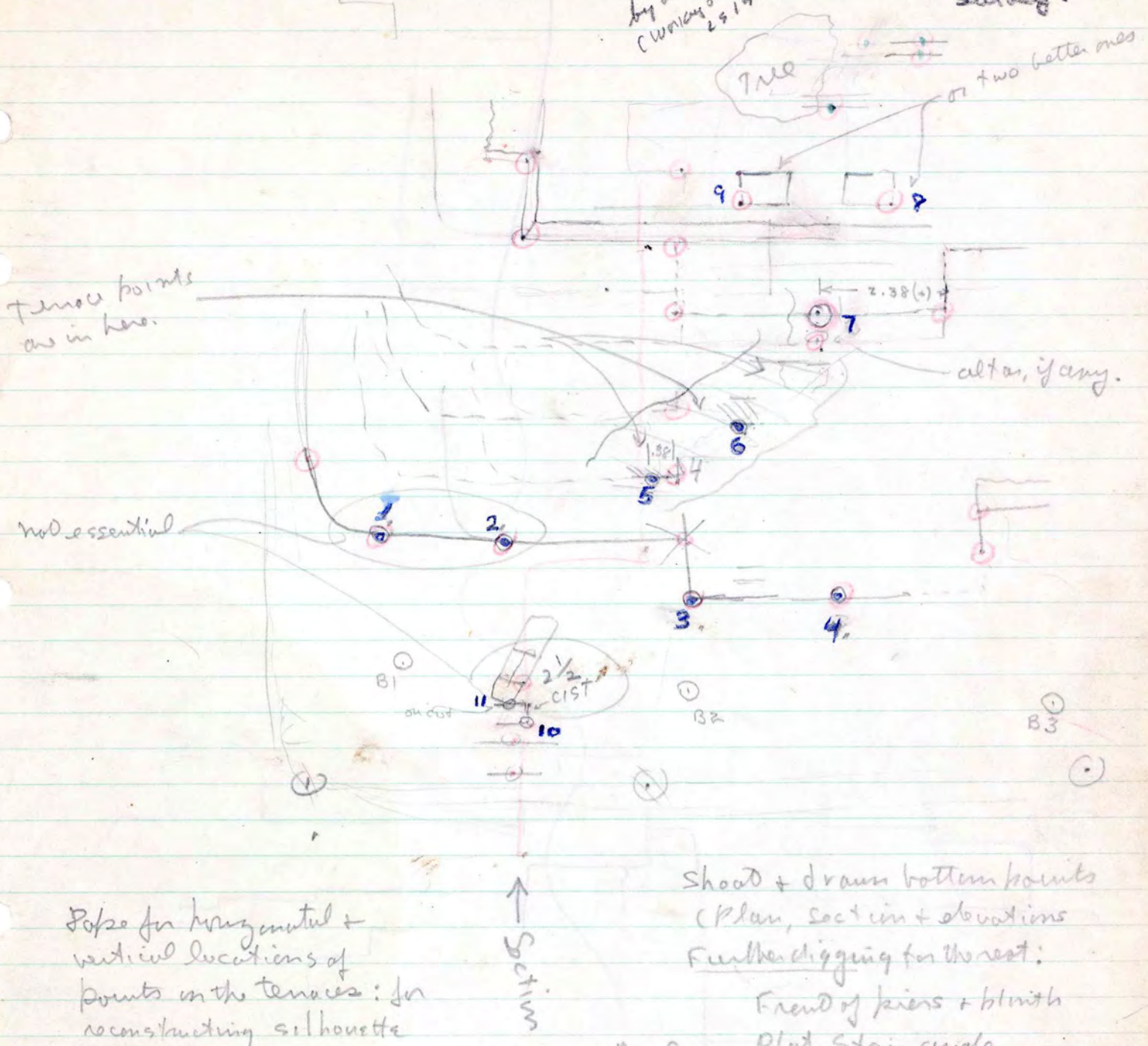
2 read down -4.04 above ⑤ lowest stone (above bed rock)
-6.995
-11.035

1 read down -3.93 from ④ level of ~~stone~~ point above bottom stone.
-6.995
-10.925

O-12 Survey Job

WSG 1940, LS
Illustr. sheet for survey.

Drawn up - the points, by WSG (working drawing) 2/5/1960



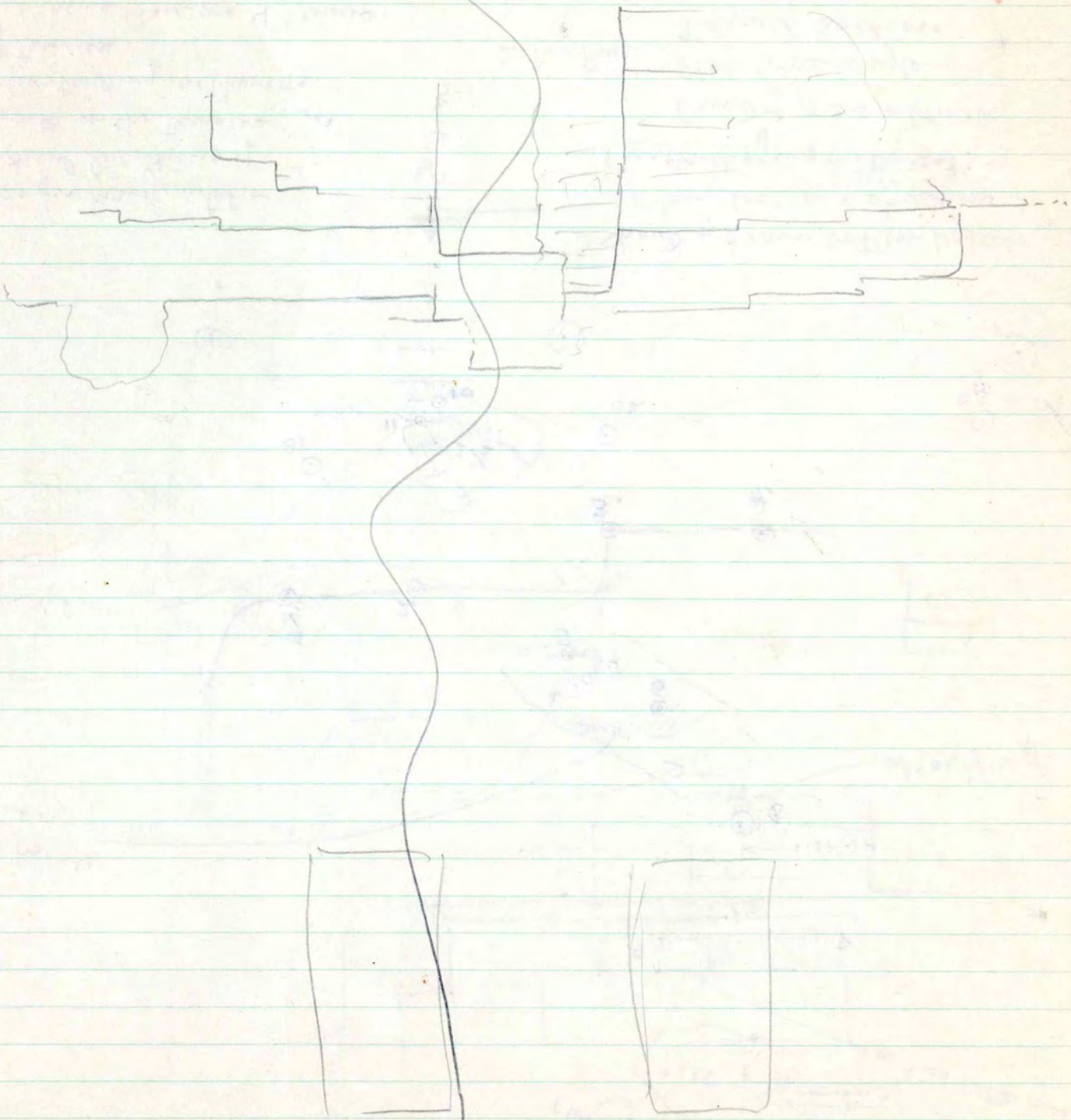
Poles for horizontal + vertical locations of points on the terraces: for reconstructing silhouette of terraces.
I think there are 4 terraces.
Don't waste much time on Rib #1: if not clear, put a red point on the wall and I will meas. down from it with Rufino later.

Shoot + draw bottom points (Plan, Section + elevations
Further digging for the rest:
Trend of joints + bluish Plat. Stain angle
Terrace Sections

2 New Pays.

For heights, include top of the step at (3) and then go on up (or come down to it) - I have heights of everything else to the bottom.

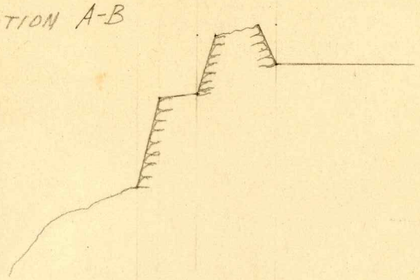
K-5- Pupa - K-5. 2nd Clean-up.

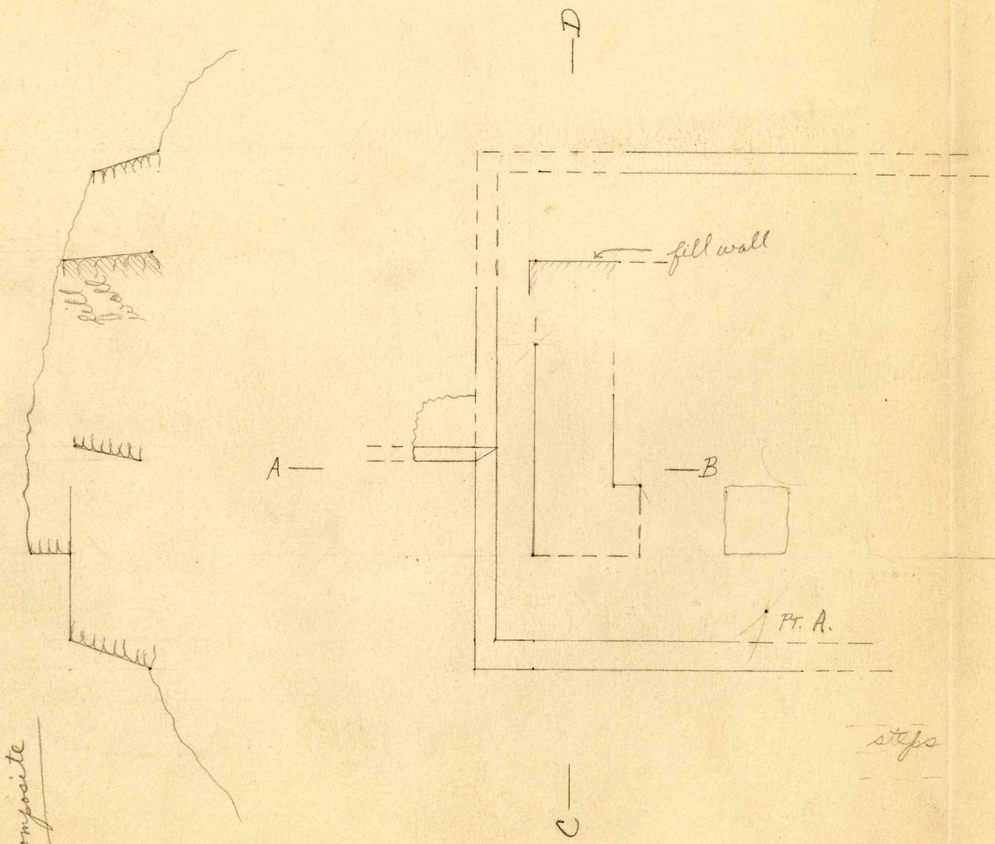


O-12
From 1936 notes
Scale 1:100
Rectified

hi = 1.03 above bottom of left rear corner of left pier.

SECTION A-B





hi = 1.03 above same zero point.

SECTION C-D
Composite

0-12

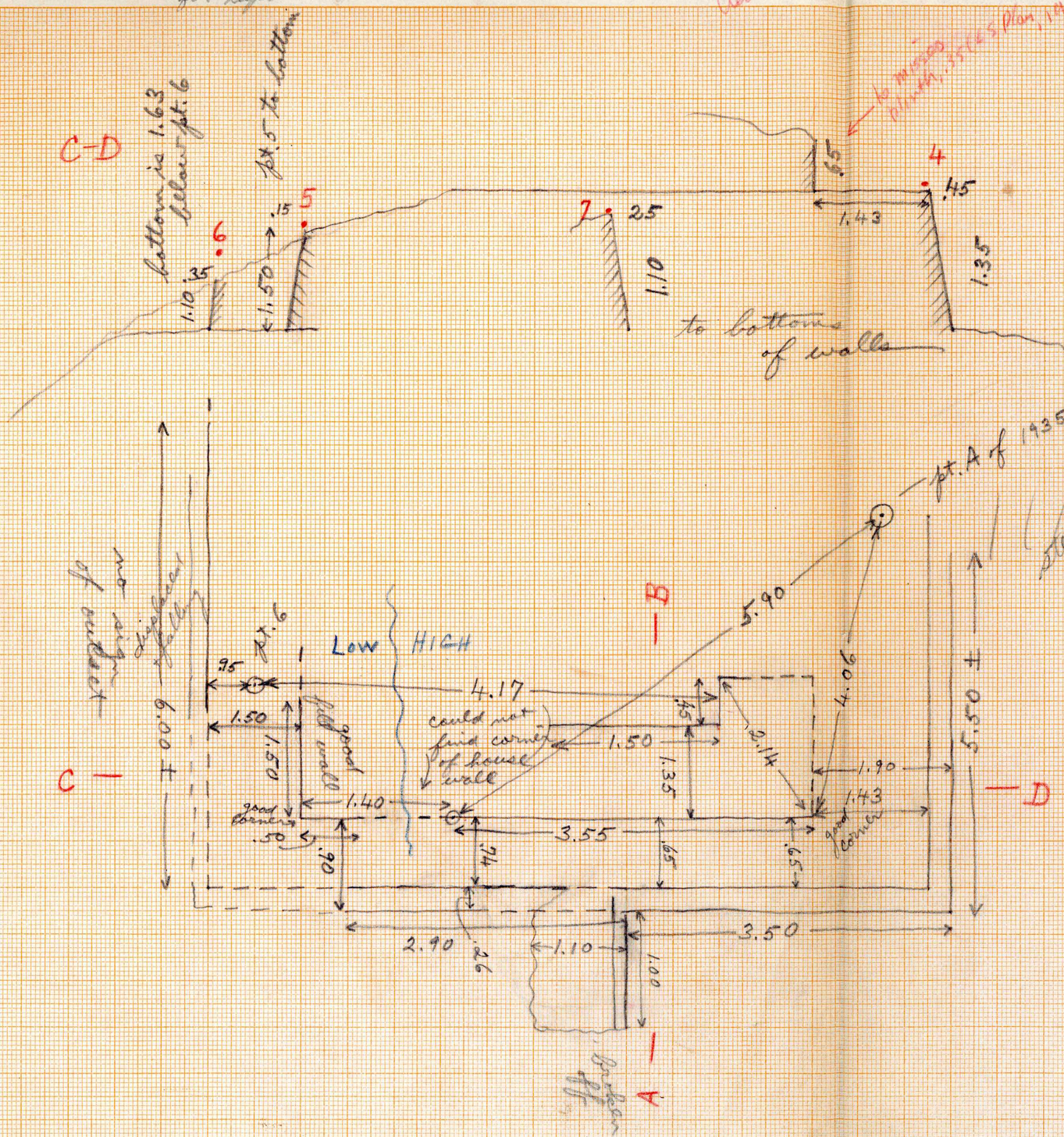
without correction for tape

4 small sq = 1.00

Caisson

0-12

6/19/36



$Z_1 = 1.03$

Z_i is height above bottom of left rear corner of left pier.

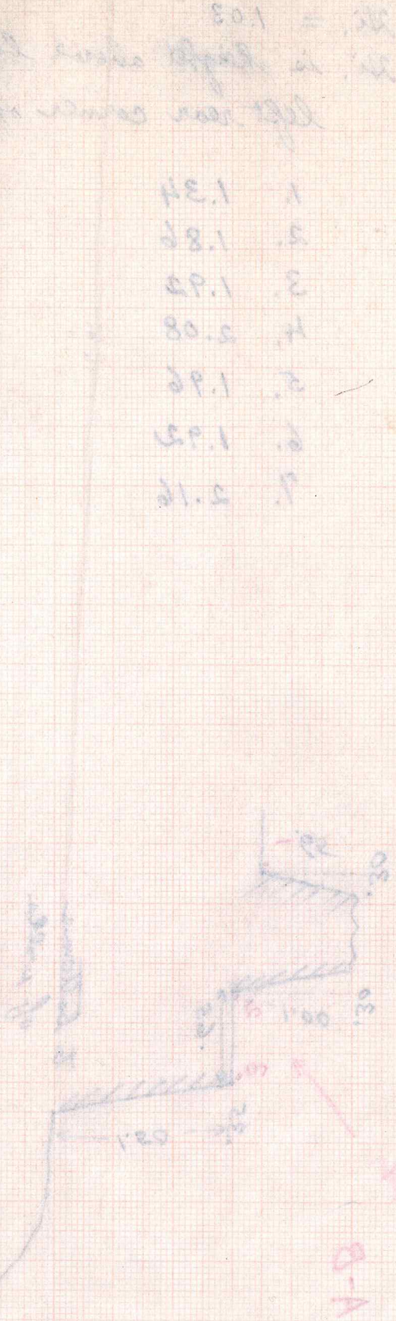
1.	1.34
2.	1.86
3.	1.92
4.	2.08
5.	1.96
6.	1.92
7.	2.16

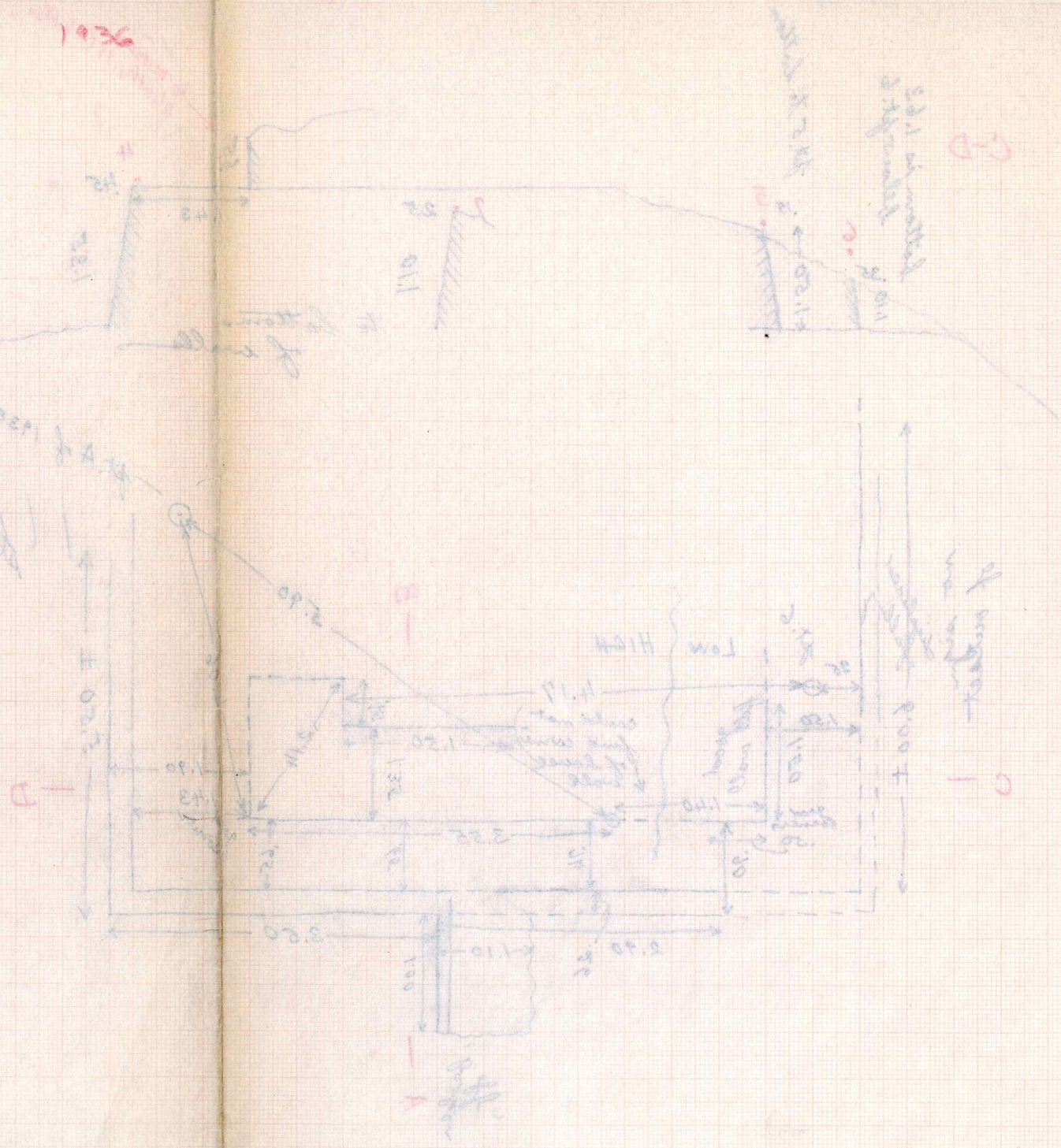
1.92
1.63
3.55

KEUFFEL & ESSER CO., N. Y. NO. 359-14L Millimeters.

012

1936





(h1 = 1.43 above pt. 5 (bottom of pier stone, left rear corner of left pier (pt. 7 on plan).
(1436 - not specified in 1935)

LS

0-12

1935

Read down

1	1.70
2	.55
3	1.17
4	1.41
5	1.43
6	1.37
7	1.72
8	1.62
9	.97

Bot. of pier stone

Ind. pt. 9.

out coat.

pt. 4 on plan

.35 plans

I

.20

.17

.09

.38

Loc the bld down (confirm.)

2 bolts in place, two following down.

nuts under pier as well as embossed in downward: Angel Floor

1.72

1.37

1.55

1.51 stone to width of bearing

1.67 to 1.63 bearing under pt 9 - pt 11 Si. Height. Good bearing surface.

1.63 to possibly 1.70±.

1.38, shroud 3 in 4 cms

1.33 - good masonry

1.51
1.47
1.33
4.31
1.23
1.40 (20 cm)
7.14

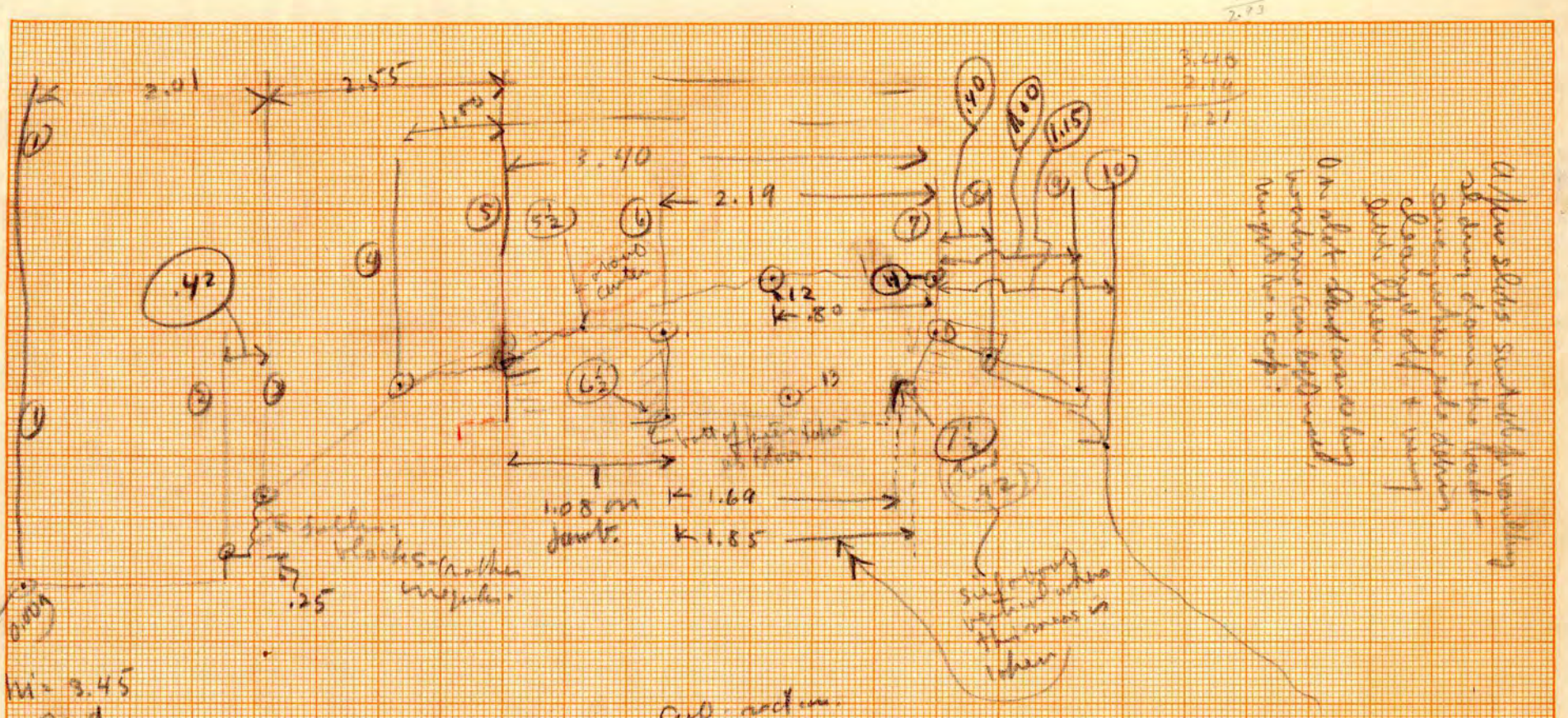
4.67
6.36
4.01

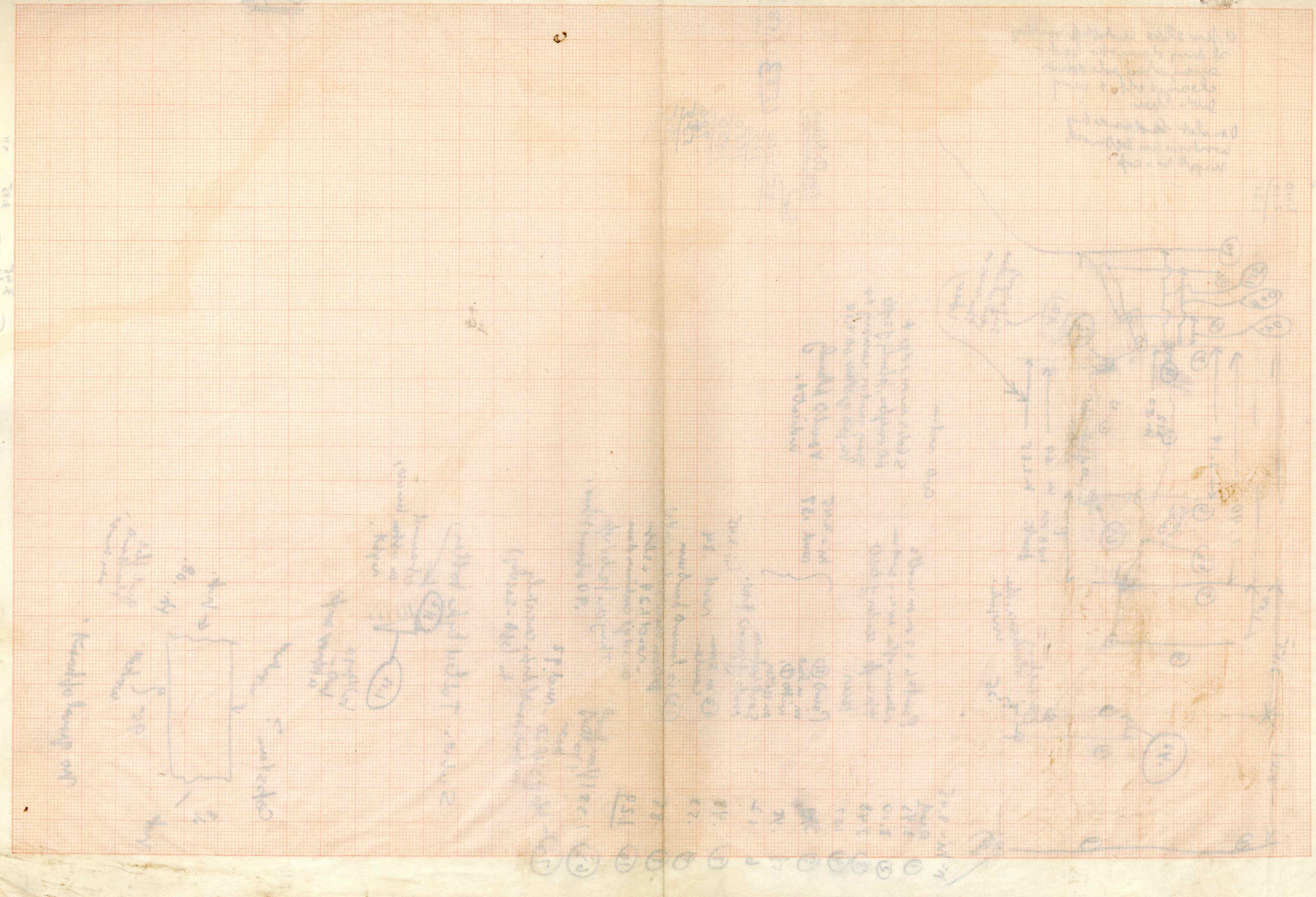
remarked corner on bottom left else many pairs below. Side is quite smooth. Top is fair but rough.

for pier

①	1.96 B;	4.61	4	1.13 ③	2.63 C														
②	2.49 B	4.80 A;	1.53 C																
③	1.79 B	5.32 A	2.28 C																
④	1.07 B	3.66 A	4.57 C																
⑤	4.04 B	5.18 A	1.49 C																
⑥	4.73 B	4.75 A	2.60 C																
⑦	2.94 B	3.80 A	2.58 C																
⑧	3.08 B	3.40 A	3.23 C																
⑨	2.38 B	2.85 A	3.70 C																
⑩	3.34 B	2.22 A																	
⑪	2.73 B	2.00 A	5.27 C																
⑫		2.10 A	6.31 C																
⑬		3.00 A	7.78 C																
⑭		3.37 A	8.24 C																
⑮	4.04 B		3.40 C																
⑯	4.50 B		2.85 C																
⑰	4.75 B;	1.50																	
⑱	4.32 B		1.69 C																
⑲	3.32 B		1.80 C																
⑳	2.34 B		4.26 C																

294 4 B





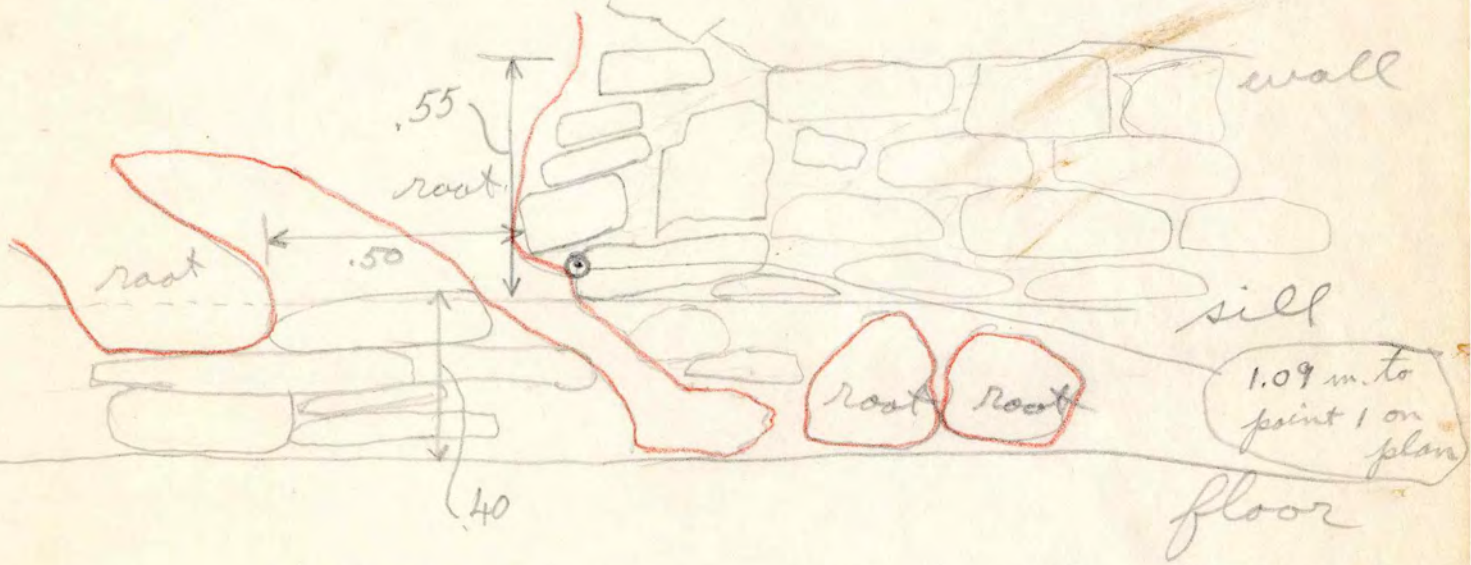
5/13/35

Piece of metate in room debris, directly under small tree. about .50 above floor, .80 to right of left side of central doorway + .90 back of front wall.

Debris here, in center of room, is about .90 deep. Made up of slabs, large + small, at various angles. Jammed tightly together with many large roots wedged between them. Slabs go all the way down to floor. Slabs are from about .03 to .09 thick. Disintegrated mortar last .10 or .20 above floor.

5/15/35

Niche in center of back wall.



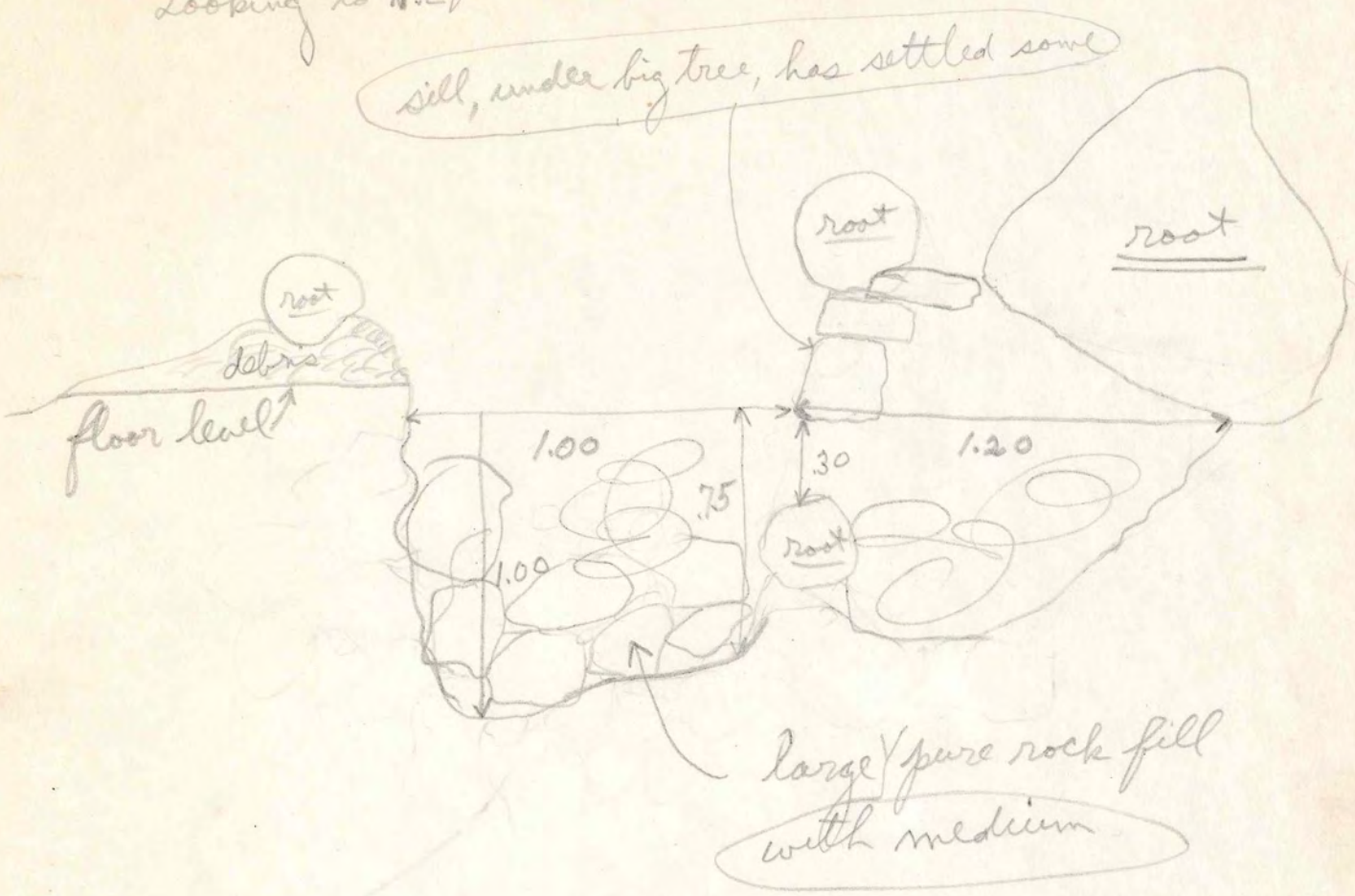
Five stones at front of left side of niche, three middle ones falling. all five have a well made corner + are worked on both sides of corner. Back of niche filled with roots. Right side covered with roots. Sill along bottom of niche.

Debris at front of niche, + going in .50 to where solid root begins was earth, small stones, + small slabs at various angles, like debris in room.

O-12

6/14/35

Section from front to rear thru central doorway + niche + hole dug in floor. Looking to N.E



O-12

Memo by J.A.M, Nov. 1933

O-12 (Old 25)

1 room. Max height walls 1 m. 3 entrances to front. Inside dimensions room 8 x 1.80. Walls 1.10 thick front, 1.50 sides and rear. Exterior dimensions 11 x 4.40, Sill 15 cm wide at rear 35 above floor. Central entrance 160 wide, side entrances 140 and 145. Piers between entrances 120 and 140 wide, walls at ends 45 and 50 long inside. Plinth 15-20 wide.

1.60
1.40
1.45
1.20
1.40
7.05

Pyramid XXV above stelae 22 and 23. 6-12 M

A large pyramid, numbered by Ricketson XXV, fronts on the east court opposite structure XXVI. At its foot are stelae 22 and 23 (photo 202) ~~(Maler, p. 68)~~. This is rather high and steep and crowned by a temple. The front faces the west. The rear (east) slope is steep and high, the side faces (north and south) also straight and but not so high or steep. The front or west face is more gentle, except near the top, and the lower slope consists of two platform terraces, as in the plan on figure (mss. 6/14).

The ground section is rectangular and practically square; the high pyramidal section is rectangular and oblong, the long axis of the pyramid and the temple being at right angles to that of the entire mound, the high section occupying the rear three-fifths of the mound. The ground is naturally sloping down from the south towards the north so that the north side is higher than the south. The terraces in front are also high at the north side, their north slope being a continuation of the slope of the pyramid, but to the south they blend with the natural slope of the ground. These terraces are naturally somewhat eroded with gullies and their slopes are now less regular and steep than formerly.

The maximum dimensions of this pyramid mound are about 37 by 39 meters; it faces about 65 degrees west of north (Brunton). The two terraces were probably originally about 5 m wide each, the slopes between them about 2.5 m. wide, but the erosion of years has made these measurements very uncertain. Stela 22 lies on the upper terrace near the north side while 23 lies nearer the front of the pyramid but considerable further out on the level floor of the court.

The steeper pyramid above the terraces measures about 32 m. along the front, the width of the slope of the terraces from this point north to the base being about 4.5 m. At the southwest corner the details of the pyramid are much better preserved, revealing the construction which was apparently in the form of stepped terraces, apparently four, narrow ones and then a broader one near the top about 2.30 m. below the present top of the walls of the temple. Apparently the te temple did not stand on this terrace, but another slope intervened. This broad terrace is not evident and apparently missing on the sides.

The temple on the top was almost entirely destroyed, excavation revealing one room with walls to a present maximim height of

1 m above the floor of the room. There are three entrances at (center of rear wall)
the front, none to sides or rear. The inside dimensions of this room are about 8 m. long by 1.80 m. wide. The thickness of the walls is about 150 cm to sides and rear, about 110 cm in front, making the total exterior dimensions about 11 by 4.40 m. Several immense trees are growing on the top, the roots of which obstructed much of the temple. At a height of about 35 cm above the floor, a narrow ledge or sill about 15 cm wide at the rear further lessened the width of the room and increased the thickness of the walls. The central entrance is 160 cm. wide, the side entrances 140 and 145 cm. The front walls at either end are 45 and 50 cm long, and the two pilasters between the entrances 120 and 140 cm wide,

On the outer wall there is a ledge 15 to 20 cm wide which also forms the sill for the entrances and which makes the total thickness of the entrances 135 cm. A step below this is a narrow terrace and then a batter retaining wall in good state of preservation. The edge of this wall is about 125 cm out from the edge of the sill. A flight of stairs probably stood in front of all three entrances, but they have been almost entirely disrupted, and in front of the northern entrance have entirely fallen away, leaving the

retaining wall straight and vertical.

The slopes of the pyramid and the surface at the base were examined and excavated in search of possible lintels which may have fallen from these doorways, but no trace of any was found. Probably they consisted of wooden beams.

No additional observations were made upon stelae 22 and 23 (Maler, p. 66).

(Extra data to add)

The floor of the terrace at the base of the steps was well plastered, and the lowest tier of steps showed well in places, this naturally being the part first covered by debris. There ware apparently no terraces on the pyramid at sides or back. Thw width of the pyramid at the upper terrace was about 18 m. The stairs on the right side apparently begin apparently at about 2.50 m from the edge. At the left side everything is much destroyed, and there is a wall 1.60 m high below and in front of the left entrance and above the upper terrace, the level of which is much destroyed here. But since there are stairs in front of the right entrance, it is likely that they formerly existed in front of the left also, now fallen and revealing the wall against which they were built.

N

South Court and Southern Section.

(See Satterthwaite)

With the exception of the ballcourt which lies between the southern and eastern groups no excavation was done in the southern or older section of the city. In this part lie stelae 24 to 37, (Maler pp. 66-74, plates XXII-XXIX; photos 40), and 42, altar 6 and lintel 4 (Maler p. 71, 72, plate XXXII). The magnificent glyph stela 36 (photo 40), was boxed for transportation to Guatemala (photos 200, 201). Search was made for lintel 6 which Maler states (page 75, figure 36) was taken from one of the temples and used as a table in the ~~monteria~~ principal house of the monteria or wood-cutting establishment which was there in 1895. One of the workmen found this after considerable search. It measures 124 by 134 cm and is very thin, 9 to 10 cm thick.(photo 140). In the center is a rather small and insignificant incised design of intricate maze design composed of three lines, one of them a circle, the others forming the main design. This measures about 50 cm in maximum width. In this general region is probably another altar, one support of which was removed by Emilio Palma, the chief of th monteria, and carried to Carmen (Maler p. 64, plr XI), but search failed to discover this.

Ruins near Guanal.

On June 19 a short trip was made to inspect some ruins on the west side of the Usumacinta. These lie about ten miles north of Tenosique and several hours ride west from the river at Guanal near the small settlements of Santa Maria and Tarenal on the telegraph line between Montecristo and Tenosique. A small number of figurines and other objects had been found in this neighborhood. A few mounds of about 6 to 12 m height were found there but no evidences of walls or edificies were seen. A few potsherds and lumps of pumice were the sole objects found.

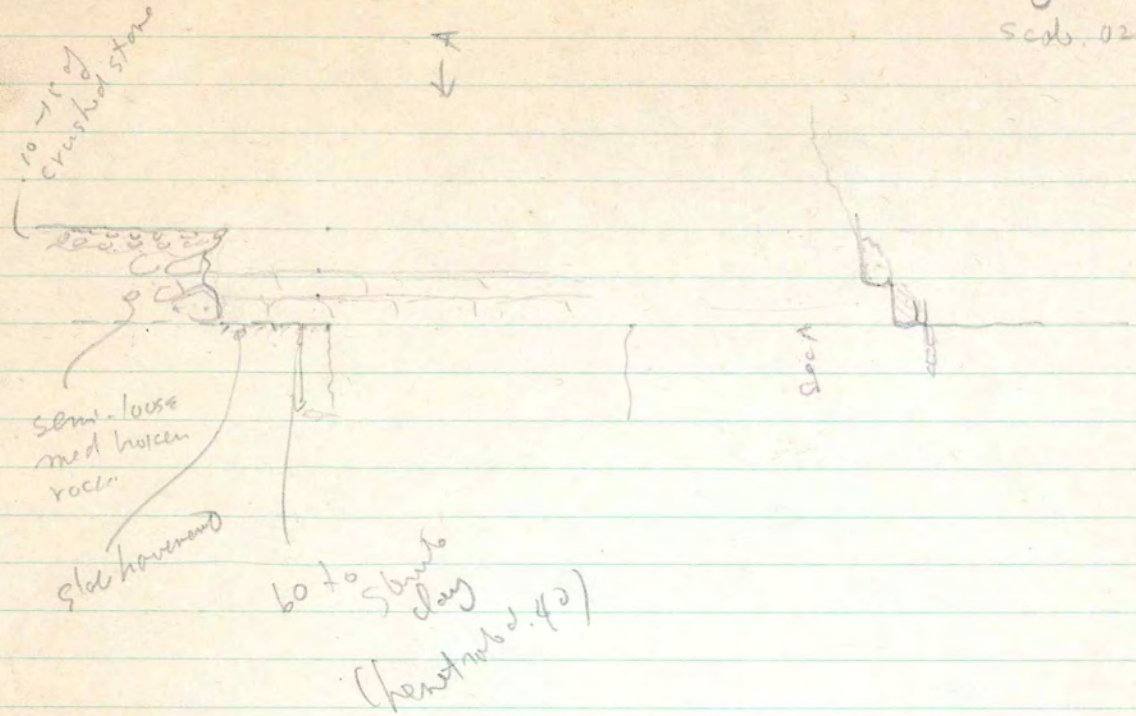
At the city of Jonuta, within the bounds of the pueblo, at the beginning of the delta of the Usumacinta and close to the bank of the Rio Jonuta, several large mounds can be plainly seen, rising above the low level land. Thelargest of these has been made into a municipal park with a terrace on the top and ascending stairs. Pls. 34 a, 35 a.

This is about 16 m in height, rather steep and abrupt, and consists of a central high pyramid with a broader terrace base at about mid height. This terrace is rectangular and probably square, the upper pyramid square or conical. At present there are no evidences of a structure on top; possibly it was a riverbank watchtower. There are also smaller mounds nearby in the village, some with houses built on them and some cut through by streets. These were probably house mounds. In one of the mounds cut through by a street, a plaster floor level was plainly seen.

A few potsherds were found on the surface of the large mounds, but in the cuts and erosions at the foot of the smaller mounds great quantities of potsherds were found, massed together. These are mainly of fine thin ware, some thick but none coarse, mainly bright red but some polished black, the fine red and fine black ware close together. Almost all are plain, a few with incised designs, several with black paint but none polychrome. The shapes are variant, with tripod or annular bases, but without handles. Study these sherds more in detail.

E. group

Pt in E. group
Plaza – (Ob. E-9).
Scale. 02 = 1.0



Str. O-13.

See Large Series of Drawings (to be Examined).

Folder of Collected Data + L.S. Notes.

Enveloped of Sam Extracts. etc. in 208:1-

Plain Lintel (?)
structure #1 – 0-14
Notes, 5/28/31

flat on both sides, upper (as found) (probably as placed) quite rough & eroded, under fairly smooth.

plaster adhering to under side as indicated, on all sides to about .05 from edge, except upper edge as shown here, where it is .12 from edge.

Thickness .12 ± all over.

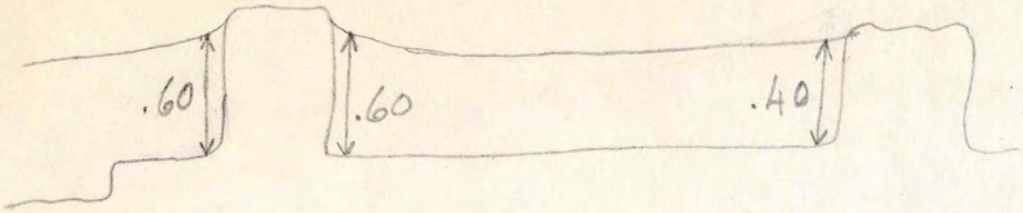
No working of edges into rounded effect of #5.

Fully exposed on surface, top edge about 1.25 below highest point of pyramid, facing SW toward ravine

Big thin slab half its side had to be moved to lift it, gent loose debris underneath.

lay lengthwise on slope. If you go any higher there is room for only one doorway.

cross section of debris thru right (S.E.) side of left (N.W.) doorway. Looking to S.E.

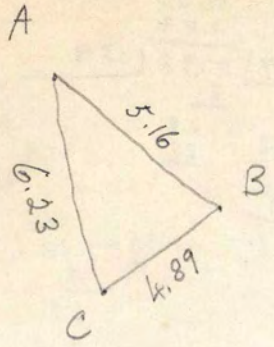


Did not contain typical large flat vault slabs but smaller stones + slabs as from walls. Loose dark humous soil gols all the way to floor level + there is no light tan colored disintigrated mortar. all this indicates a non-vaulted building, especially the shallowness of debris.

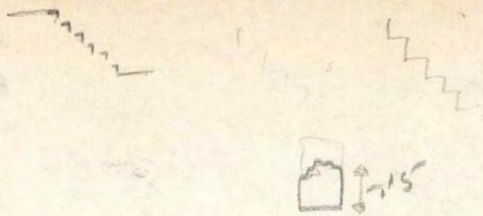
Small slabs found in wall debris at E. + N. corners of building

O-15

6/18/35



Point	From A	From B	From C	
1		2.97	2.39	
3		3.61	1.95	
4		2.09	3.18	
9	4.44	1.50		
10	3.97		4.35	
12	3.89		6.31	
13	2.32	3.25	6.09	
14		3.00	4.88	
15	1.11	5.48		
16	1.02			3.29 from pt. 13
19	2.68		5.87	
20	1.90		5.09	
25	2.94	2.50	4.08	
26	3.58	2.58	3.21	
31	5.85		6.23	
32	5.12		6.65	



4.30
1.92
7 | 2.38 | 34
21
28
28

1.03
1.80
-
~~2~~3 187
1.83 183
+4

1.02
85

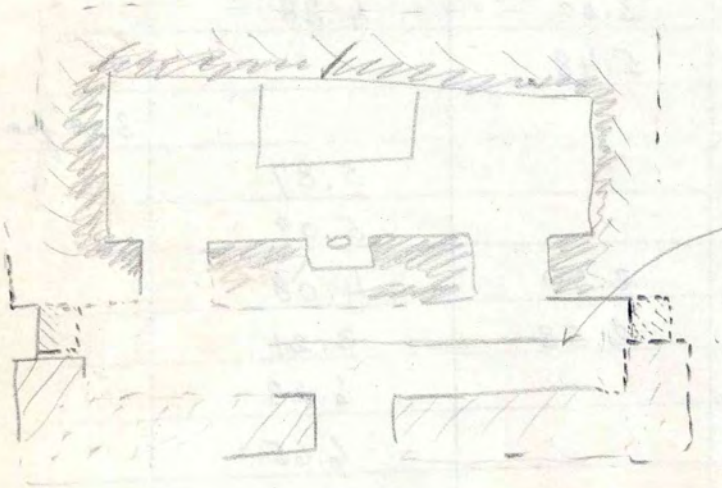
25

2 | 1.38 | 19
7
6.8
6

Sec. - nuchi vatten.
stelpa - hakan lino
- nuens .25

187
1.62
25

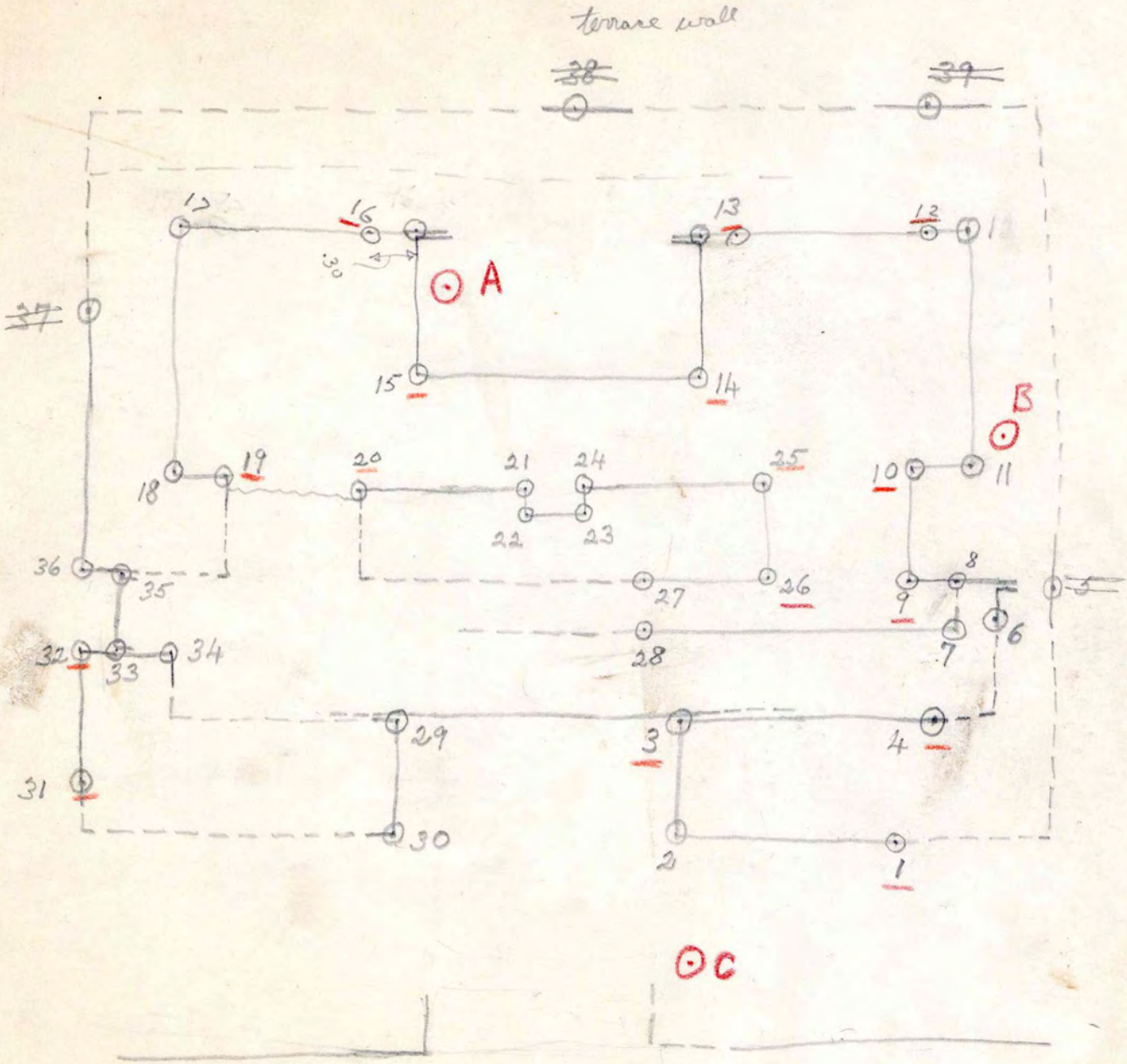
25

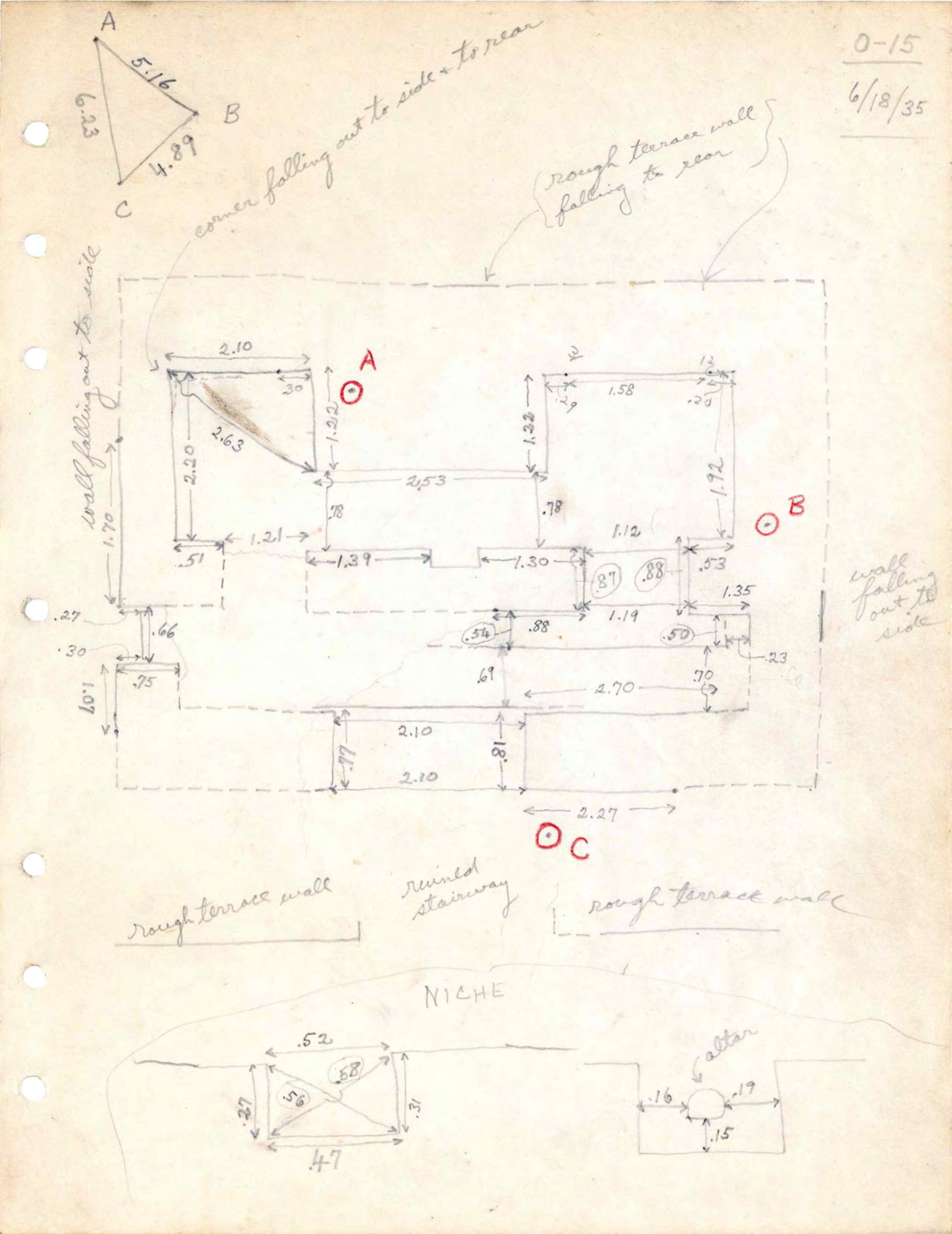


??

0-15

6/18/35


terrace wall
38
39
17
16
30
A
13
12
1
37
15
14
B
18
19
20
21
24
25
10
11
22
23
36
35
27
26
8
5
9
7
6
28
32
33
34
29
3
4
31
30
2
1
C

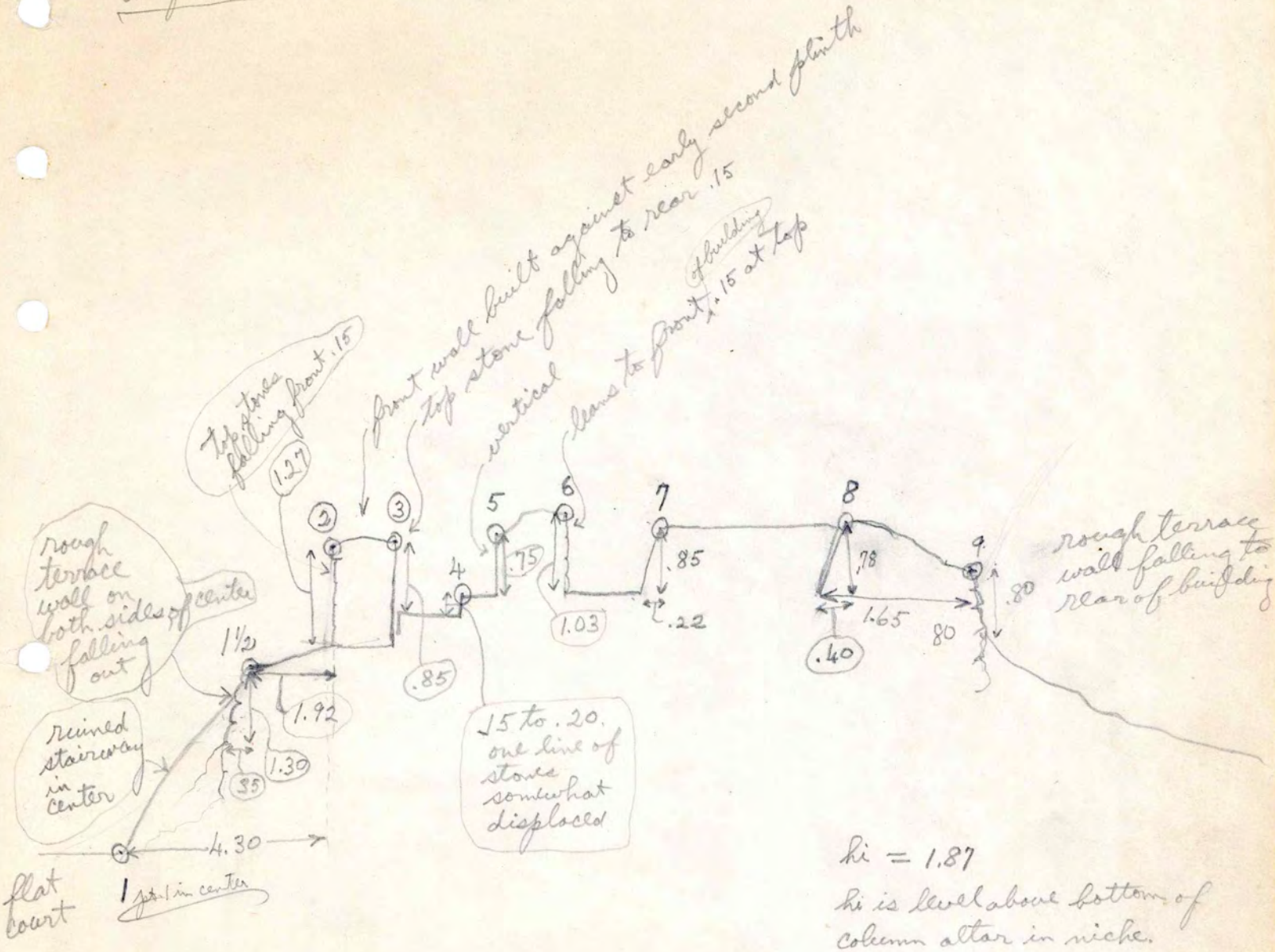

A
B
C
5.16
6.33
4.89
corner falling out to side + to rear
rough terrace wall falling to rear
wall falling out to side
2.10
.30
2.63
2.20
1.70
1.22
2.53
.78
1.21
.51
1.39
1.30
1.58
.29
.20
1.32
1.92
1.12
.53
.87
.88
1.35
1.19
.27
.66
.30
.75
.54
.88
.50
.23
.69
2.70
.70
10'1
2.10
.77
.81
2.10
2.27
A
B
C
wall falling out to side
rough terrace wall
ruined stairway
rough terrace wall
NICHE
.52
.58
.56
.27
.31
.47
altar
.16
.19
.15

0-15

6/18/35

6/18/35

Composite section

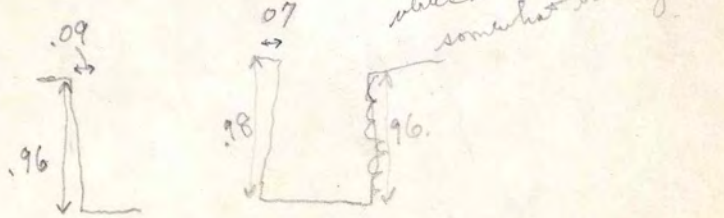


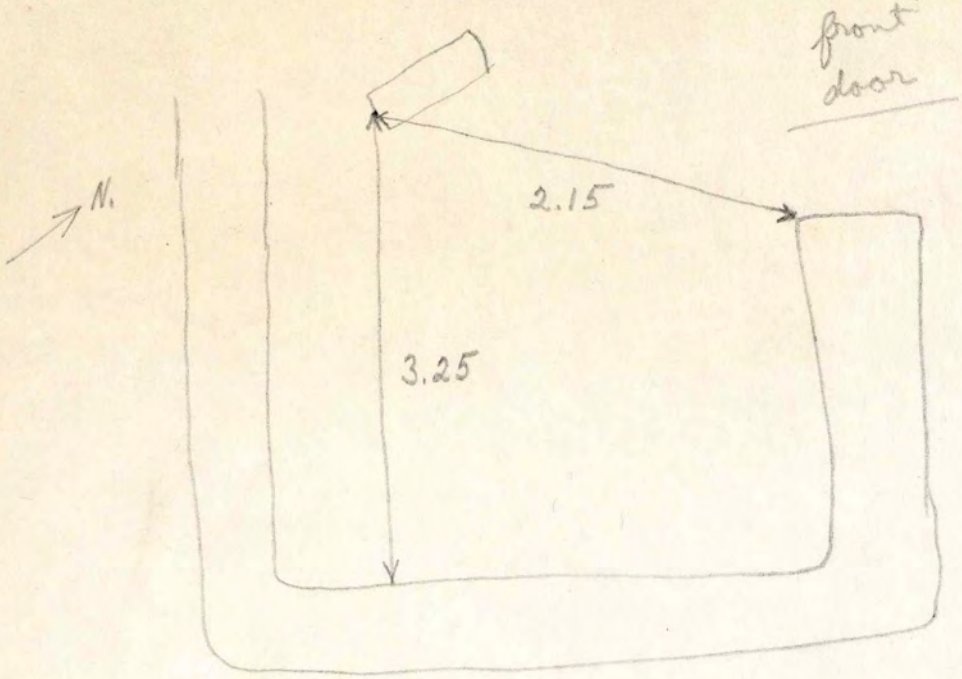
1	4.50
1½	2.50
2	1.13
3	1.14
4	1.79
5	1.10
6	.80
7	1.02
8	1.01
9	1.62

$h_i = 1.87$

h_i is level above bottom of column altar in niche.

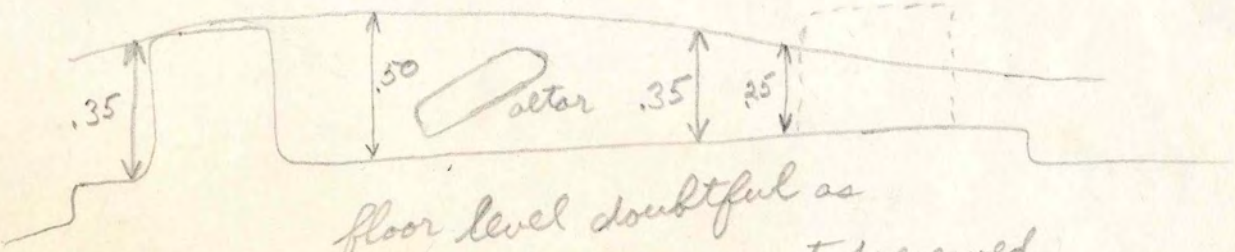
NICHE





Position of base of column altar as found.
May be a little above floor.

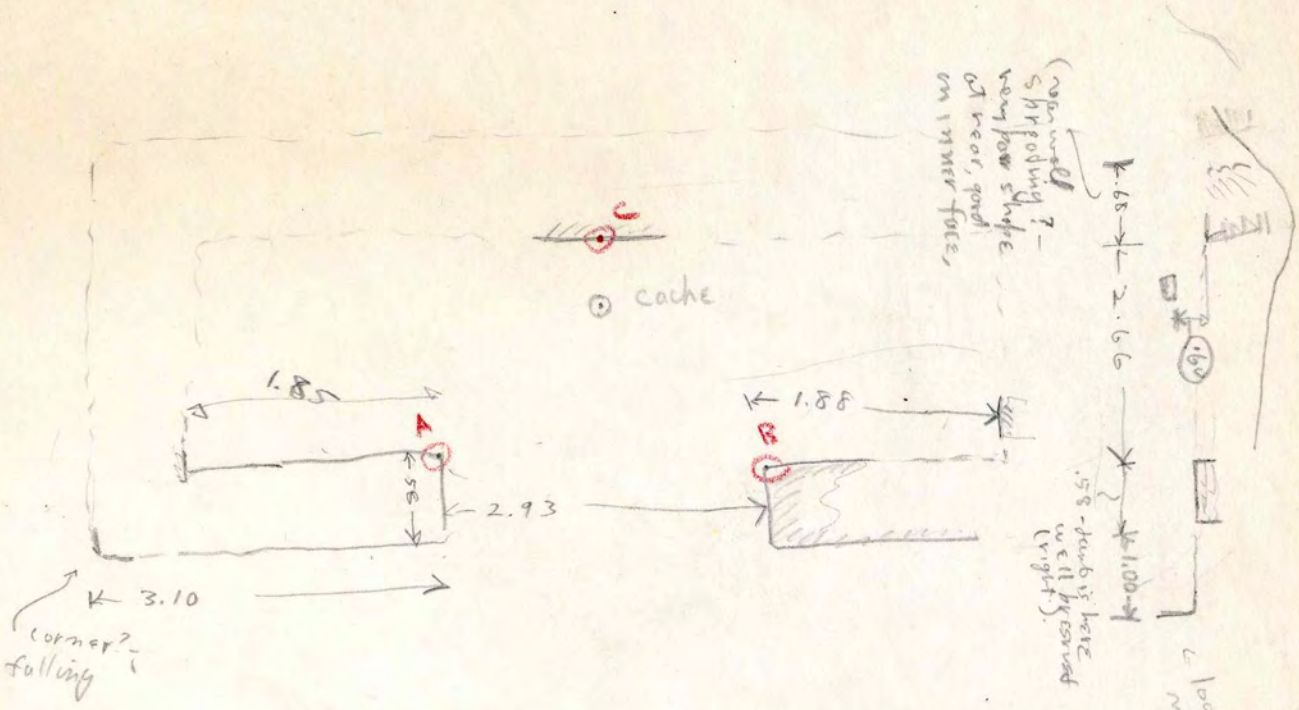
Cross section of debris thru column altar + front doorway. Looking to N.W.



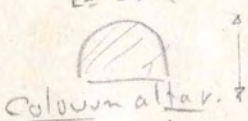
floor level doubtful as
floor surface was not preserved.
Room debris did not contain slabs.

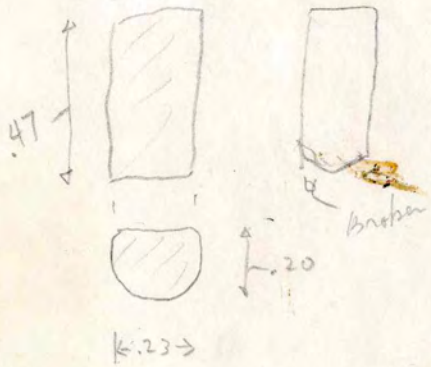
Pietras Negros 1935.

Str. O-16

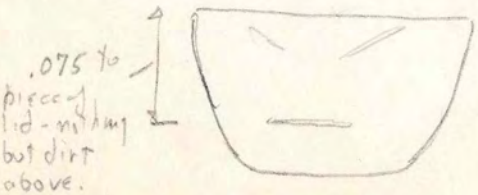


cache bowl – 2.40 from A (door jamb corner)
2.65 " B (" " ").
.58 from line of rear wall.



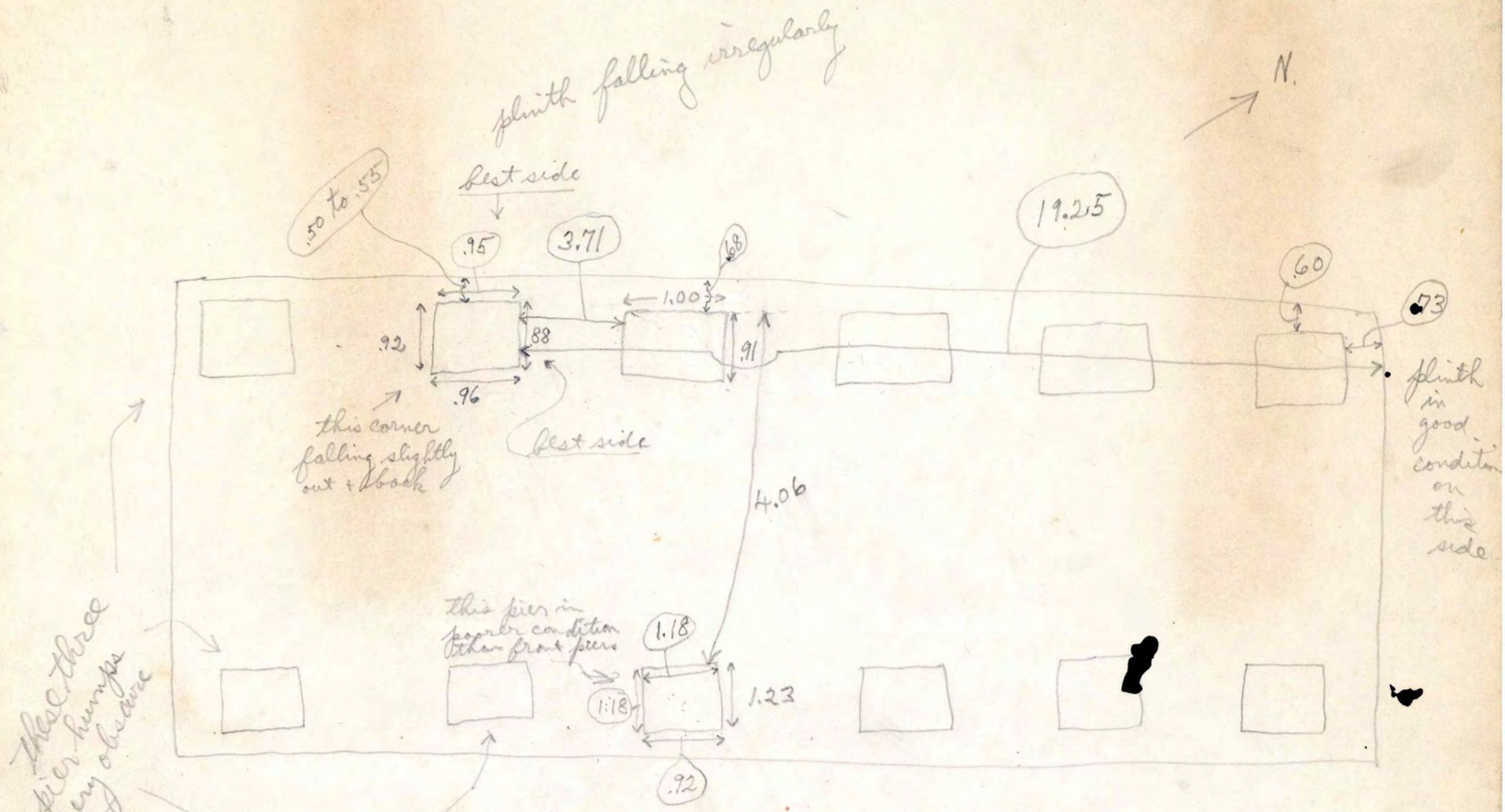


was well worked though mod very finely, probably; somewhat weathered.



Bird bones under pieces of lid.
Thin eccentric flint.

Jade was below flint
Bones go down + through tube
Obsidian on bottom (serrated)
few birds bones, top to bottom.
+ 2 pieces of "hematite"


plinth falling irregularly
N.
best side
.50 to .55
.95
3.71
.68
19.2.5
.60
.73
1.00
.92
.88
.91
.96
this corner falling slightly out + back
best side
4.06
plinth in good condition on this side
this pier in poorer condition than front piers
1.18
1.18
1.23
.92
these three pier humps very obscure
others fairly clear.
those to front, toward acropolis, are clearer.
From sill
4.06
- .91
3.15

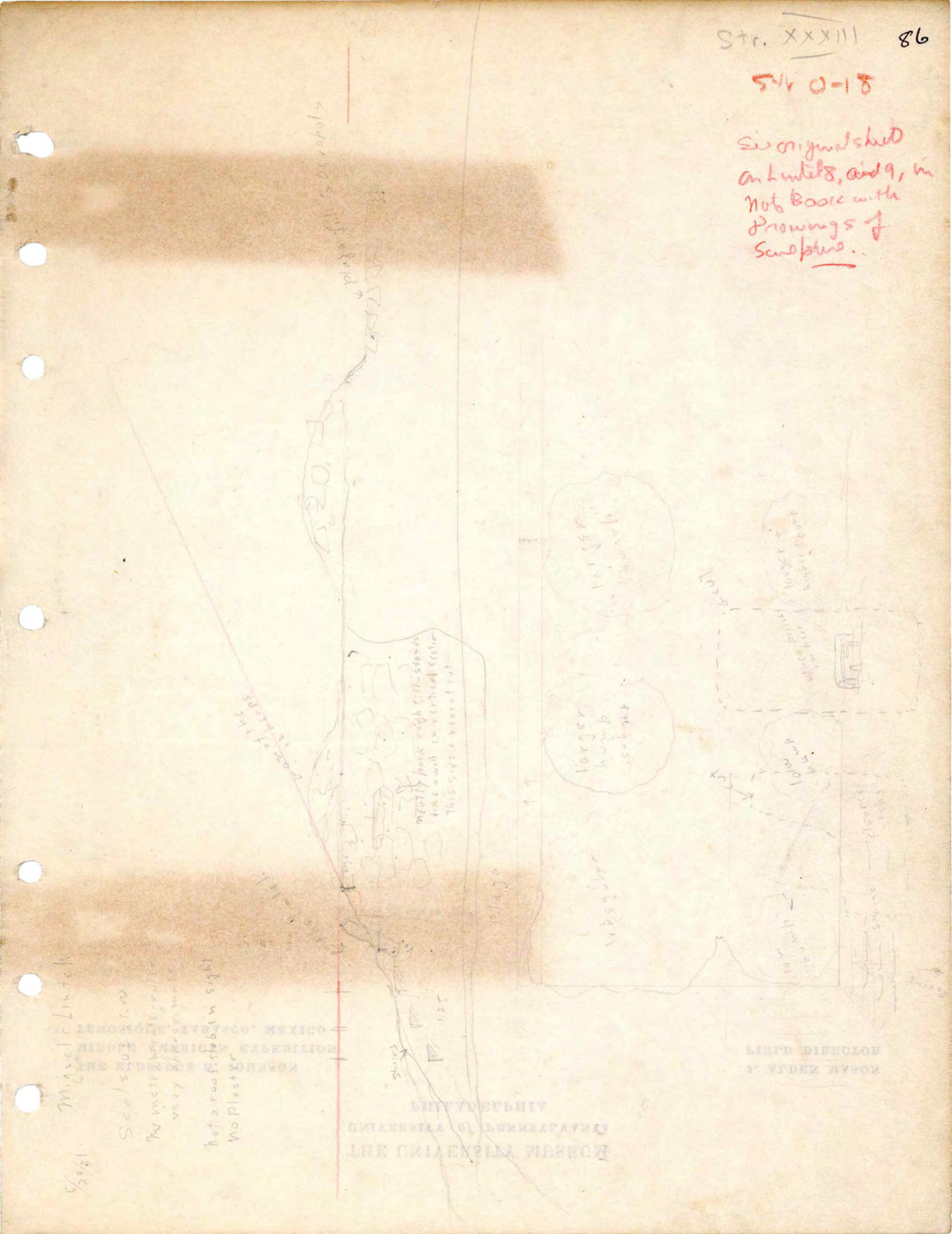
6/8/35

0-18

Str. XXXIII 86

S/4 0-18

Six originals
on Labels, and 9, in
Note Book with
Drawings of
Sculpture.



1940 Summary of Information on Sta. 0-18 (Old Sta. XXXIII)

Examined May 1938 by LS:
Found "Limit" ☒ ; and Limit ⊙ (now bgl - both on surface
Cut Section through both stations.
Rough plane Sedimil Scale 1:40 with rule only.
Gerson Mode Contain check. measurements, 1935.

LS in Motley 1938, III p21

Height of Mortarium above 0.50 (Humps of section scale 1:40 .35 + .50).
- humps, presently based on wooden posts?

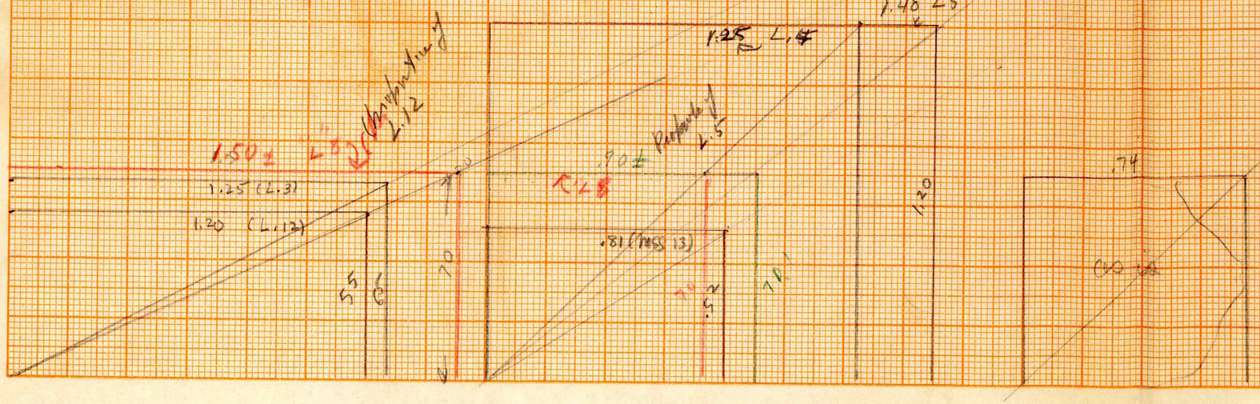
2 This is why these Gerson notes are 'obscure'

L. 8 - in tied "pub: city mile longer

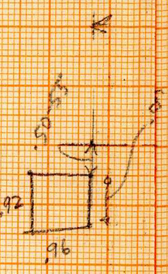
Limit 9 ▷ "turned in some part of fill
Connected by x-Head to Limit 8 fragment

Humps - Six rebbon E. the S. of Limit 5;
+ big Gerson -; 2 at mouth end.

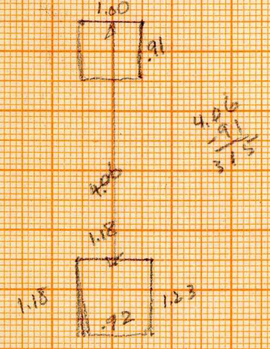
Limit 5. - Motley 1938. III p 204. Photo 1420.



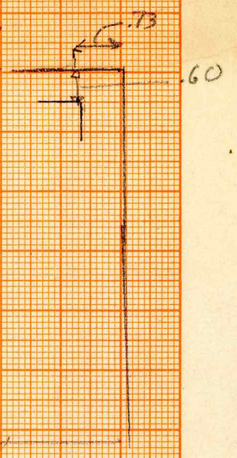
Gerson Measurements: 19.25



19.25



4 | 18.52 | 4.63 = av. for house + door.
-3.70 moved down
.92 for pair. face.
(Mouth of Door: .95 x 2.87 (96 27 18)
1.00
.92



Cross Section per Gession:

.50
4.06
1.23
(.50)
6.29 Called 6.30

4.06 / .91 = 3.15 the only 3 beam measurement

.05 off from a determined 6.30

Width:
50 plinth
.95 here
3.15
95
51
6.05

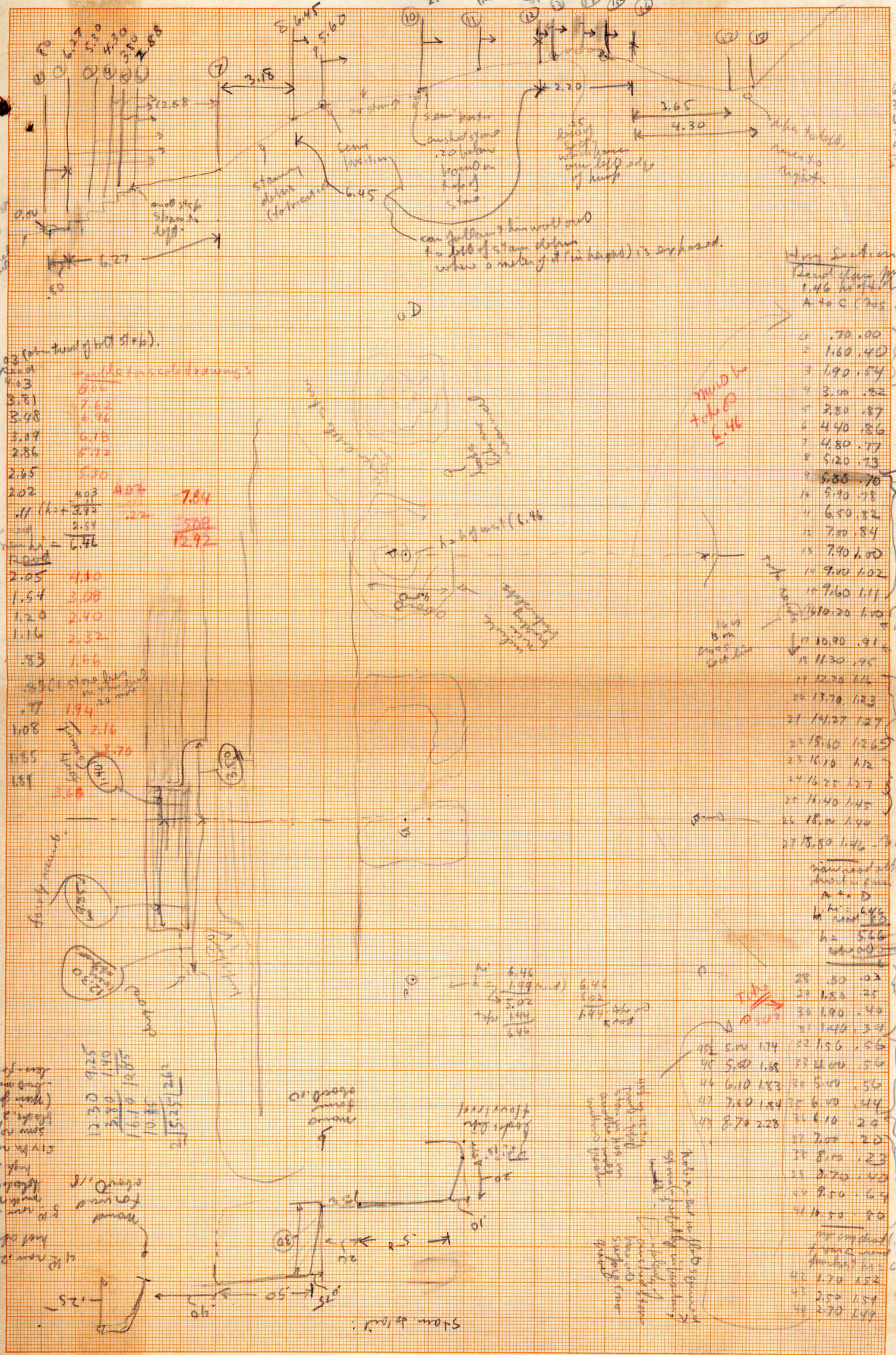
Bead Frame for Facets:
.95" for pivot hole
x4
3.80
4 | 14.72 | 3.68 call it 3.70.
12
27
24
32

Motto Piers .95
Doorway 3.70
4.65

6 piers: 95
6
5.70 5.70

5 doors @ 3.70
18.50
18.50
3 24.20
2 plinths @ .50 1.00
25.20 = scaling on Plan of Cotty.

This checks roughly with w. 16 LS sketch plan with rule only.


Stone drain
Sewer junction
Storm drain
Sewer manhole
Storm manhole
Catch basin
Gas line
Water line
Telephone manhole
Electric manhole
Fire hydrant
Gate valve
Curb inlet
Area drain
Footing drain
Roof leader
Cleanout
Bench mark
Property line
Building line
Edge of pavement
Curb
Fence
Tree
Shrub
Contour
Spot elevation
Flow line
Top of wall
Bottom of wall
Retaining wall
Concrete
Asphalt
Grass
Existing
Proposed
Demolish
Remove
Relocate
Abandon
Cut
Fill
Slope
Grade
Elevation
Station
Offset
Radius
Tangent
Chord
Bearing
Distance
Scale
North
Legend
Notes
Section
Detail
Plan
Profile
Elevation
Typical
Standard
Specification
Quantity
Unit
Total
Subtotal
Grand total
Contractor
Owner
Engineer
Architect
Surveyor
Date
Revision
Approved
Not approved
For review
For construction
As-built
Survey
Boundary
Easement
Right-of-way
Lot
Block
Subdivision
Zoning
Setback
Coverage
Density
Parking
Loading
Access
Egress
Circulation
Pedestrian
Vehicular
Bicycle
Transit
Utility
Water
Sewer
Storm
Gas
Electric
Telephone
Cable
Fiber optic
Overhead
Underground
Pole
Guy wire
Transformer
Meter
Valve
Hydrant
Backflow preventer
Pressure reducing valve
Flow rate
Pressure
Velocity
Capacity
Demand
Supply
Fixture unit
Pipe
Fitting
Coupling
Reducer
Elbow
Tee
Wye
Cap
Plug
Union
Flange
Gasket
Bolt
Nut
Washer
Thrust block
Anchor
Support
Hanger
Insulation
Heat trace
Freeze protection
Backfill
Bedding
Compaction
Trench
Excavation
Shoring
Dewatering
Erosion control
Silt fence
Straw bale
Inlet protection
Sediment basin
Detention
Retention
Infiltration
Permeable
Impervious
Runoff
Rainfall
Intensity
Duration
Frequency
Time of concentration
Rational method
Manning's equation
Hydraulic grade line
Energy grade line
Head loss
Friction factor
Roughness coefficient
Reynolds number
Laminar
Turbulent
Open channel
Closed conduit
Weir
Orifice
Spillway
Culvert
Bridge
Ford
Low water crossing
Floodplain
Floodway
Flood fringe
Base flood elevation
Freeboard
Levee
Dike
Berm
Swale
Ditch
Gutter
Curb and gutter
Sidewalk
Crosswalk
Ramp
Curb cut
Handicap ramp
Truncated domes
Bollard
Guardrail
Handrail
Stairs
Steps
Landing
Retaining wall
Gabion
Riprap
Geotextile
Geogrid
Soil nail
Tieback
Anchor
Micropile
Caisson
Pile
Footing
Foundation
Slab
Grade beam
Pier
Column
Beam
Girder
Joist
Truss
Deck
Roof
Parapet
Coping
Flashing
Waterproofing
Damp proofing
Vapor barrier
Insulation
Vapor retarder
Air barrier
Weather barrier
Rain screen
Curtain wall
Window
Door
Frame
Sill
Header
Jamb
Threshold
Lintel
Arch
Vault
Dome
Shell
Membrane
Tension structure
Cable
Strut
Tie
Node
Member
Connection
Weld
Bolt
Rivet
Pin
Hinge
Bearing
Expansion joint
Control joint
Construction joint
Isolation joint
Seismic joint
Settlement joint
Crack
Spall
Delamination
Corrosion
Rebar
Mesh
Prestressing
Post-tensioning
Tendon
Duct
Grout
Shotcrete
Formwork
Falsework
Shoring
Scaffold
Crane
Hoist
Rigging
Lift
Concrete pump
Batch plant
Mix design
Slump
Air entrainment
Admixture
Retarder
Accelerator
Plasticizer
Superplasticizer
Water reducer
Curing
Finishing
Troweling
Broom finish
Exposed aggregate
Stamped concrete
Colored concrete
Integral color
Surface hardener
Sealer
Joint filler
Joint sealant
Backer rod
Bond breaker
Primer
Adhesive
Epoxy
Grout
Mortar
Brick
Block
Stone
Veneer
Cladding
Panel
Siding
Shingle
Tile
Slate
Metal roofing
Membrane roofing
Built-up roofing
Modified bitumen
EPDM
TPO
PVC
Green roof
Skylight
Clerestory
Louver
Vent
Exhaust
Intake
Duct
Damper
Fan
Air handler
Heat exchanger
Boiler
Chiller
Cooling tower
Condenser
Evaporator
Compressor
Refrigerant
Piping
Insulation
Vapor barrier
Thermostat
Sensor
Actuator
Control valve
Variable frequency drive
Motor
Pump
Sump
Sump pump
Oil separator
Grease trap
Interceptor
Backflow preventer
Pressure reducing valve
Expansion tank
Pressure relief valve
Temperature relief valve
Vacuum breaker
Air gap
Cross connection
Potable water
Non-potable water
Reclaimed water
Irrigation
Sprinkler
Drip irrigation
Backflow preventer
Rain sensor
Soil moisture sensor
Controller
Zone valve
Quick coupler
Hose bib
Fire protection
Fire sprinkler
Fire hydrant
Fire department connection
Standpipe
Fire pump
Jockey pump
Diesel engine
Electric motor
Transfer switch
Generator
Uninterruptible power supply
Battery
Inverter
Rectifier
Switchgear
Panelboard
Circuit breaker
Fuse
Disconnect
Conduit
Wire
Cable
Grounding
Bonding
Lightning protection
Surge protection
Arc flash
Ground fault
Ground fault circuit interrupter
Arc fault circuit interrupter
Emergency power
Exit sign
Emergency lighting
Occupancy sensor
Daylight sensor
Dimmer
Switch
Receptacle
Outlet
Junction box
Pull box
Conduit body
Cable tray
Raceway
Busway
Transformer
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Phantom line
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Leader
Dimension line
Extension line
Arrowhead
Tick mark
Witness line
Datum
Grid
Coordinate
Origin
Benchmark
Control point
Monument
Property corner
Lot corner
Block corner
Subdivision corner
Section corner
Quarter corner
Meander line
Riparian
Wetland
Delineation
Mitigation
Habitat
Species
Endangered species
Threatened species
Critical habitat
Buffer
Setback
Easement
Right-of-way
Encroachment
Variance
Conditional use
Permit
Approval
Denial
Appeal
Hearing
Public comment
Notice
Posting
Publication
Mailing
Recording
Filing
Fee
Bond
Insurance
Indemnity
Liability
Warranty
Guarantee
Maintenance bond
Performance bond
Payment bond
Letter of credit
Escrow
Lien
Mechanic's lien
Stop notice
Claim
Dispute
Arbitration
Mediation
Litigation
Settlement
Release
Waiver
Subrogation
Contribution
Indemnification
Hold harmless
Force majeure
Act of God
Strike
Labor dispute
Delay
Extension of time
Liquidated damages
Penalty
Bonus
Incentive
Termination
Default
Cure
Notice of default
Notice of termination
Suspension
Resumption
Abandonment
Assignment
Subcontract
Subcontractor
Supplier
Vendor
Manufacturer
Fabricator
Installer
Erector
Inspector
Tester
Commissioning agent
Project manager
Superintendent
Foreman
Crew
Labor
Equipment
Tool
Material
Waste
Recycling
Salvage
Disposal
Landfill
Hazardous waste
Asbestos
Lead paint
PCB
Mold
Radon
Contaminated soil
Remediation
Abatement
Containment
Decontamination
Personal protective equipment
Safety
Hazard
Risk
Job hazard analysis
Toolbox talk
Safety meeting
Incident
Accident
Near miss
First aid
Medical
Emergency
Evacuation
Assembly point
Fire extinguisher
Spill kit
Material safety data sheet
Hazard communication
Training
Certification
Qualification
Competency
Supervision
Inspection
Audit
Corrective action
Preventive action
Root cause
Lessons learned
Best practice
Standard operating procedure
Work instruction
Checklist
Form
Log
Report
Record
Archive
Retention
Disposal
Confidentiality
Security
Access control
Badge
Key
Lock
Alarm
Surveillance
Camera
Intercom
Visitor
Escort
Restricted area
Clean room
Laboratory
Testing
Calibration
Measurement
Uncertainty
Accuracy
Precision
Resolution
Range
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Linearity
Hysteresis
Repeatability
Reproducibility
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Filter
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Data acquisition
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Telemetry
Wireless
Antenna
Satellite
GPS
GNSS
GIS
CAD
BIM
Model
Simulation
Visualization
Rendering
Animation
Virtual reality
Augmented reality
Mixed reality
Digital twin
Point cloud
Laser scanning
Photogrammetry
Drone
UAV
Aerial survey
Topographic survey
Boundary survey
As-built survey
Construction survey
Control survey
Geodetic survey
Leveling
Traverse
Triangulation
Trilateration
Resection
Intersection
Azimuth
Bearing
Distance
Angle
Coordinate system
Datum
Projection
Zone
Meridian
Parallel
Latitude
Longitude
Northing
Easting
Elevation
Height
Depth
Volume
Area
Perimeter
Slope
Grade
Aspect
Contour
Hillshade
Terrain
Watershed
Catchment
Drainage basin
Stream
River
Creek
Lake
Pond
Reservoir
Dam
Levee
Floodwall
Seawall
Revetment
Groin
Jetty
Breakwater
Pier
Wharf
Dock
Marina
Boat ramp
Navigation channel
Dredging
Spoil
Beach nourishment
Erosion
Sedimentation
Scour
Deposition
Littoral drift
Tide
Wave
Current
Salinity
Temperature
Dissolved oxygen
pH
Turbidity
Conductivity
Water quality
Monitoring
Sampling
Laboratory analysis
Chain of custody
Holding time
Preservation
Container
Label
Field blank
Duplicate
Spike
Recovery
Detection limit
Reporting limit
Quality assurance
Quality control
Data validation
Data review
Exceedance
Compliance
Permit
Discharge
Effluent
Influent
Outfall
Mixing zone
Dilution
Toxicity
Bioassay
Biomonitoring
Benthic
Plankton
Nekton
Macroinvertebrate
Fish
Amphibian
Reptile
Bird
Mammal
Vegetation
Riparian
Wetland
Upland
Forest
Grassland
Shrub
Tree
Canopy
Understory
Ground cover
Invasive species
Native species
Restoration
Revegetation
Planting
Seeding
Irrigation
Maintenance
Monitoring
Success criteria
Performance standard
Adaptive management
Contingency
Remediation
Abatement
Containment
Capping
Excavation
Disposal
Treatment
Bioremediation
Phytoremediation
Soil vapor extraction
Groundwater extraction
Air sparging
Permeable reactive barrier
Monitoring well
Piezometer
Observation well
Extraction well
Injection well
Recovery well
Aquifer
Groundwater
Vadose zone
Saturated zone
Water table
Hydraulic conductivity
Transmissivity
Storativity
Porosity
Permeability
Darcy's law
Flow net
Capture zone
Drawdown
Recharge
Discharge
Pumping test
Slug test
Tracer test
Dye test
Groundwater model
MODFLOW
Finite difference
Finite element
Boundary condition
Initial condition
Calibration
Sensitivity analysis
Uncertainty analysis
Scenario
Forecast
Prediction
Hindcast
Validation
Verification
Peer review
Quality assurance
Quality control
Documentation
Report
Memorandum
Letter
Email
Meeting minutes
Agenda
Action item
Decision
Issue
Risk
Opportunity
Mitigation
Contingency
Schedule
Milestone
Critical path
Float
Lag
Lead
Dependency
Resource
Budget
Cost
Earned value
Variance
Forecast
Progress
Percent complete
Status
Dashboard
Key performance indicator
Metric
Benchmark
Target
Threshold
Alert
Notification
Escalation
Resolution
Closure
Lessons learned
Archive
Retention
Disposal
Confidentiality
Security
Access control
Backup
Recovery
Disaster recovery
Business continuity
Redundancy
Failover
Uptime
Downtime
Maintenance window
Patch
Update
Upgrade
Version
Release
Deployment
Configuration
Change management
Incident management
Problem management
Service level agreement
Help desk
Ticket
Support
Training
Documentation
Knowledge base
FAQ
Tutorial
Video
Webinar
Conference
Workshop
Seminar
Presentation
Poster
Publication
Journal
Proceedings
Thesis
Dissertation
Patent
Trademark
Copyright
License
Open source
Proprietary
Software
Hardware
Firmware
Operating system
Application
Database
Server
Client
Network
Protocol
API
Interface
Integration
Middleware
Cloud
Virtualization
Container
Kubernetes
Docker
Microservice
Monolith
Architecture
Design pattern
Algorithm
Data structure
Programming language
Python
JavaScript
SQL
HTML
CSS
Framework
Library
Package
Dependency
Version control
Git
Repository
Branch
Merge
Commit
Pull request
Code review
Continuous integration
Continuous deployment
Testing
Unit test
Integration test
End-to-end test
Test coverage
Bug
Feature
Backlog
Sprint
Agile
Scrum
Kanban
Waterfall
DevOps
Infrastructure as code
Monitoring
Logging
Alerting
Dashboard
Metrics
Observability
Tracing
Profiling
Performance
Optimization
Caching
Load balancing
Scaling
Horizontal scaling
Vertical scaling
Auto scaling
Serverless
Function as a service
Platform as a service
Infrastructure as a service
Software as a service
Multi-tenancy
Single-tenancy
Data center
Edge computing
Content delivery network
DNS
Domain
Subdomain
URL
HTTP
HTTPS
TCP
IP
Port
Firewall
Intrusion detection
Intrusion prevention
Encryption
Decryption
Hashing
Digital signature
Certificate
Public key infrastructure
Authentication
Authorization
Single sign-on
Multi-factor authentication
Password
Token
Session
Cookie
Vulnerability
Penetration testing
Security audit
Compliance
Privacy
GDPR
HIPAA
SOC 2
ISO 27001
Risk assessment
Threat modeling
Incident response
Forensics
Backup
Recovery
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Redundancy
Failover
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Downtime
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Upgrade
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Problem management
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Firmware
Operating system
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Client
Network
Protocol
API
Interface
Integration
Middleware
Cloud
Virtualization
Container
Kubernetes
Docker
Microservice
Monolith
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Authorization
Single sign-on
Multi-factor authentication
Password
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Session
Cookie
Vulnerability
Penetration testing
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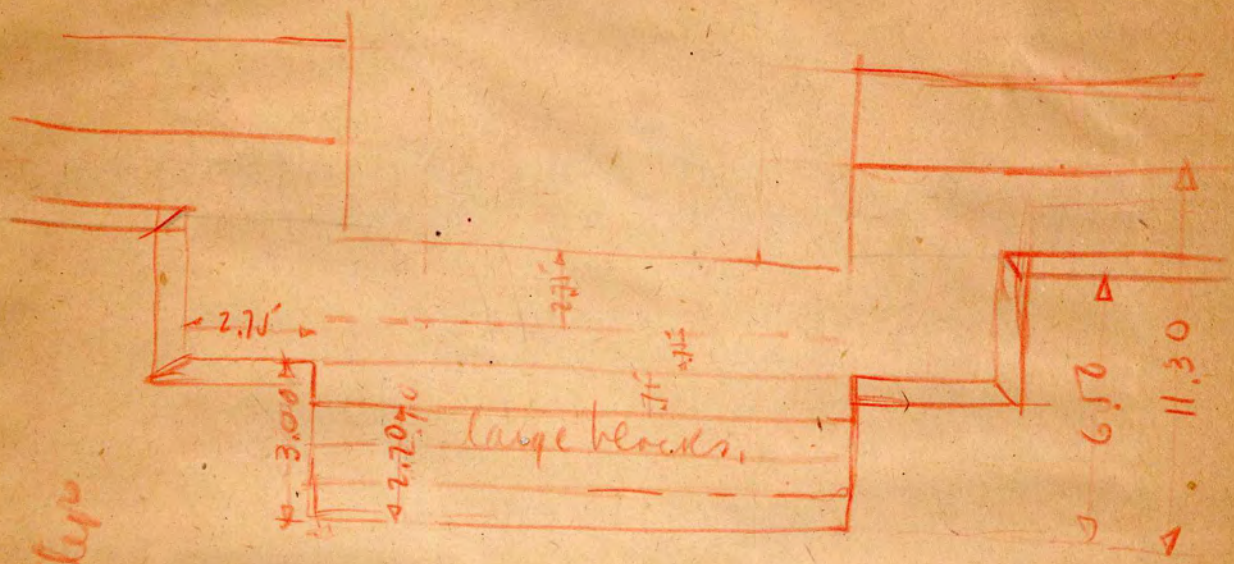
GDPR
HIPAA
SOC 2
ISO 27001
Risk assessment
Threat modeling
Incident response
Forensics

East group Megalithic Stairway

Str-P-6



average width/step
75 ± 1.00

Paris notes
1933

NB: these dimensions do not agree locally with LS careful section of 1934, which was subscribed in making up final drawings + text.

PM notes
from J a M Test.

Sand 3. S.11 in doorway.

+ b 14 This to be on the "-46" floor. would be ~~about~~ level of latest sean stone wall. Believe I am misled this on my say-so, for this reason. But TAP shows it in solid block.
Any mention of this sill in J. a. M. notes?
OK. – b 14 – decided from ups the blocks.

Sand 17 S.11 at entrance to tunnel this chamber, blanked by above.

Sherds Sand 17 Some sherds in final floor material in steamroom. ~~(illegible)~~

'18 Levelled cent. of this chamber

22 – Places Further jambs 20 below upper passage floor. – agreeing with my drawing.
TAP has jambs too long (visible bed?).
Places the sill between them.

22-3 Sill stones of this bed much fractured, probably by heat – between + here with them lying, bones, charcoal + ashy. 3 fine handled holy chun sherds found here.

sherds.

Quartz 23-4 Describes excavation of sherds.
2 or 3 fine (sand) holy chun.

24 – Paving slabs in this bed: all covered level ("Few" below base of jamb, sill and "lower" passage floor") to go with earlier Nine passage.

Lower heated slabs. 56 below steam room floor with "very good sill of 2 stones".
How thick? – i.e. what was the height of the lower sill?

Outer Ro

Outer Rooms - p. 39.

Front room bench. 48 x 48 x (1.70?). Plaster on front - doubt say it was seen top.

443 - notes 13 cm slope formed in front floor, rear room.

Objects. Flint knife on rear floor, left rear room (subsequently retrieved herein).

Pram - p 7

Chamber - p 9
- no plaster - p 10
depth of debris 50 to 120
many stones in debris

Bench - right rear: on floored floor + up blocked wall - p 45

as base 1.80 x 1.05 x .63 (Way: 1.95 x 1.10 x .60)
plaster traces on top (L.S. 1.76 x x .63) Error 61

Ave 1.80 x 1.07 x .60

screen .15 thick; min. height .50 (Way (?)
debris - rubble + much earth

left rear. - screen - "even less height" p 46.
tree in the way
1.85 x 1.20 x .59 (plaster top - p 49.
scree 20 cm. L.S. (x 1.12 x .59) (SW 14)
(x 1.10 - Error 04)

Obj: Flint knife - front of bench (left rear).

From Jamie notes.

Front Room bench. bench width, .48.

Redone

Memo re Str. P-7, Piedras Negras. (Aug. 1943). (By LSJr)

I have recetnly worked out the time sequences for this structure, apart from minor episodes which might be deducible form plaster layers. The earlier ones are drawn in isometric on sheet marked "1943 A". Lettered units are placed onthe drawings; some solid lines remain to be made broken, and other known areas may be added.

The seuqnces are:

P-7-5th-B	Units	ON (N not drawn)
-A		M (not drawn)
-4th		LKK'
-3d		JJ'II'H
~~2nd~~-B		GF rear level)
-A		(re-surfaced floor indicating higher/
~~1~~lst		EDCBA

P-7-5th-B N is a floor called "red" in the notes, known only at center. It is .07 or .08 below K and K'. The wall of O, at top, was .35 below K' nearby. While surface of O was not properly investigated, or at least recorded, it is too close to slope up to K'; correct for placement with N as top of a low (2.5 cm p~~l~~m platform, which is reconstructed on this basis.N shows turn-up and "hump" suggesting veru shallow plaster passage.

-A M is the "green" floor of the notes, which blanked the above supposed passage, hence suggests significant change.

P-7-4th L is a new basal platform and stwy; ~~xxxxxxxxxxxxxxxxxxxxxxxxxxxxxx~~ K and K' are a supposed building platform, with pe fectly certain remnants of passgae with stone walls. These are in line with that if I I', but notalways exactly. Low height is sure at right front corner.

P-7-3d JJ' encloses base of K almost certainly raising level in old passage; II' is new bldg. platform, built as a raising of the old one, but not coinciding exactly at right front corner, nor, at some points, in the passage. The fire-place arrangements of K were torn out, those of I built on the higher level corresponding to JJ'.The reoonstruction shows I as reaching full height of th4 later F; possibly it did not. A thick deposit of _____ resurfacecings belong in this and the next period, without rainsing the II' passage walls as here restored. H is remnant of outer Bldg. wall.

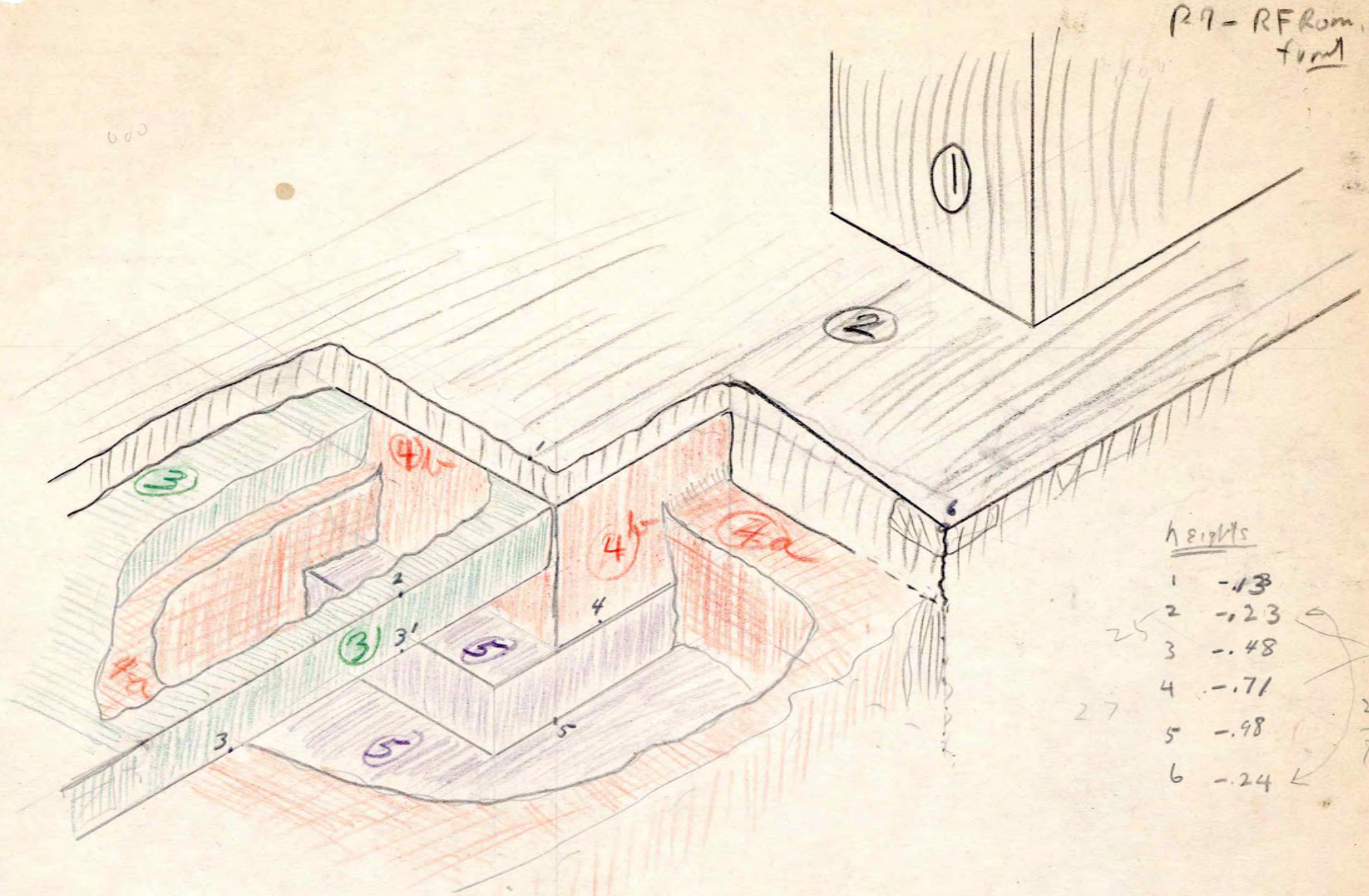
P-7-2nd-B G is known only by the remnant of wall G' indicated; no plsster or floor identifiedable.

FF' are quite certain extensions. Plaster turn-ups, not in line, are shown. Also wall remant, facing rear, indicated in plan. These prove that a new building, or at least addition, accompanied F'. (see below)

-A See notes, p 35-14. A resurefaced floor lay immediely under 2 cms of yeelow bedding for final rear wall which is at higher rear level. Hence a raisi g of the rear level ~~is~~ before the final period is sure, but it cannot be reconstruction. Very likeky this would be a full period, if enoguh was known. Yes - rear wall remants indicate new outer building

P-7-1st A is the building proper, B the steam room, D the new Building platform, ~~D a front step-terrace~~, E new front steps. E' steps terrace ?

P9 - RF Room, final



Heights

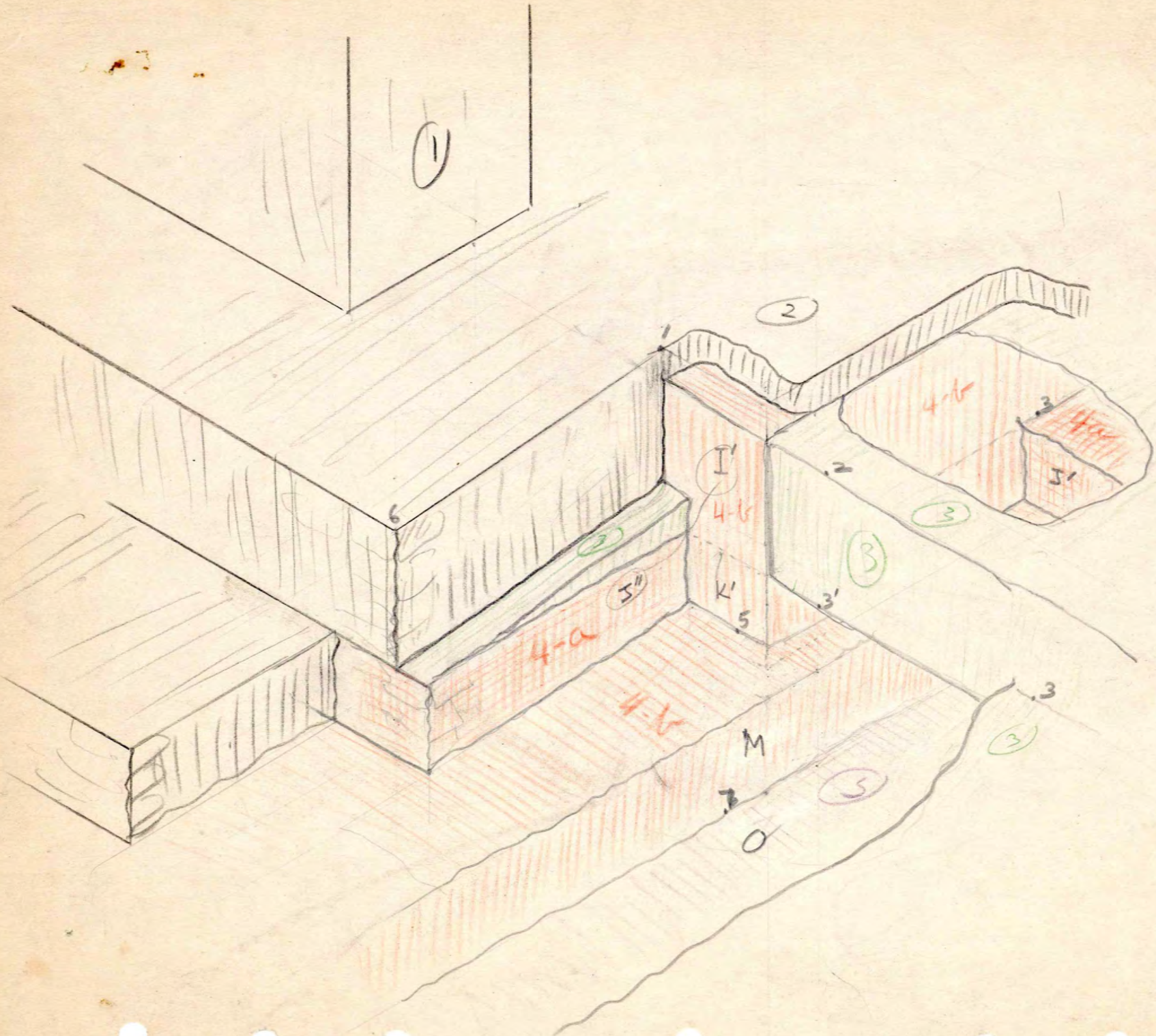
1	-.13
2	-.23
3	-.48
4	-.71
5	-.98
6	-.24

25 48 27 27 75

48 23 71

See p 35 - 6

15 23 48

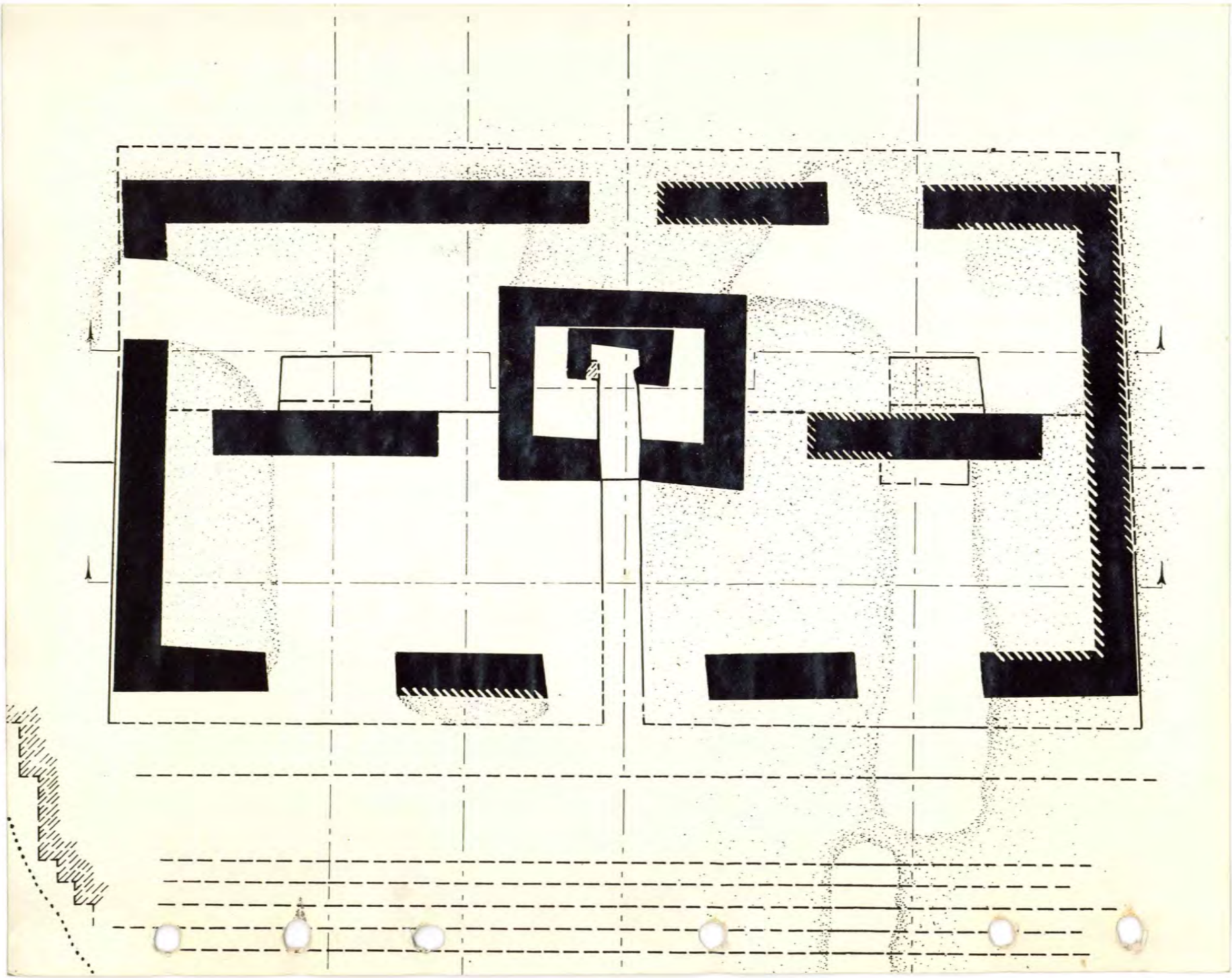


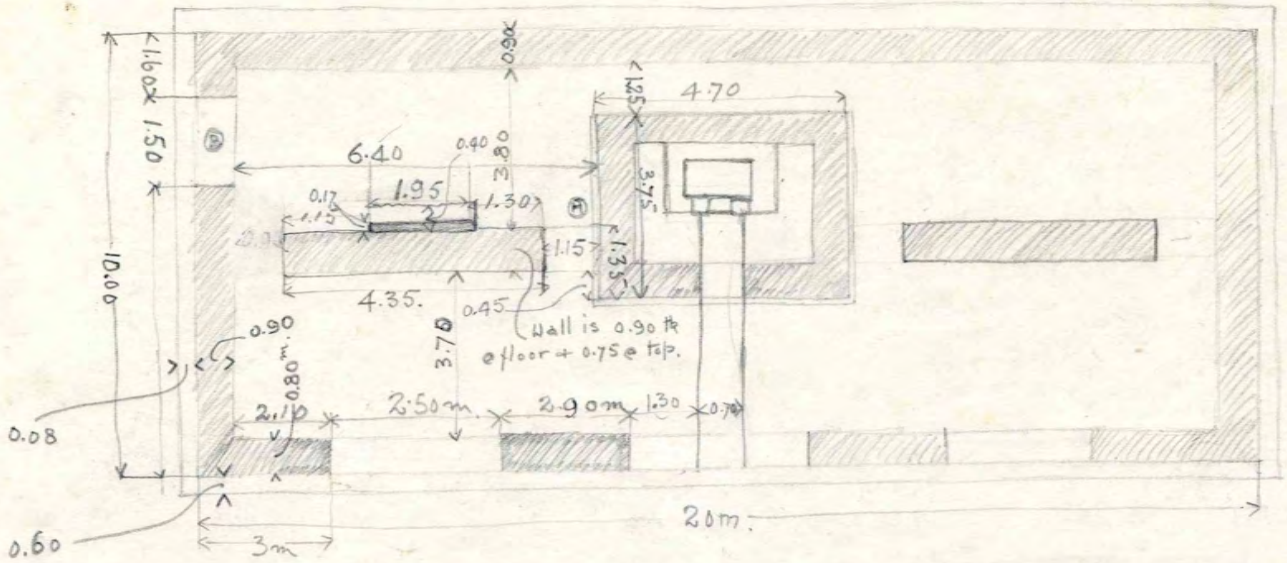
1 -.10
2 -.20
3 -.60
3' -.71
4 X
5 -1.01
6 -.20 calc.
7 -1.36

55-13

R 7

rear bld room





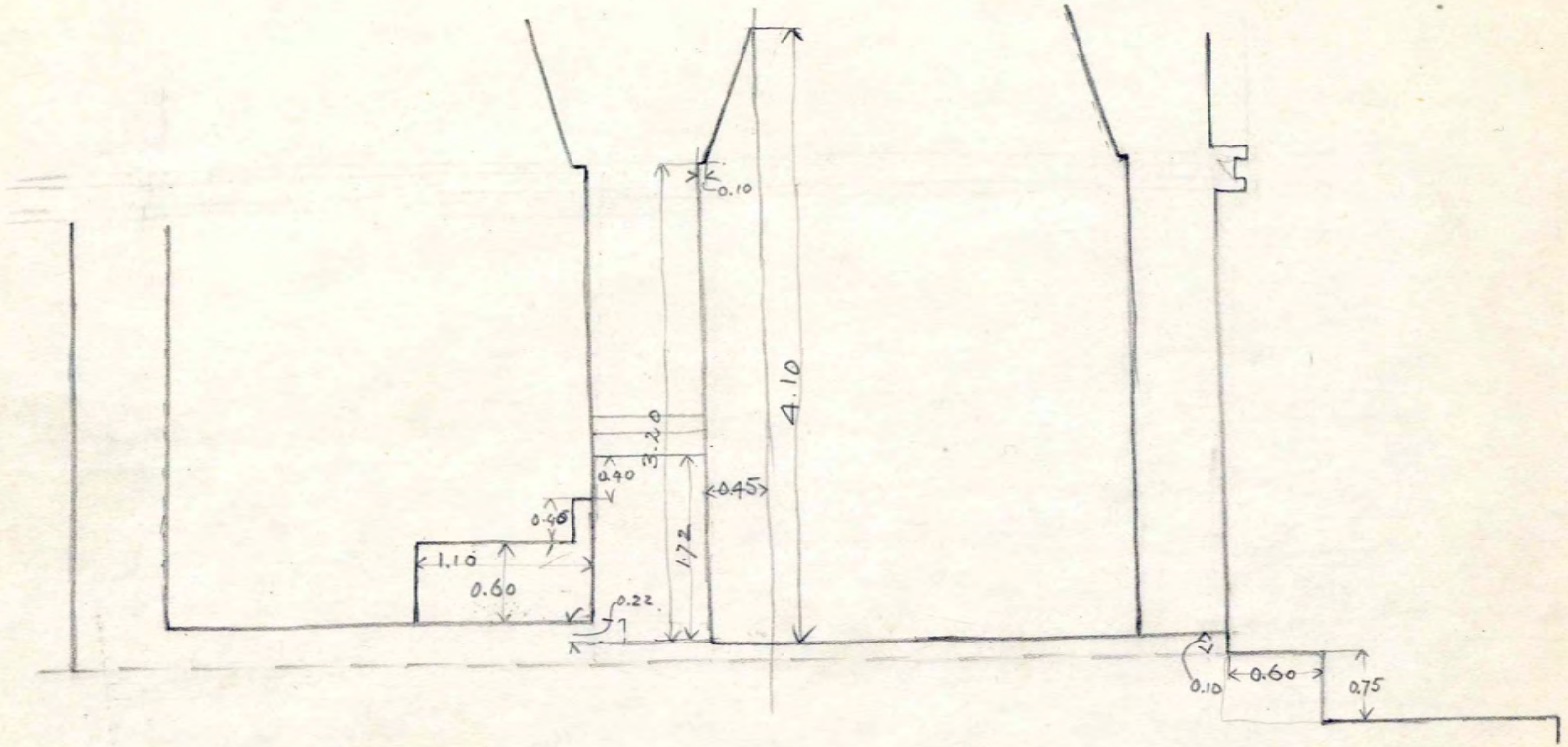
1.725 B
1.566 A.
-.159
difference in
Points (A) & (B).

1.95
1.30
1.15
4.40

Sept. 27
when 1931
(redrawn
1934 from
new accurate info.

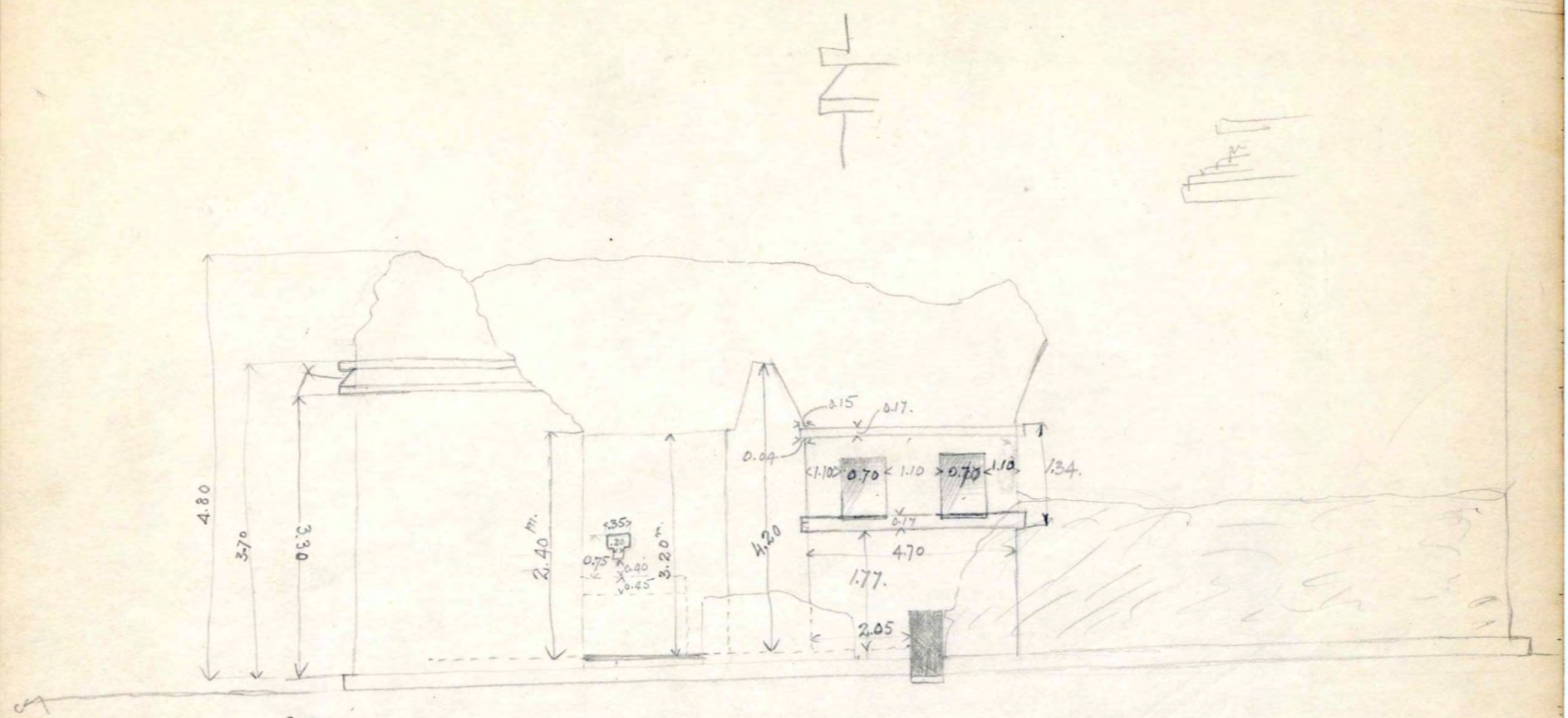
Wyers SKETCH.

This is Str. XXVI, Section through wkg front & rear rooms. S →. (H.S. 1932).



1.50
.95
.555

May 1931
Str. XXVI



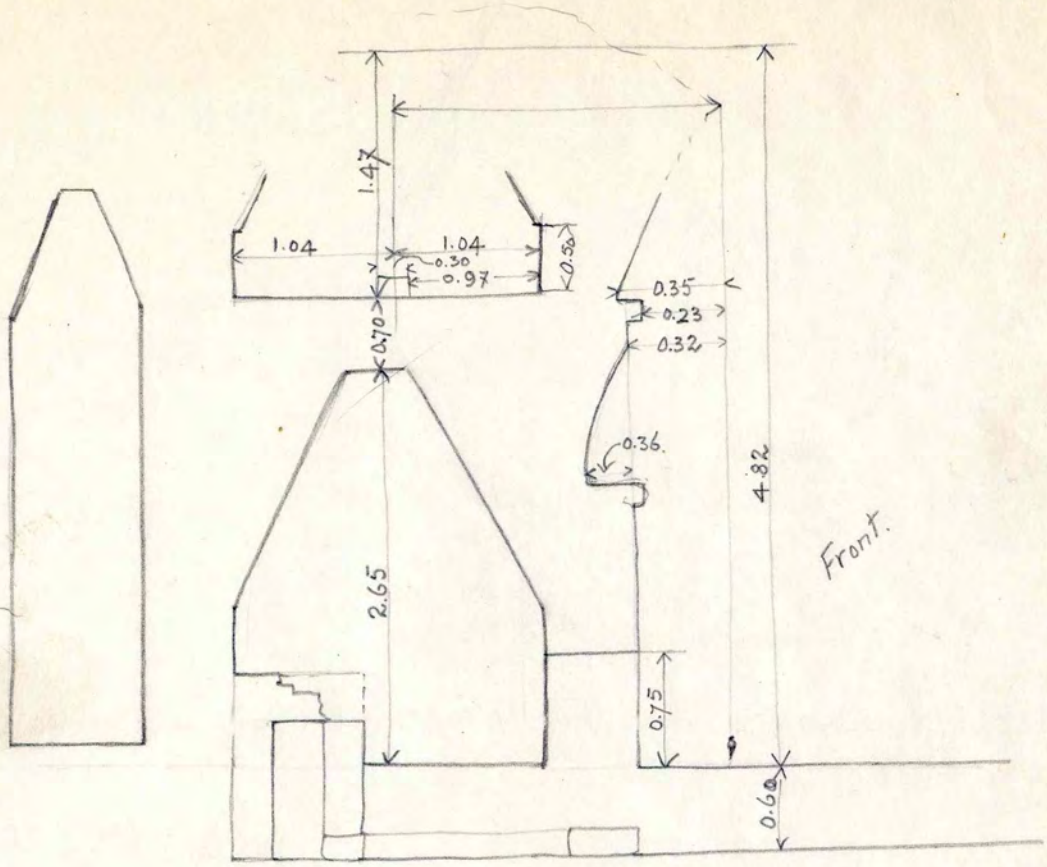
Front View.

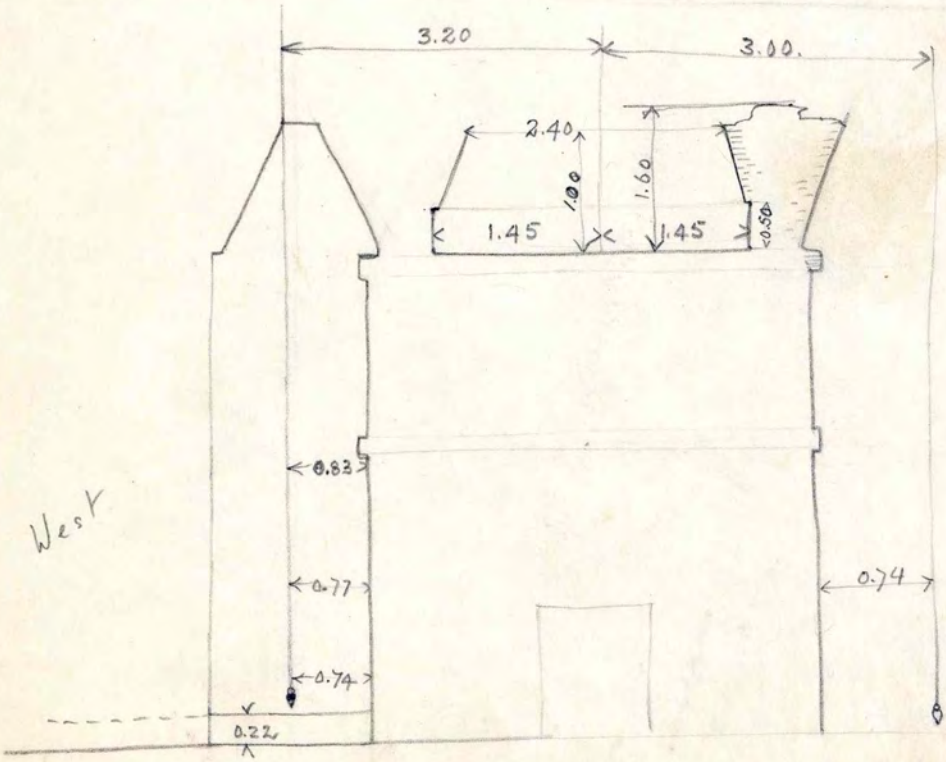
Aug. 27 1931

Sta. P-7

Wyo. 1931

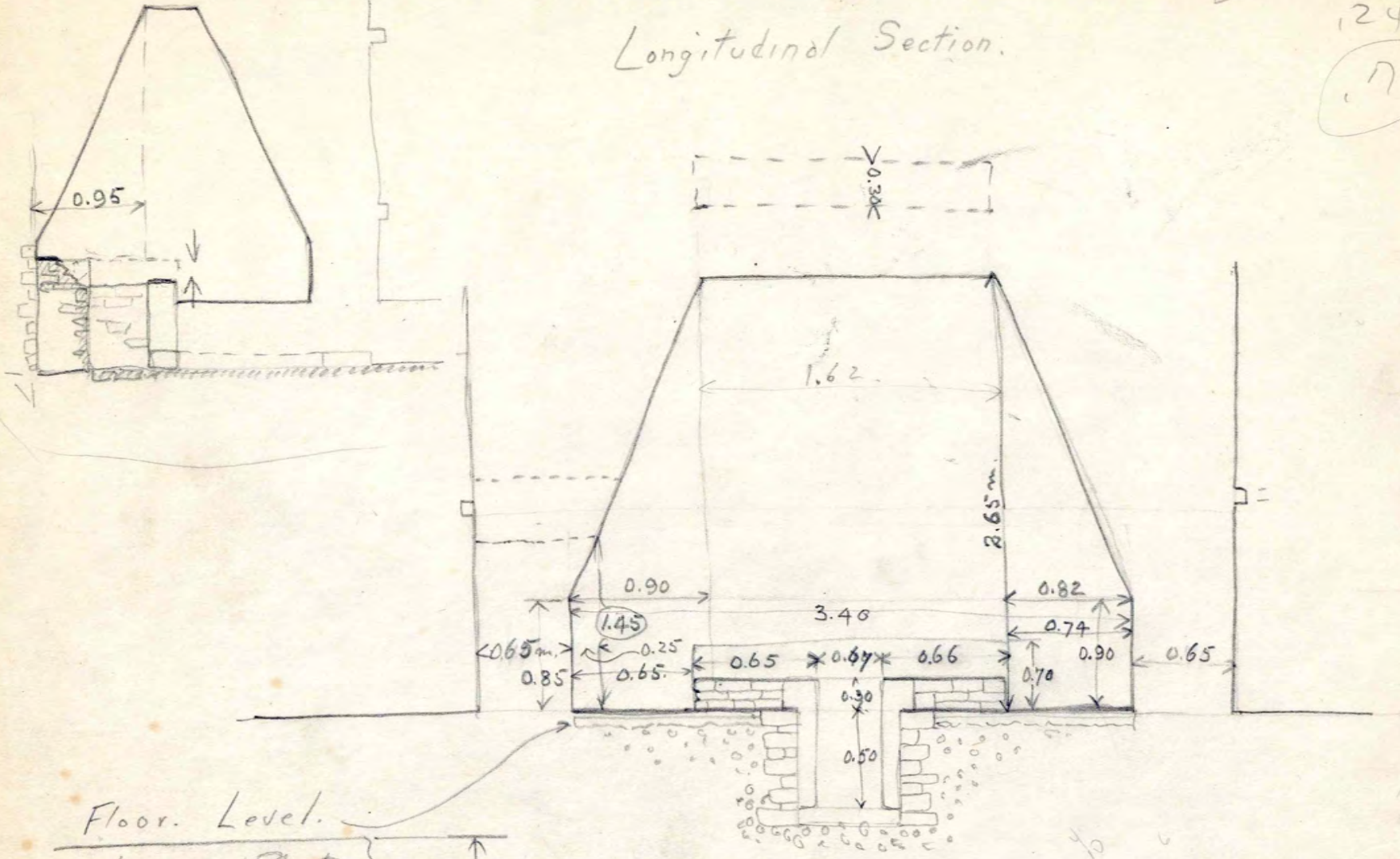
(26)



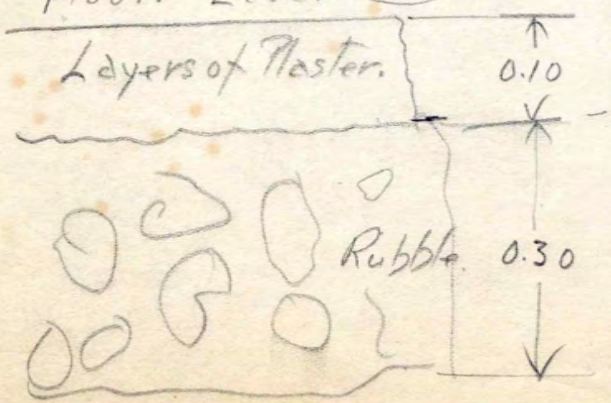


Front View.

Longitudinal Section.



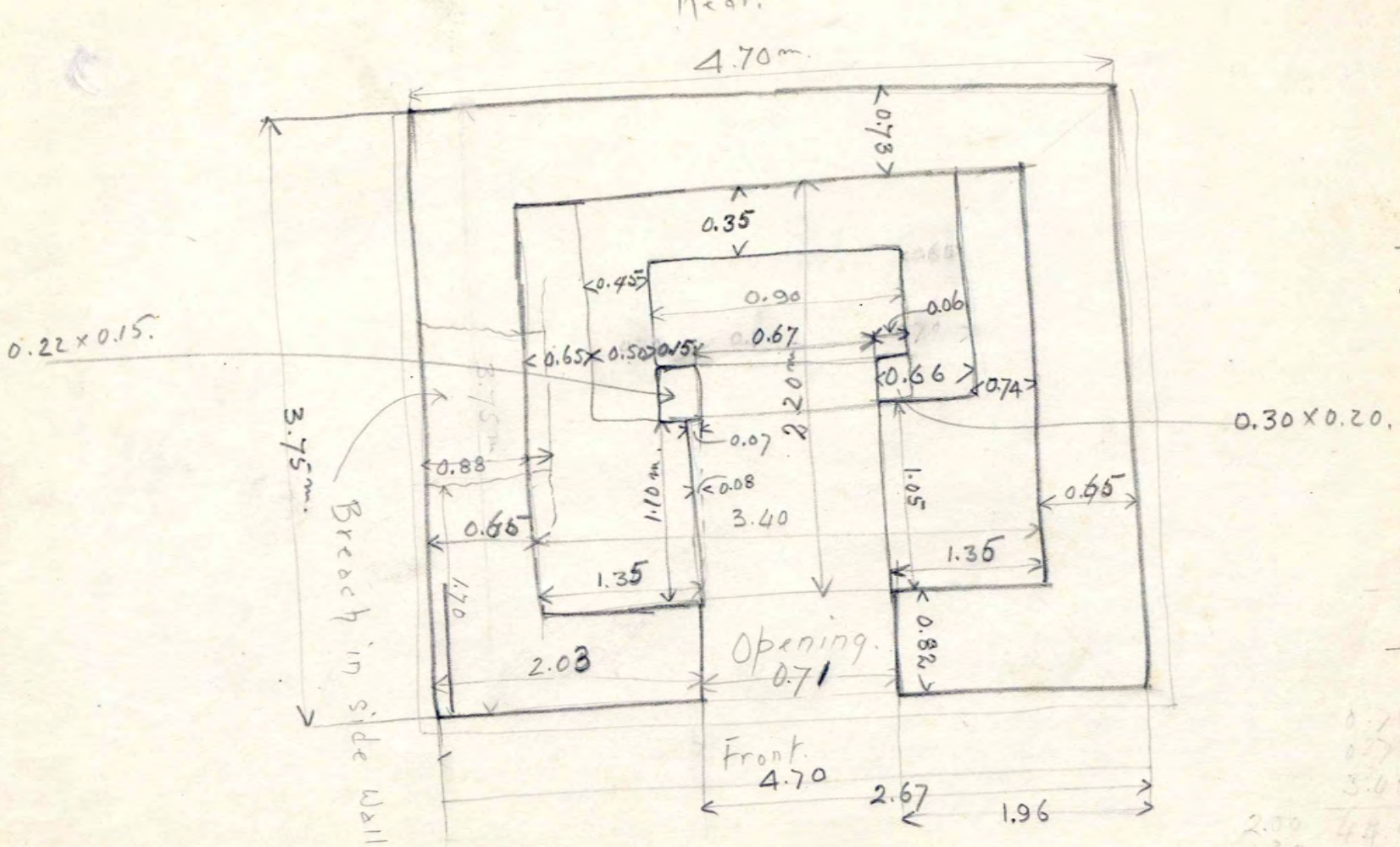
Floor. Level.



1248

3.40
1.72
1.68

Str. P-7

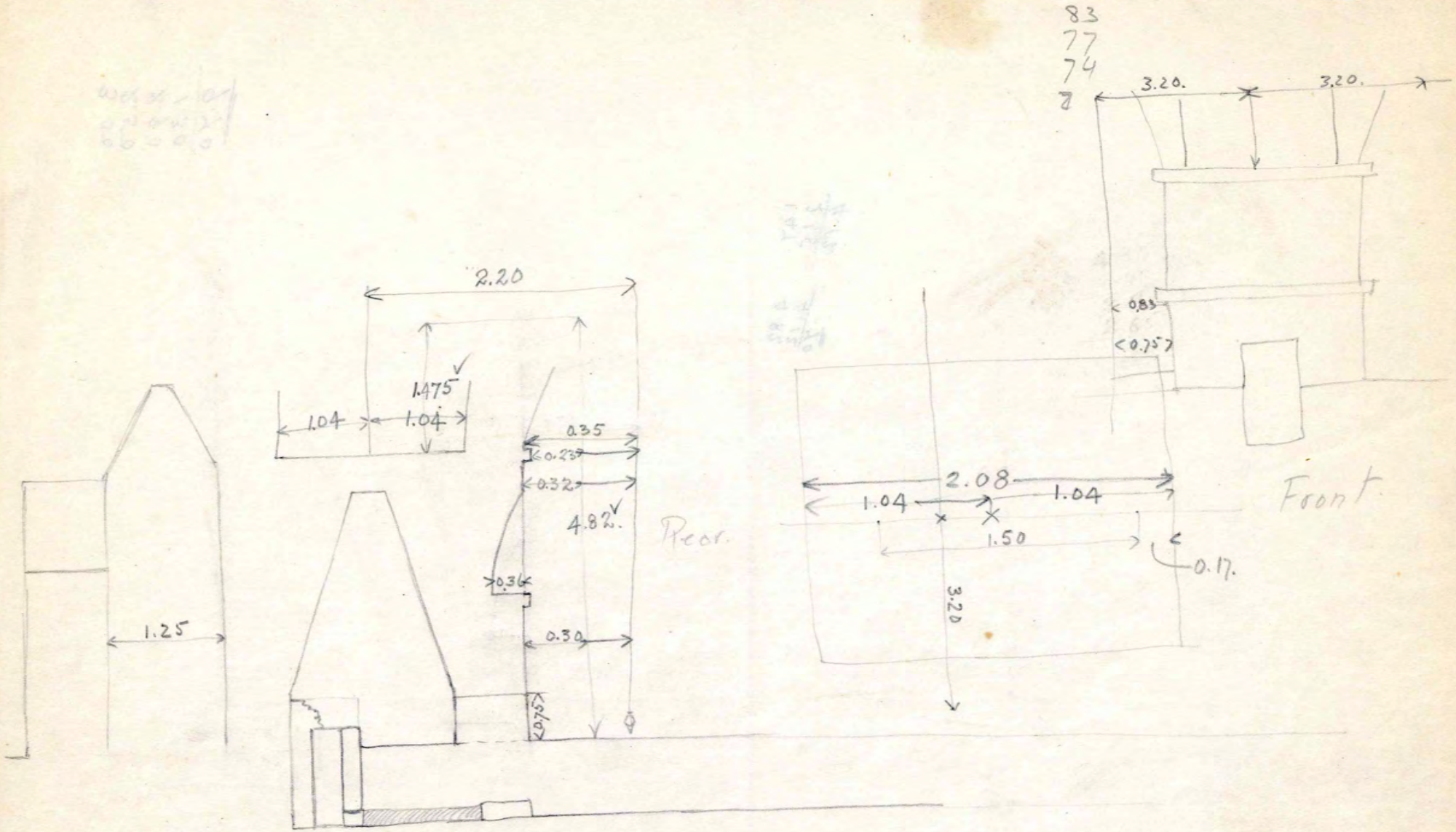


0.65
0.50
0.15
0.67
0.06
0.60
0.74
3.37

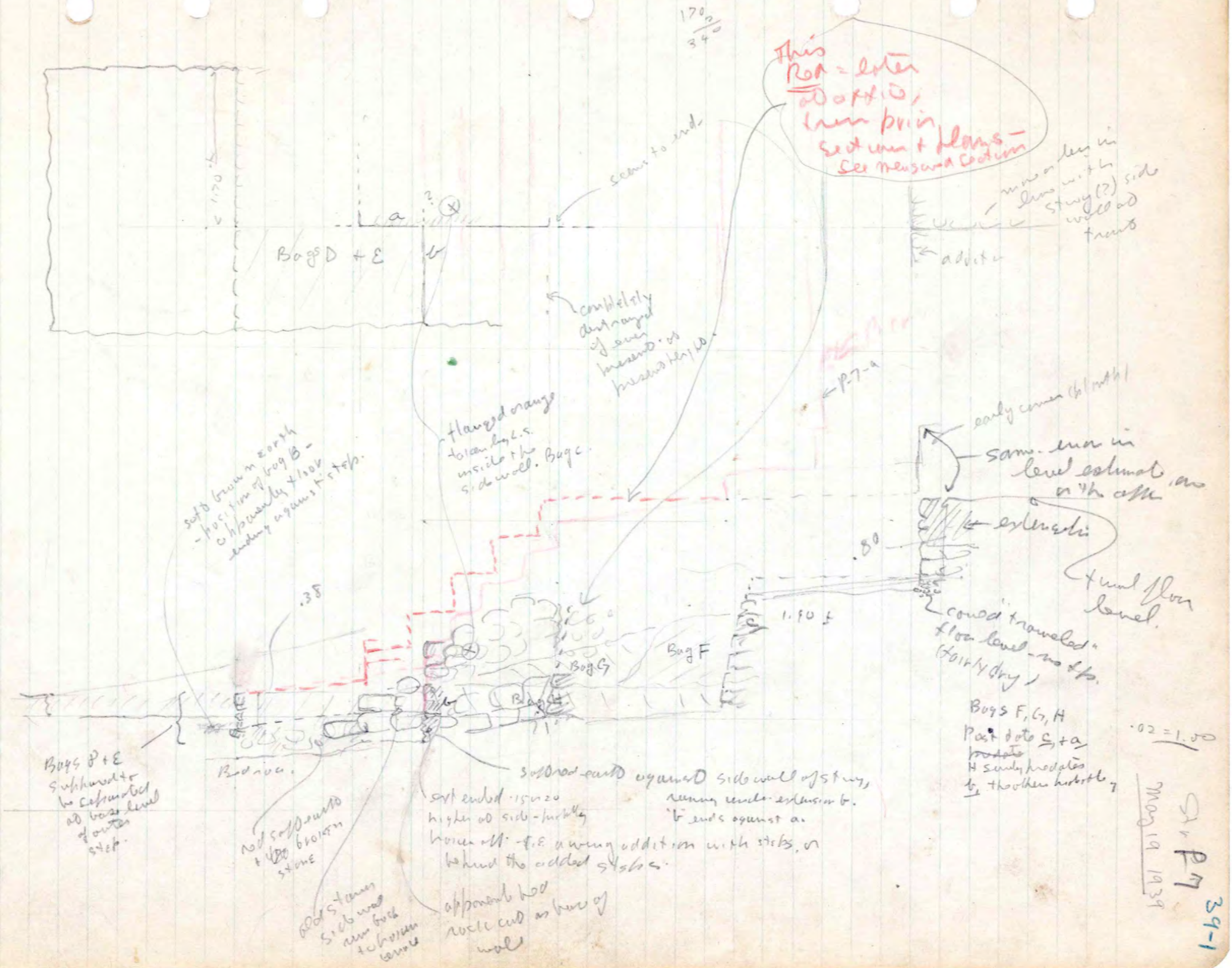
4.70
2.67
2.03

3.75
0.82
2.93
2.20
.73

St. P.T. Wyer. 1931



Sta. 9.7
Wyer, 1931


170 n
34 o
This Rod = later addition, less prim sed unit + flags - See measured section
seems to end
a
Bags D + E
1.70 ±
completely destroyed if even lowered as high as
flagged orange tag only c.s. inside the sidewall. Bag C
soft brown earth - top portion of bag B - coherently t/out ending against stub
.35
.80
1.50 ±
Bag F
Bag G
Bag H
Bags D + E
Bag C
sod roof and broken stone
sod ended - 15 to 20 higher on side - luckily known all - E awning addition with stubs, or behind the added stubs.
sod roof and organic sidewall of stump, running under extension b. 'b' ends against a.
approach road inside end as base of wall
add'l stones sidewall run back to known level
p.7-a
early corner (b/out)
same - run in level estimated on 4th addn
extension
trench floor level
corner trenched to floor level - no ftg. (solidly dry)
Bags F, G, H
Post date S, + a/
H surely predates b, the other habitable
.02 = 1.50
May 19 1939
St. P7
39-1

Outline of evidence for the semi-vaulted nature of the P-7 roof.

1. Low debris depths as compared with known fallen complete vaults at P.N., Palenque & Yaxchilan - except (left front) where fallen wall and vaulting account for it. Note: the P-7 walls are a meter higher than in other vaulted P.N. buildings, and this meter has here fallen: The very low debris in the rear left room indiates that the entire double vaulting on this meidial wall feal into the front room, which thus received more than its proportionate share.

2. The projection or offset at the top of exisiting vaulting on right medial and central chamber walls. This is consistent with our hypothesis but can be reconciled with a complet vault only by supposing the later was stepped. This style is unknown in other P.N. buildings and at alenque, though there are a number of examples at Yaxchilan. The point is therefore not conclusive. Its weight in in our direction is added to by the fact that two or the three slabs observed in this position are only 5 cms thick, whereas a good heavy slabnwould be expected at this offset, by analogy with Yaxchilan.

3. The fact that the the preserved vaulting on the right medial wall extends to a fairly uniform height throughtout most of its length, on both sides. If this is a remnant of higher double (balanced) vaulting, one would not expect such an even line marking the points where the fallen masonry parted from what remains. This condition is on the other hand entirely consistent with our hypthosis, since these lines fallow rather closely the level of the under-side of the offset or projection as determined at three certain points.

   In line with this, the surface over the center of this vaulting slopes down evenly on either side, but is fairly level in a lengthwise direction, except toward the right where (I think) it was excavated sli htly in 1931). This contour would it seems to me, naturally result from gradual disintegration on our hypothesis.

4. The distribution of identifiable roof-cap material.

   a. Identifiability - description.

      1. Gravel-concrete slabs.

         Where not disintegrated to gravel, these are small fargments of concrete in which there is much gravel, a minimum of mortar.

         Mortar is white, opoosed to usual yellowish mortar used in walls and vaults of this (and other)P.N.) buildsings.

         It is harder than the above.

         It contains occasional brick-red potsherds, not observed in cross sections of the above.

It was found usually in association with small stone slabs and thin stone flakes, in one or two cases adhering to the latter. This is a week point as small slabs and flakes also occur in walls and vaults of this building - but the point takes on more force in connection with the distribution of the gravel.

The gravel comes from a thin sheet, to cms thick, as evidenced by a satisfacory number of pieces recovered. Max. dia of loose pebbles observed was cm.

2. The finishing plaster layer.

A number of larged frgaments (up to 30 cms in width) were found, which had a surface coating of lime finishibg plaster to cm thick. The two layers thus established form a suitable surfacing for roofs.

- the upper finishing plaster is the normal thing at Palenque and doubtless in the Maya area generally, though it is laid on basic concrete of crushed (hard stone) like stone and mortar, in all known cases.

- The large proportion of gravel in the second layer and the extra hardness of the mortar (if it was always harder), this layer being close to the surface would make the roof as a whole more imperious to mositure and more resitant to plant growth than an ordinary roof of finishing plaster on ordinary crushed lime stone concrete.

3. The foundation of crushed-stone concrete.

The gravel layer was found usually in association with ordinary crushed-limes stone concrete, which was much softer. In several places this was identifiable as underlying the gravel which in turn underlay the finsihing plaster. In one place this combination was found lying directly on the well-preserved floor and the three layers showed every sign of being integrated. Here the thickness of the three layers taken together was 15 cms, which we take as the minimum thickness in our reconstruction. In this case one pebble was found near the bottom of the crushed stone concrete, confirming the association of the three layers.

4. Small slabs and limestone flakes in most cases were found in close association with the gravel concrete. In one case gravel was found cemented to such a small flake; in two or three cases the small irregular slabs lay directly under the three layers as above discribed. But the lowest layer of ordinary concrete was never identified as having been laid directly on the slab. It seems highly probable that small limestone slabs and flakes entered into the roof construction, below the gravel-concrete layer, but whether they formed distinct layers could no be determined. This may have been, however as the lower layer was too soft to be expected to retain its grip on the slabs during its fall. In unprotected position above remaining vaulting disintegratation was too far advanced to afford evidence one way of the other.

5. As part of the observed deposits of associated finshing plaster, gravel concrete, crushed-stobe concrete, small slabs and flakes, occasional weathered potsherds were encountered. These were not noted elsewhere, and in two or three cases they were still imbedded in the gravel concrete. They thus seem to form an additional item in the complex under discussion, and aided in its recognition. There probabtive force is considerable, perhaps. But they were not plentiful, and taken alone, would prove nothing.

supposed
b. Distribution of the/roof-cap material.

1. Uniquness: nothing like this well defined layer of river gravel, closely packed in mortar, was been observed in the de of other vaulted structures at Piedras Negras (all known va units, buildings, have been examined; nor in standing portions walls and vaults; nor on roofs or observed sections of walls and va at Palenque and Yaxchilan.

2. It does not occur in standing sections of walls and vaulti the central chamber and outer walls and vaulting of this building.

3. Disintegrated gravel, and small pieces of the still hard concrete were found well distrubited on the center of the surface vaulting over the right medial wall, and on the sloping su on either side, right down to the edges. They were also found on th point over the vaulting at the right front corner, and at several p (including the highest) over the vaulting above the central chambe

This is in harmony with our hyptothesis, under which we post a roof surface, now disintegrated where it is not fallen to the roo which was slightly above the levels where the fragemetns and gravel found. If we postulate a roof surface two or three meters above thi it is difficult to bring much of it to these positions.

4. Another logical possibility might be that this gravel fo a horizontal layer or course running through the interior of compl vaulting, something like the layers running through pyramid hearti at Cgichen Itza. If this were so, however, we should find inthe ri as well as the left rooms, where all the vaulting is fallen, depos the river gravel between vaulting slabs, which is not the case; an we should not find pieces of the grvael concrete nicely finsihed w finsihing plaster, which we do find. It therefore seems safe to el this possibility from consideration. If we do, the presence of th at the points above surviving vaulting establishes the case.

5. The great bulk of the vaulting in this buil ing has falle under either hypothesis, and the bulk of the roo material is therefore known to be in the debris on the floor or ju the building. Because of the unique character of gravel in concret even where the layer in question has disinegrated, the remaining h pebbles show us exactly where it has fallen. Any roof restoration must conform to the observed positions of this gravel.

It is formed the roof of completely vaulted unit it should rarely if ever closr to the fllor level. In this case wall stones, vaut-facing slabs and cap-stones would have to fall before the ro could move. They weuld all be nearer the flbor and would reach the together with masses of soft yellow wall and vault mortar, and roof concrete, which should overly the gravel levels above the flbor, that while the bulk of the gravel should be close to the floor, the Bulk of the rubble would be very close to the floor. Scattering out close to the wall deposits of gravel with occasional hard pices of the gravel concr along with the associated deposits outlines above, were found on the three cross sections examined in the front room, spaced as fbb m from the right wall; just left of the central sun passage; m from the left wall. Note that these pass repespectively through very shallow, medium and the deepest deposits encou ntered. In each much of the gravel was within

or 30 cms of the well defined floor. In no case did it rise to a
greater than cms below the debris surface. If we include the
crushed limestone concrete, small slabs and flakes which we
believe formed part of the roof cap, much of the deposit as a wh
directly on the floor.

On the right section, there were no large slabs such as
to form a large part of the vault facing. This is understandable
the right medial vaulting still stands to maxium height, under c
hypothesis. It is clear that the front vaulting fell forward and
the building. If however, we suppose that only a half or less of
vaulting remains, we can only explain this situation by supposir
to have fallen in the rear right room. Here we did not save
more than the rear half of a cross section, and the
itself is disintegrated. But a thick deposit of gravel remains
up to 30 cms above floor level on a satisfacory logitudinal sec
but, as in the front room, cannot be traced to the rear wall. I
certain therefore, that in the centers of the rooms before and
the right medial wall, any fallen vaulting must be placed above
below, the gravel complex.

On the center section the gravel complex does in fact ly
vault slabs. These have obviously slughed off from the semi-va
the front of the central chamber. Their quanity is not suffi
to account for complete vaulting even here whe
room width is at a minimum, but is far short of it.

On the left section similar conditions occur. On this c
the gravel depsosits rise toward the rear to a maximum height c
, but the bulk is close to the floor and no vault sla
were found below it; on the contrary, not only vault slabs but
a section of intact vaulting, with its finsihing plaster comple
showed by its high position that it fell after lower gravel dep
little to the front, while loose gravel occured directly above

Here it is quite certain that the medial wall falied
forward direction, precipating most if not all of the vaulting,
front and rear, into the front room. This is the only way to a
for the relatively great depth here in the front room, in comb
with a very shallow deposit in the corresponding rear room.
rear room the gravel was found immediately above the bench "al
above fllor levelsin front of it, and against the medial wall
side, just above fllor level. Here, as in the first and second
of the front room, large pieces of the gravel concrete, with t
plaster surface were found, with only a thin layer of ordinary
between them and a well-preseved floor. One piece was inverted
the other, the two finsihed surfaces in contact, showing what
course clear, that we were dealing with material fallen from a

It is impossible to reconstruct in imagination the an
which this building, as a completely vaulted unit, went to
and in the process dropped roofing material under wall and vau
material in all cases.

partially

Postulating a/beam-supported concrete roof cap at the
shown in our reconstruction, on the other hand satisfactorily
the observed facts. The beams would be expected to rot and to
prey to termites long before vegetation began to tear vaulting

walls apart. This would precipitate the central portion of the roof/cap of each room onto the floor below, breaking it into small piec This would occur bit by bit, so that while much of the material woul lie directlynon the floor (though usuauly not close to the walls, wh were still overhung by semi-vaulting) much also would pile one piece on another. Partially fallen beams might easily act as slides and so precipiate portions of the cap against the bases of v on occasion. This would account for this condition in the left rea not observed elsewhere.

Where the semi-vaulting has not fallen, the cap de in itself not very thick, would not pile up to great depth. This i conidtion in the right front room, Where it has completely fallen one would expect the cap which was over it, as well as over beams, to leave traces at a maximum height above the floor, perha a lower deposit having its point of departure above the be This is the siuation in the left front room. Here and here only w gravel found more than 60 cms above fllor level. In this case a d 2o to 30 cms thick, badly disintegrated, has its maximum height a 1.80 m immediatelynundrlying large slabs which slope in the sam direction as the deposit. Vault slabs may be supposed to have tur over in their descent. On the other side of the trench an intact of vaulting, already mentioned, appears in the same relative po Below the high deposit just mentioned is another with its maximu height only 60 cms, approximately the maximum observed on the ri

As stated before, the possibiloty that the concrete extended through the interior of complete vaulting is ruled out finsihed surface found on it at three widely separated points by the fact that it is never found between parallel vault slabs debris, but on the other hand, is below them whereever they occ present when they do not.

In recapitulation it should be stated that all elements supposed roof-material complex were found, not only only or clo the floor, but also above the existing vaulting - that is, grav concrete, ordinary concrete, small slabs, stone flakes, occasional sherds. The only exception is the final finsih coat on the gravel concrete, which was preservedonly in buried close to the floor. The distribution of this complex then, its fallen positions, sustains our reconstruction and seems to the only other hypothesiies avai able. It cannot be reconciled with the theory of complete vaulting tofull height or of inter

5. Especially long slabs, suitable for cap stones in complete vau ti were not recorded as occuring in the fallen debris. These have been found in all vaulted units where they have been looked for.

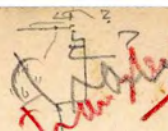
6. Large slabs suitable for vault facing were in no case found in co with the floor. In all known cases of fallen complete vaulting, such slabs have been so found.

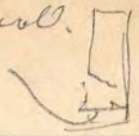
P-7

5/21/35

Left front room. Plaster material from roof covers floor. also with some small slabs. above this debris is of large slabs, blocks, + mortar. Roof plaster at bottom has some pieces of plaster with river pebbles.

(Nesson)

Sand.  Plan of old stone.

god wind [illegible] on side wall. 

P-7
1935

P7. Queries.

~~Chamber~~ jambs:
~~Ok~~ Did passage provide walls. ⌊ ⌋? yes draw

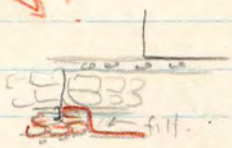
→ { Look for floors · blaster in hole in headroom floor.
Cut Passg wall to make sure it doesn't divide horizontally. -a0 -50

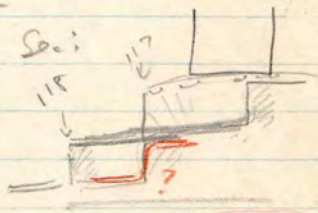
→ Draw Footing a bit to locate - see floor near right end of platform. take level.

The entrance is about certainly a jump passage was hardly occupied both used again. Cross from it.

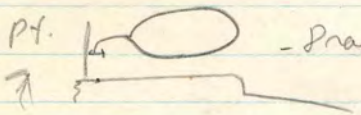
Open section l&D end, Front & room (1. P. lengthened)
~~Ok~~ add h. of bench,
~~Ok~~ sketch debris section.

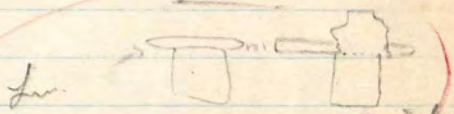
~~Ok~~ l&D front: can we duplicate it? ?



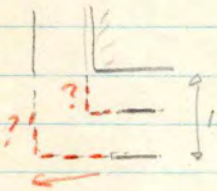


~~Ok~~ 2 photo notes // This requires a new existence step, and bend a hook, in platform wall.

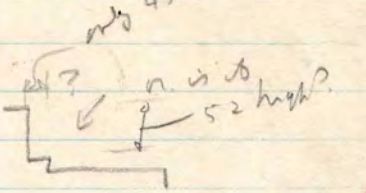
~~Ok~~ Near Pt.  - Draw everything on this end now.

note:


Rt. Corner. Draw this.



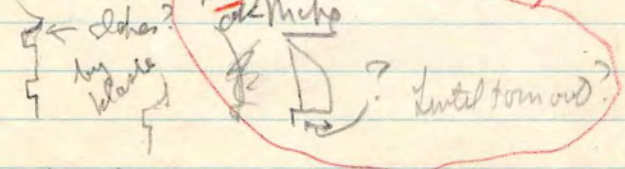
Check. Horizontal distance lower front steps when looks as if in place?



Ok, How far front does Cross section through Ramey, outside?

~~Ok~~ Floors under Rt. room wall?

Thanks for [illegible] Platform is double at end of Passage.

Mason p4. 

by water only

Levels of sand floors inside.
Follow floors from sand to outside. See p41
Corner stones at stairs: all from.
Thick of front room floors at rear wall - contacts stairs

-.40

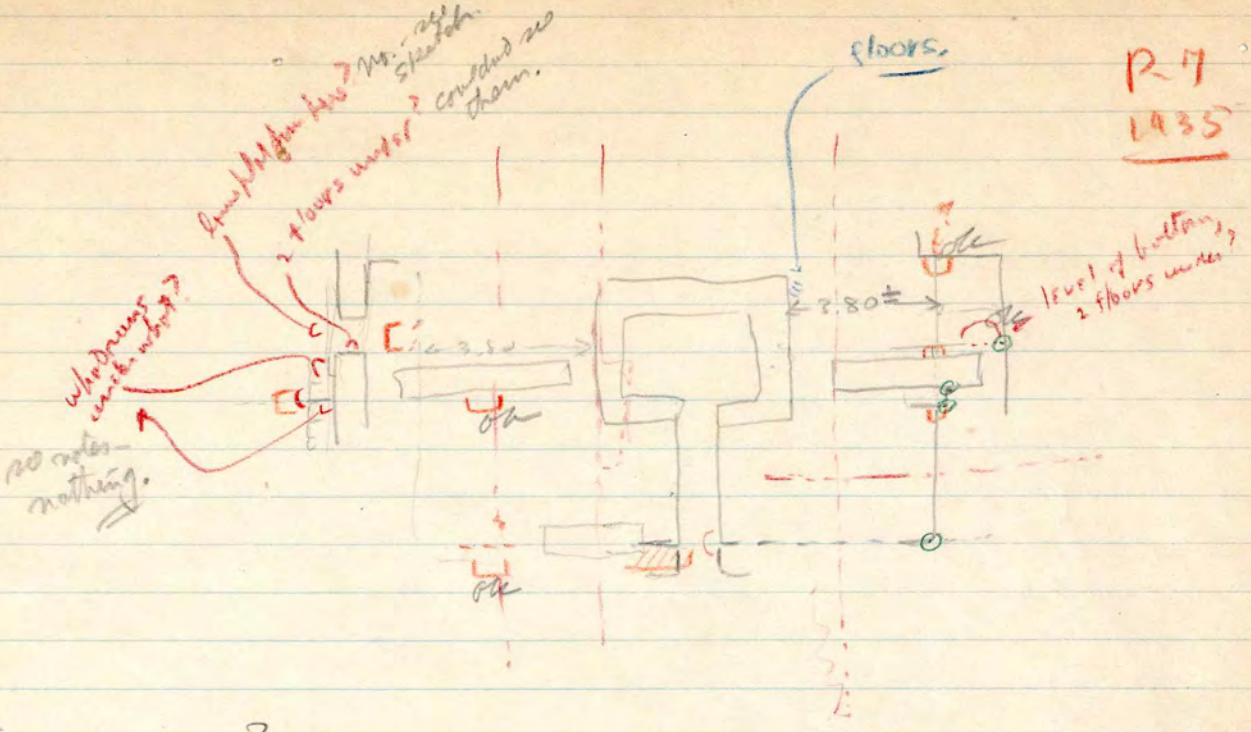
p. 56 - Found plenty of Pots - .58
only 20 at 610 cm 2

p58 - Potsherds at front of passage
bed h2 98 - 31 = -.67 (above earlier floor)
.54

p 45 - Poor pt. "throw" near pavement to floor? no

p. 52 - flint.

R-7
1935



There are probably 5 floors.?

1. Platform.
2. 2 nd "
3. Resurface of 2 nd Plat. } under all.
4. ~~Resurface~~ Sanct.
4. Resurface Sanct.
Excd over walls +
5. resurface.

← this is the doubtful one.

Is this true?

See Drawings

all floor levels
possible in relation to
Early platform.
- left rear room
- left front room.
elsewhere? - Sanct

all floor levels in
Rt. rear room.
left " "
check wall + floor
levels in
Sanctuary.

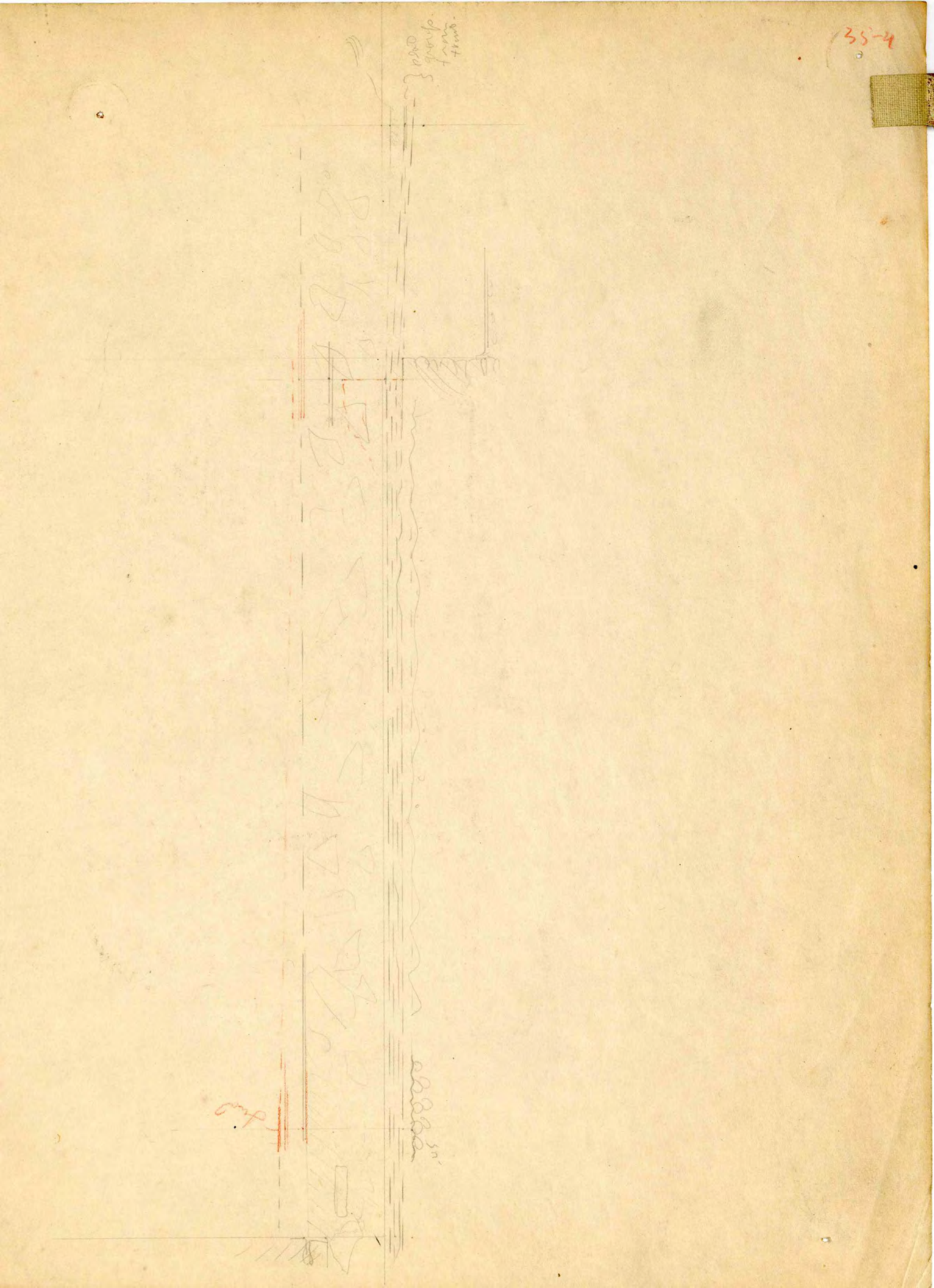
Transition
Signs of long bench of left rear room in Rt? - None Remaining
Sight over to end in left rear. — (Broken off by Mayus)

3. Cross Section
long + Elevat. left front.

Plan: to scale

Describe floors 1 to 6 in left rear Room
- there in left front
" " in Rt front
" " " rear
" " " Sanctuary.

Follow purple floor.
Find another floor below it (as on other side of Mod. wall.)
Find a floor at base of Sanctuary, near left or near rear passage.
Check level of base of rear of Sanct. — both rear corners.



Apiculture and Mod Mod P7-40

AVERAGE DIMENSION TABLES

Basal Platform Units

Phases	Units	Heights	Lengths	Depths	Slopes
Str. P-7-1st-B & -A	35	1.50*	?	?	82
Str. P-7-3d to -1st-A	30	1.90	?	?	82*
Str. P-7-2nd-F					
-E					
-D to -A					

Supplementary Platform Units

Str. P-7-4th-B & -A	none?				
Str. P-7-3d	none?				
Str. P-7-2nd-E & -F	25	.40	19.00*	11.20*	V
Str. -D to -B	19	.40	21.20*	11.20*	V
-A	"	"	"	6.00	V
Str. P-7-1st-B & -A	99'	.40	21.20*	6.00	V

Building Platform Units

Str. P-7-4th-B & -A	34	.50*	?	?	?
Str. P-7-3d	28	.40	12.35	7.30*	V
Str. P-7-2nd-F	26	.40	12.10	7.30	V
Str. P-7-2nd-E	26,26X	.40	12.10	9.50*	V
Str. P-7-2nd-D to -A	26,26X,18	.40	19.70	9.50*	V
Str. P-7-1st-B & -A	99,113,18	.65	19.70	11.20*	V

Building Units of Str. P-7-1st-B and -A

Units	Section Table					Facade Table			
								Doors	
	W	RR	M M	R' R'	W'	Length	Depth	Width	Height
4 (Encl. Bldg.)	.90	3.75	.88	3.60	.90	19.50	10.02	2.50	
								3.15	
8 (Sweat-room)	.80	2.20			.80	4.80	3.80	.77	1.10
8 (same, interior)						3.30	2.20		
6 (Fire-box)						2.00	1.05		
6 (same, interior)						.95	.35*		

Addendum: Maximum dimensions, lintel of Unit 8, 1.30, .83, .30

Note: Starred dimensions are approximation/usually based on reconstruction; the letter V means approximately vertical; see Part I, p 13 for further explanation of dimension tables.

AVERAGE DIMENSION TABLES

Dimensions as for report (this structure dug up in 1947).

Platform Units

Basal Platforms (Units)

Phases	Units	Heights	Lengths	Depths	Slopes
Str. P-7-4th-B & -A	35	1.60	?	?	82
Str. P-7-3d to 1st-A	30	1.90	?	?	82*

c+c

~~Platform Units~~ Probable Enclosing Building Platforms (probably limiting the dimensions of Enclosing Buildings)

Phases	Units	Heights	Lengths	Depths	Slopes
Str. P-7-4th (-B & -A)	34	.50*	?	?	?
Str. P-7-3d	28	.40	12.35	7.30*	V
Str. P-7-2nd-F	26	.40	12.10	7.30	V
Str. P-7-2nd-E	26,26X	.40	12.10	9.50*	V
Str. P-7-2nd (-D to -A)	26,26X,18	.40	19.70	9.50*	V
Str. P-7-1st (-B & A)	9,13, 18	.65	19.70	11.20*	V

Supplementary Platforms (Units)

Phases	Units	Heights	Lengths	Depths	Slopes
Str. P-7-4th (-B & A)	none?				
Str. P-7-3d	none?				
Str. P-7-2nd-(-E & F)	25	.40	19.00*	11.20*	V
Str. P-7-2nd (-D to -B)	19	.40	21.20*	11.20*	V
Str. P-7-2nd-A	19	.40	?	6.00	V
Str. P-7-1st (*B & A)	19,9	.40	21.20*	6.00	V

Building Units (Str. P-7-1st) B and -A

Building Units (Str. P-7-) Facade Table

Units	Section Table W	R	M	R'	W'	Length	Depth	Doors Width	Doors Height
4 (Encl. Bldg.)	.90	3.75	.88	3.60	.90	19.50	10.02	2.50	
8 (Sweat-Room)	.80	2.20	~~.88~~ 3.60		.80	4.80	3.80	3.15 .77	1.10
6 (Fire-box) (same, interior)						3.30 2.00	2.70 1.05	.67	.50
6 (same, interior)						.95	.35*		

(Maximum dimensions, lintel of Unit 8: 1.30, .83, .30)

Note Starred ~~items~~ dimensions are approximations usually based on reconstruction; the letter V means approximately vertical. See Part I, p 13, for further explanation of dimension tables.

	Sta. P-7	Sta. I-11	Sta. F-4
Span	3.70	2.60	2.55
Wall thickness	.80	.75*	.60
Wall Height	3.20	2.15	?
Door-width (max)	3.60	2.15	1.35
"Pier" width	2.90	1.30*	1.30
Span to wall thickness (here and)	22%	29%*	24%
Span to wall height (")	86%	83%	?
Door to "Pier" width (")	80%	60%	96%

*Piers created by T-shaped piers.

Span

3.70 | 80.00 | 21+ = 22%
740
600
370
230

Door span 3.60 | 2.900 | 80 = 81%
2580
200

Span to wall height

3.70 | 3.200 | 86%
2960
2400
2220
180

Wall thick to thin

3.20 | 80.0000 | 25%
640
1600
1600

.80 / 3.2 = 0

Span 2.55 | .600 | 235+ = 24%
510
900
765
1350
1275
75

Door span 1.35 | 1.300 | 96%
1215
850
810
40

Span +th. 260 | 75.00 | 29%
520
2300
2340

Door-Span

215 | 1.300.0 | 60%
1290
100

Span to wall th. 260 | 2150 | 83%
2080
700
780

2.15 | 7500 | 34.55%
645
1050
860
190

Probable Building Plat Van Units (Probably Limiting Dimensions of Enclosing Buildings)

Units	Lengths	Widths	Heights	Slopes
34 (Str. P-7-4th (B.2-A)	?	?*	.50*	
28 28' (Str. P-7-3d ~~B~~)	12.35	7.30*	.40	
26 26' (Str. P-7-2nd E)	12.10	7.30	.40	
26-26 - 26X (Str P-7-2nd E &	12.10	9.50*	.40	
26-26X-18 (Str. P-7-2nd P+C+B	19.70	10.20*	.40	
9-18-18 (Str. P-7-1st B+A.	19.70	10.20*	.65	

Subbl. Plat. ~~Units~~

~~34~~ (Str. P-7-4th B&A)	none?	none?	none?	
(Str. P-7-3d	none?	none?	none?	
25 (Str P-7-2nd F)	18.00*	11.20*	.40	
25 ~~more than~~ (Str P-7-2nd E	"	11.20*	.40	
19 (Str. P-7-2nd B, C) ~~B~~	21.20*	11.20*	.40	
19 (Str. P-7-2nd A,)				
19-9 (Str P-7-1st B+A.)	~~21.20~~ "	16.00	.40	

Note: ~~Width of Unit 34 was more than ____, and length was less than ____.~~ ~~Only the~~ Unit number of latest plan only is given

Note: Length of Unit 34 must have been less than 12.35 (See Section 48).

Units 8

4 | 1.07 | 27
8
27
28

Units 8 4 | .017 | 42
16
10
8
2

4 | 26 | 65
24
20

4 | 35 | 8
32
3

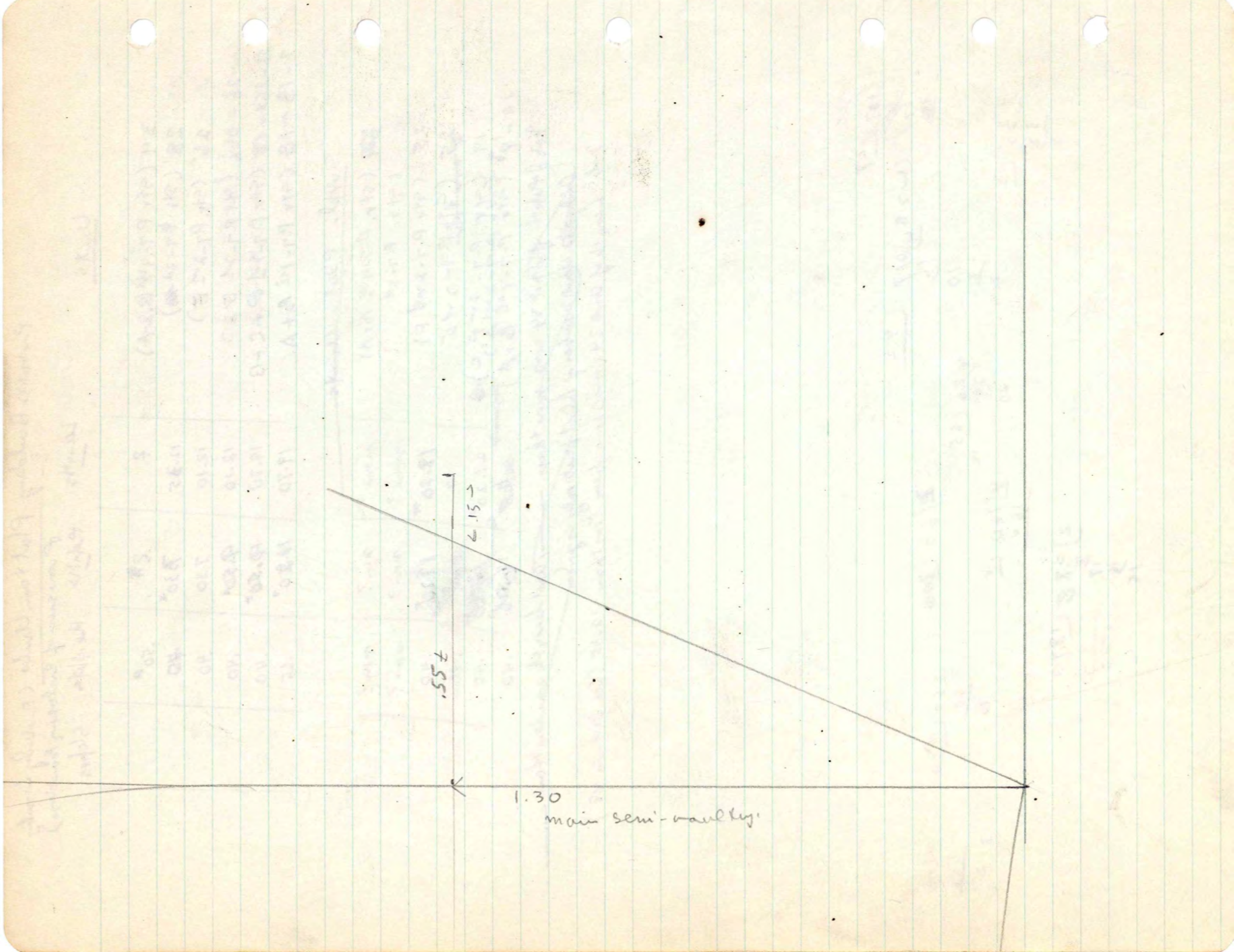
2 | 60 | 30

4 | 160 | 4
160

2 | 38 | 18.90
38
17
16
16

2 | 39 | 19.50
38
10

19.70
1.50
21.20


.15
.55
1.30
main semi-vaulting

P-7 1946.

Final mens. for use in dent + av. d.m. tables.

Vault height (adjunctions mid + sword-room boarding) 1.30

of mid wall 3.09
of front wall 3.29 } call it 3.20

from n.y. plan

Wall thickness - .80 N check up 1948

Room widths - front right 3.00 (check with Mayhes artist
rear " 3.00 (on at ft boundary)

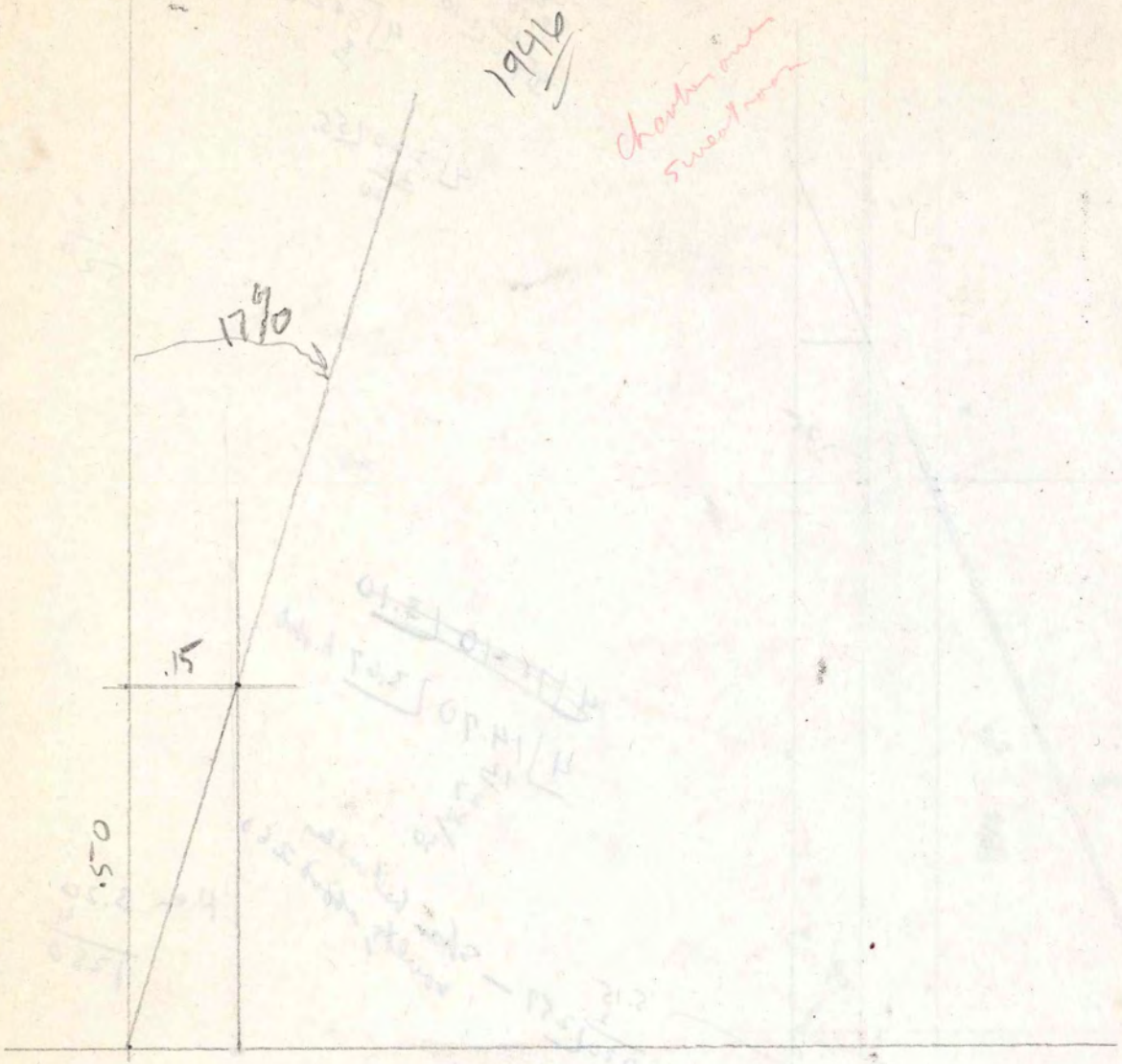
3.00 | 8.00 | 2.6
6.0
2.00

3.70 | 80.00 | 21 = 22%
74 0
600
370
230

Pon widths: Side 2.40 + 2.50 = 2.45

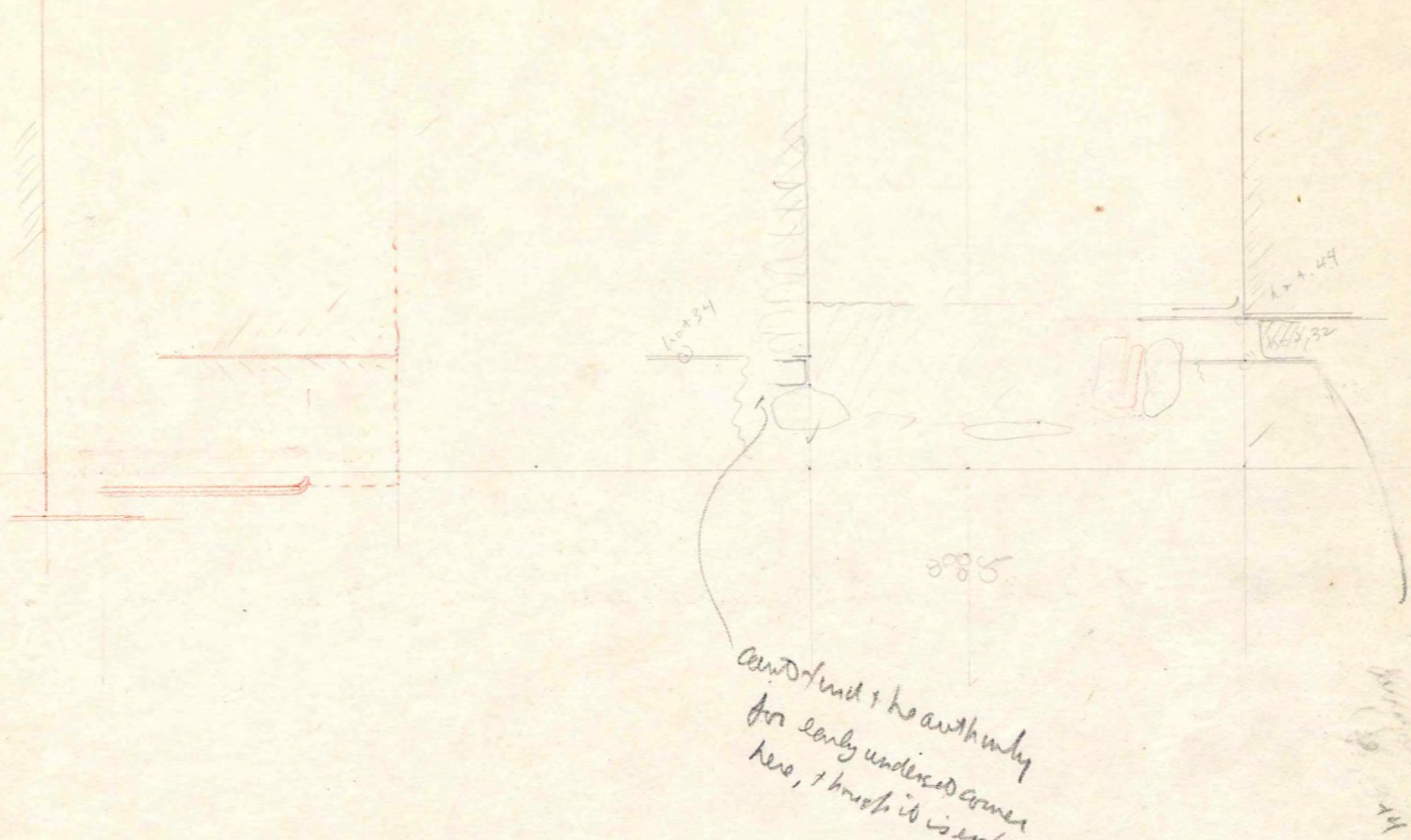
Center 3.60 3.15 1948

"Pier Widths" 2.85 + 2.40 = 2.90


1946
17%
.15
.550

P.77

to Brown Sand.



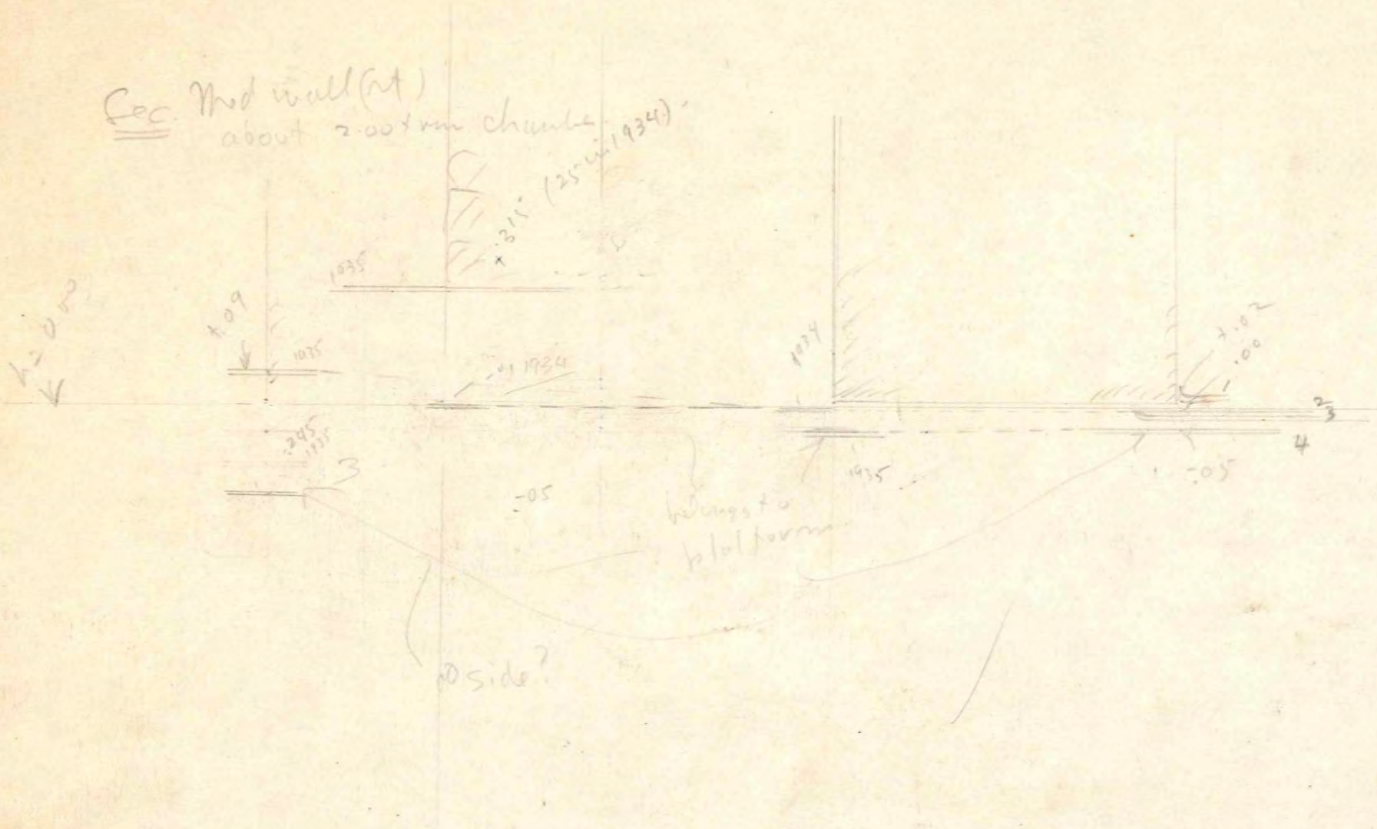
Centre of trench + beam thereby
for early undercut corner
here, + knock it in overboard

2

74

55-5

Rt Side Floor under Mod wall & Bent 1



July 13 Conclusion:

The P-7-2nd platform attained heights of wall heights of P-7-1st, even on rear rooms. These were probably elevated from logging. (check on left rear).

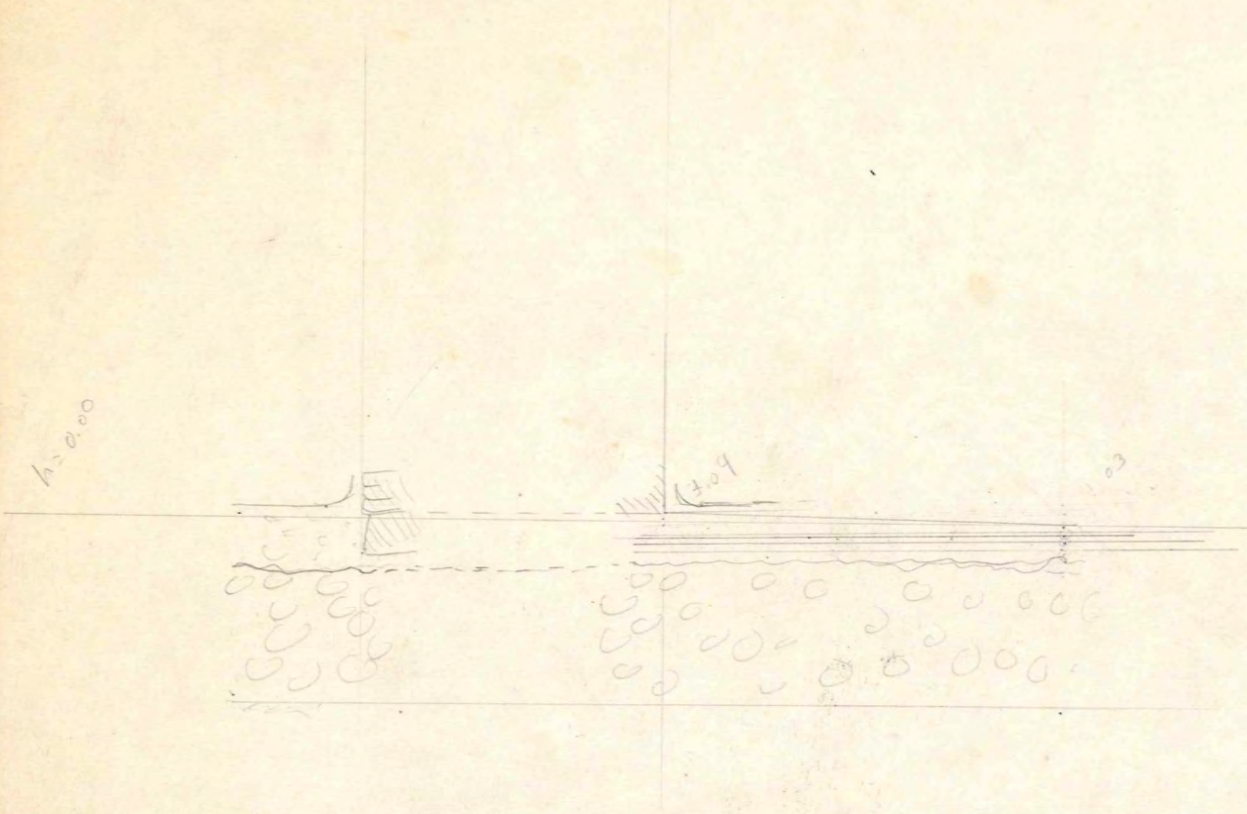
But P-7-2nd did not show this elevation.

(Continuing

S col
.05 = 1.50

P-7

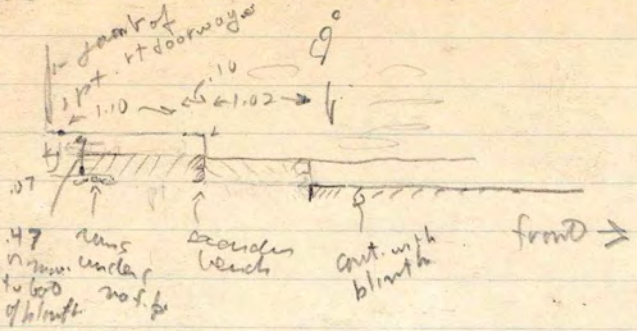
3-56


h=0.00
+0.9

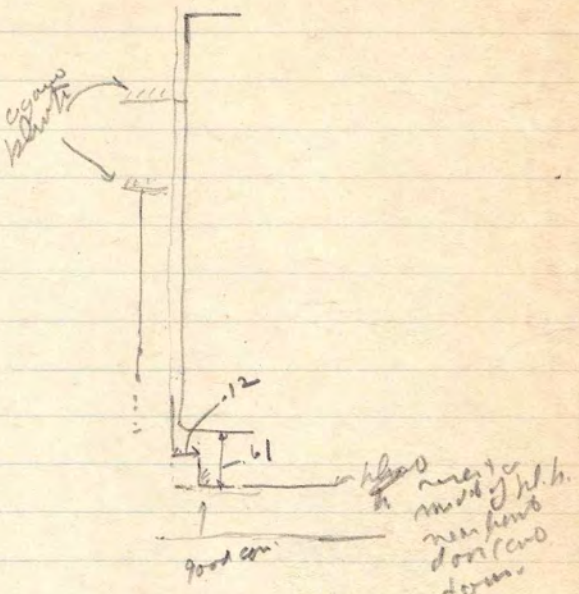
P.7 P.7 35-9

1935

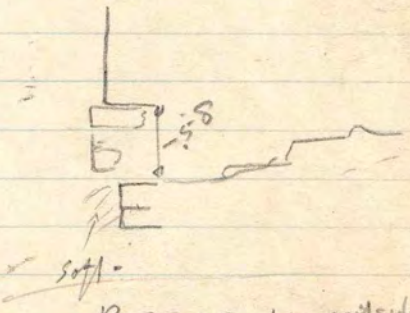
Right Facade — Section - Elevation



Right Facade. Stairway

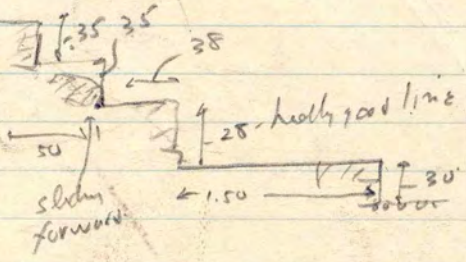


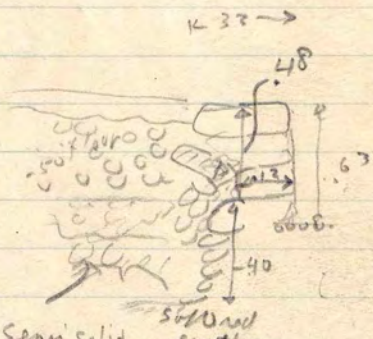
Could find no evidence that plinth bodates wall.



Passage, 1.60 outside.

Front Steps





Semi solid earth dark reddish ones and stones in soil, possibly wall as in V-1-3rd.

Fairly clear that -50 floor was broken for making passage through to a structure floor only.

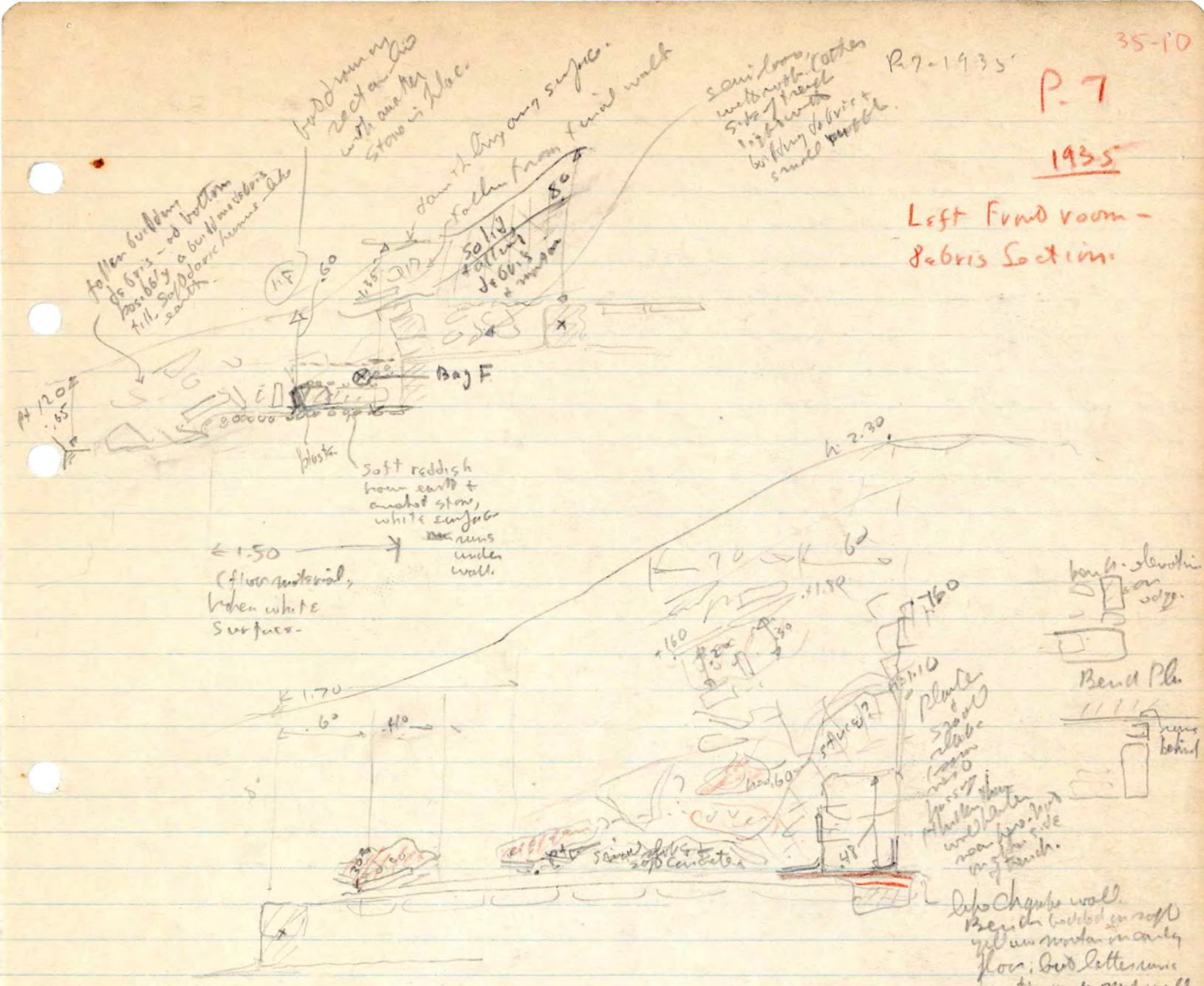
35-10

R7-1935

P. 7

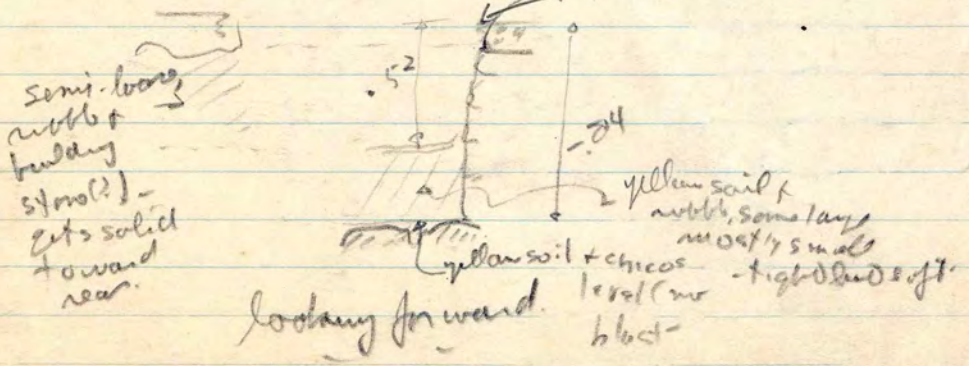
1935

Left Fund room – Debris Section



Other end of trench

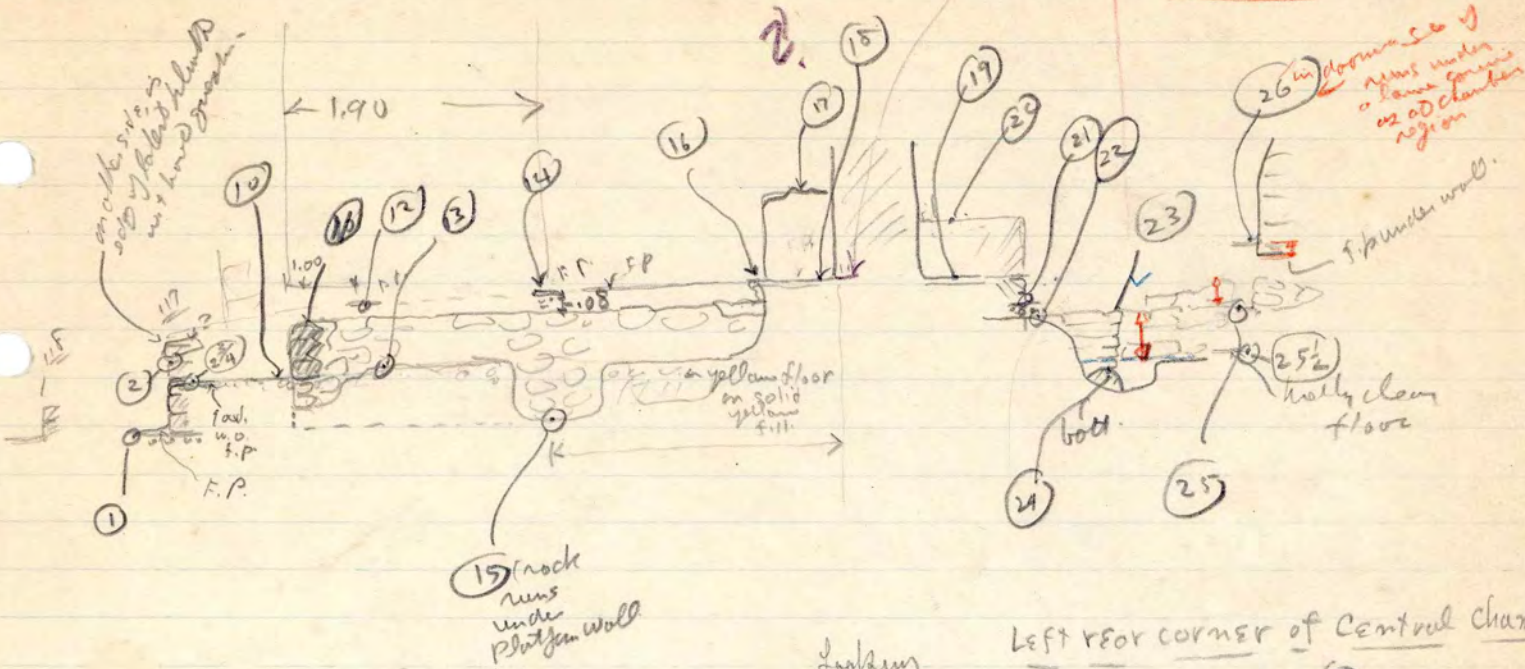
Roof concrete & small slabs entire length of cut, .30 × .40 deep. Fallen & semi-roofed section above. – no gravel in this mortar.



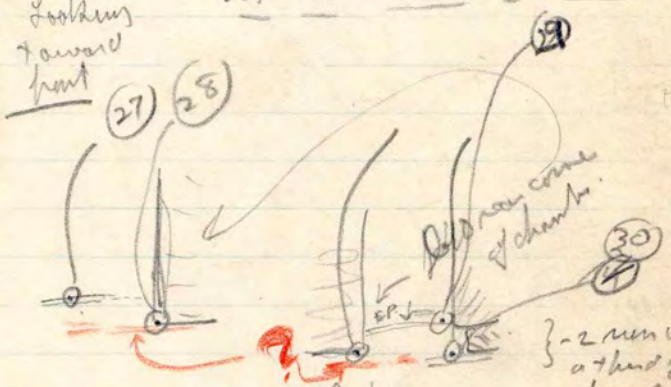
Mitchell Survey Camp - wing, none

R7

Platform &c. - 1935
Left Trench + rear room



Left rear corner of Central Chamber



hi' = +.43
Read down.
① - 1.50
② - .90
2⅔ - .65 (rock, for shaft)
2¾ - read 1.86, hi = 1.12 h = -.74

check
hi' = 1.12
② 1.59 h = -.47
① 2.19 h = 2.19 − 1.12 = 1.07

hi = dam .54 on +108 = +.54

hi = +.32
Read down.
⑩ .92
⑪ .52
⑫ .39
⑬ .92
⑭ .38
⑭ +.20
⑮ 1.20
⑯ .37
⑰
⑧ .40

hi = read 2.92 on Rt. 18 wlnch = 2.84

hi = 3.06

⑲ 2.62
⑳ 2.00
㉑ 2.81
㉒ 2.93
㉓ 2.88
㉔ 3.48
㉕½ 2.91
㉕½ 3.29
㉖ 2.44 (wall about .05 below centers, ends.

㉗ 2.50
㉘ 2.59
㉙ 2.40
㉚ 2.52
h = +.32

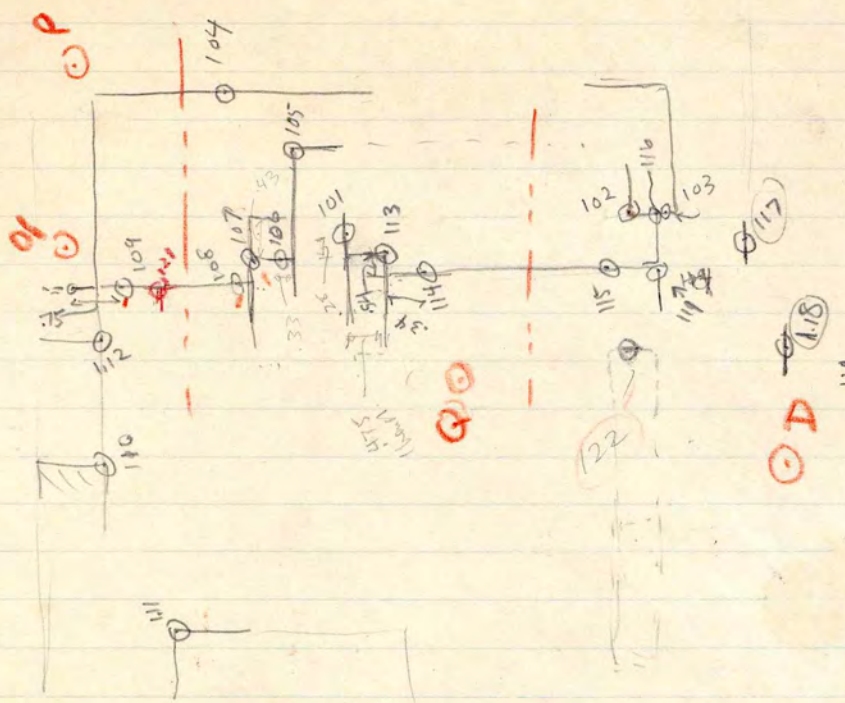
(bottom) check OK

Wall 117 below to latest period
only 20 top

Left Side Plan. Stairway.

P-7. P-7 3512

1935



(102) - 9.34 0; 9.35 P; 33.1 Q
3.65 (101). 5.52 D.

(103) 9.91 0; 9.91 P; 3.77 Q

(101) 5.67 0; 5.85 P; 2.26 Q

(104) 4.39 0; 3.77 P; ~~4.02 (111)~~

(105) 4.90 0; 4.65 P.

(106) 4.42 0; 4.68 P

(107) 3.63 0; 4.02 P

(108) 3.61 0; 4.39 P;
3.46 Q

(109) 1.73 0; 3.26 P;
5.46 Q

(110) 3. 30-0; 5.22 P; 3.87 Q

(111) 5.30 0; ~~3.57 (109)~~
5.07 Q.

(112) 4.22 - (104) 2.38 (108).

(113) .54 - (104) 3.23 (102);

(114) .62 - (113); 3.02 (102);

(115) 3.12 - (101); 1.23 (102);

(116) .21 (102) on line to (103).

(117) - 5.05 (101); 1.46 (102);
1.33 (119); 4.44 D

(118) 3.37 (102) 2.18 (117);
2.28 D;

(119) 4.02 (101); 1.13 (102);

(120) 4.98 (102); 1.82 (118).
2.01. D step falling over - house adjusted about right

(121) E is 7.42 from Q. ac

(122) 2.42 (102); 3.38 D (on side of house)

(123) 3.83 D ~~6.63~~ 7.60 B

(124) 4.61 D 6.64 B

~~(125) 8.83 D~~

h' = +.43 road for ③ +.65 ck, h' = 1.12 road 2.31

④ -1.88 Read 2.51 h' = 1.12 / 1.39

⑤ -2.00

⑥ 2.53

⑦ -2.60

⑧ 3.12

⑨ 3.47 check 4.13 1.12 3.01

Check

h' = road 1.85 1.12 .73

grade flatter (sandy) grass

118 112 120 118

5.10

.45

.52

1.25

1.70

3.15

1.88 / 1.65 / .23

2.00 / 1.88 / .12

2.53 / 2.00 / .53

2.60 / 2.53 / .07

3.12 / 2.60 / 52

3.47 / 3.12 / 35

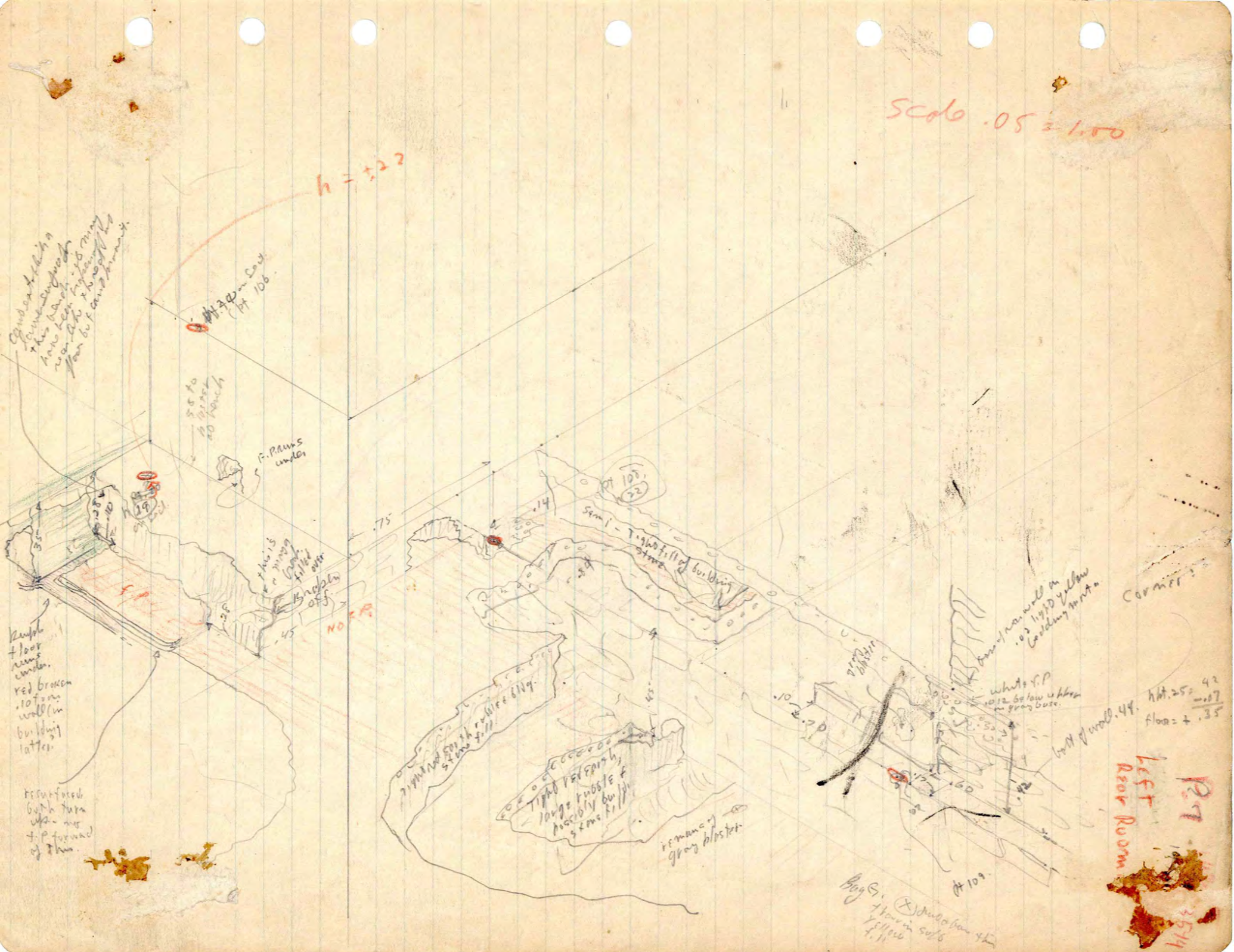
3.47 / 1.88 / 1.59

1.88 / 43 / 1.45

1.65 / 43 / 1.22

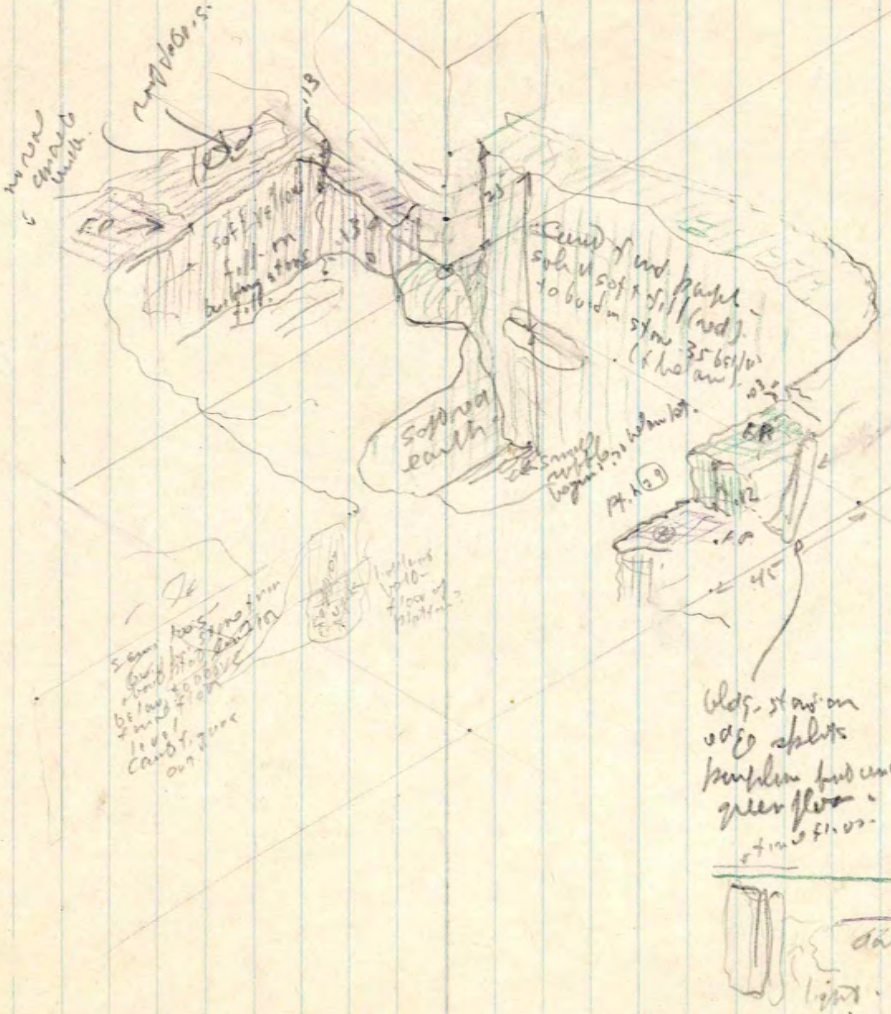
1.45

3.47 / 1.65 / 1.82 / 1.36 / 1.5 / 1.32

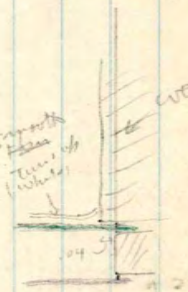

Scale .05 = 1.00
h = ±.22
Pt 106
F. Pans under
Pt 105
(22)
Semi-T. ware fr. (11th) bur. living
Pt 109
Pt 1
LEFT REAR ROOM
Corner
NO F.P.

R4 1937

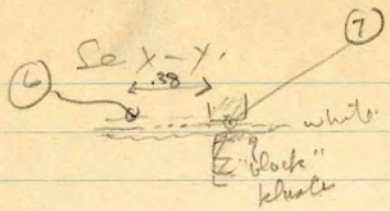
Floors and left rear corner of Central Chamber.

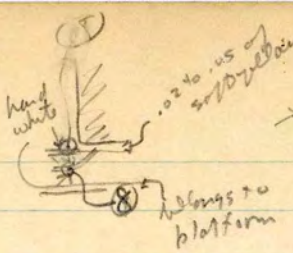


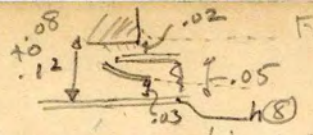
Sockets 4 mm bowl h 2.7



Proof of no stone in lumpier green floors







From →

35-16

R-7, 1935

Sec. mat. wall, right side, above zero from chamber

Plat., floors &c., outside.

h' = 1.12

(1)	1.36	h = -.24
(2)	1.25	h = -.13
(3)	1.35	h = -.23
(4)	1.08	h = +.04
(4½)	1.13	h = -.01
(5)	1.15	h = -.03
(6)	1.08	h = +.04
(7)	1.11	h = +.01
(8)	1.17	h = +.05

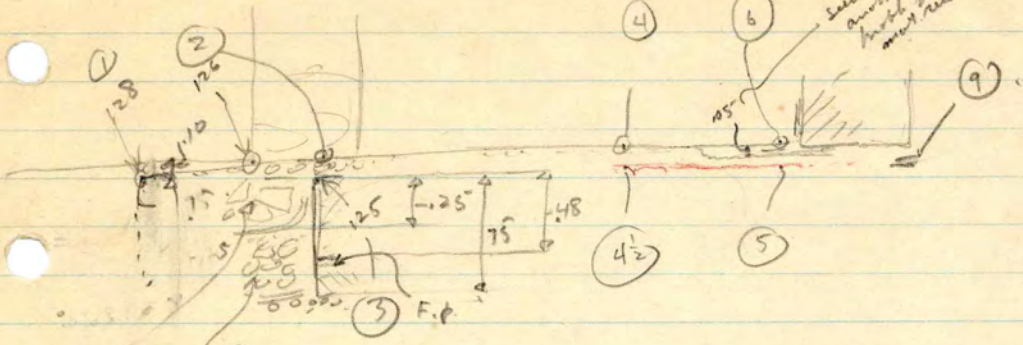
h' = 1.20

rows on stair: .83 (rise) / .37 = h of steps.

rise: 1.47 / 1.84 (2nd time for this h.

(9) 1.91 h = -.07

K .80 →

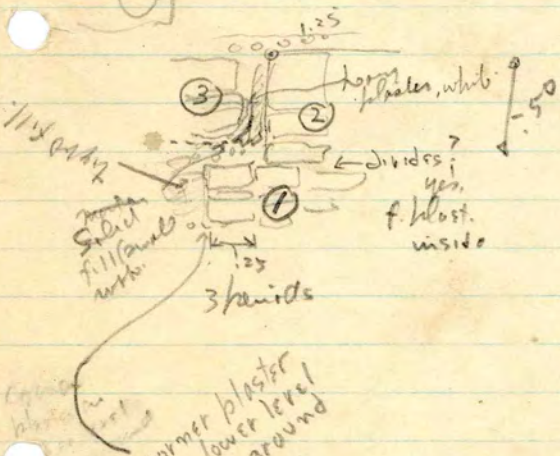


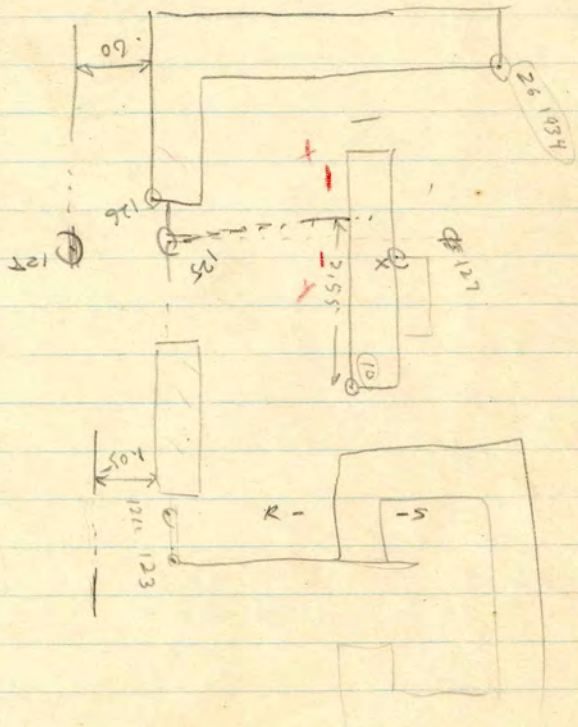
Semi figure, rubb.

Sec R.S.

building debris used as fill like near room under levels

chan.





(1.25) 8.83 D 3.12 B. 3.42 E

(1.26) 4.40 E 2.53 B

(1.27) 1.87 (26) 1.29 (X)

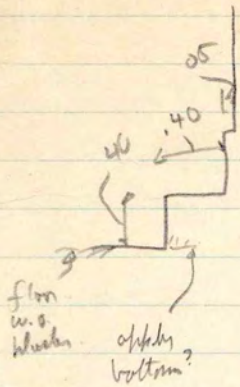
(1.28) 2.36 B; 1.86 (1.26) 3.28 E

plan data

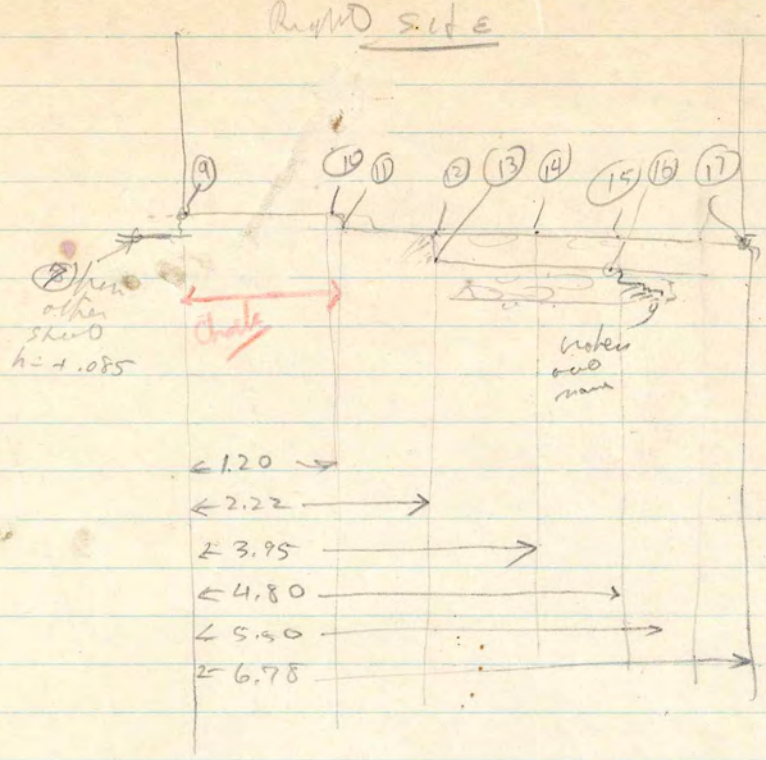
RZ-1935 P-7

Right Facade

1935



Right side



h= .085
1.42 road
= 1.505

(9) 1.20 = +30.5
(10) 1.26 = +.245
(11) 1.45 = +.055
(12) 1.48 = +.025
(13) 1.82 → 1.82 − 1.50 − .32 = −.315
(14) 1.64 = −.135
(15) 1.70 = −.195
(16) 2.05 → 2.050 − 1.505 = .545
(17) 1.90 = 1.900 − 1.505 = .395

150
120
30

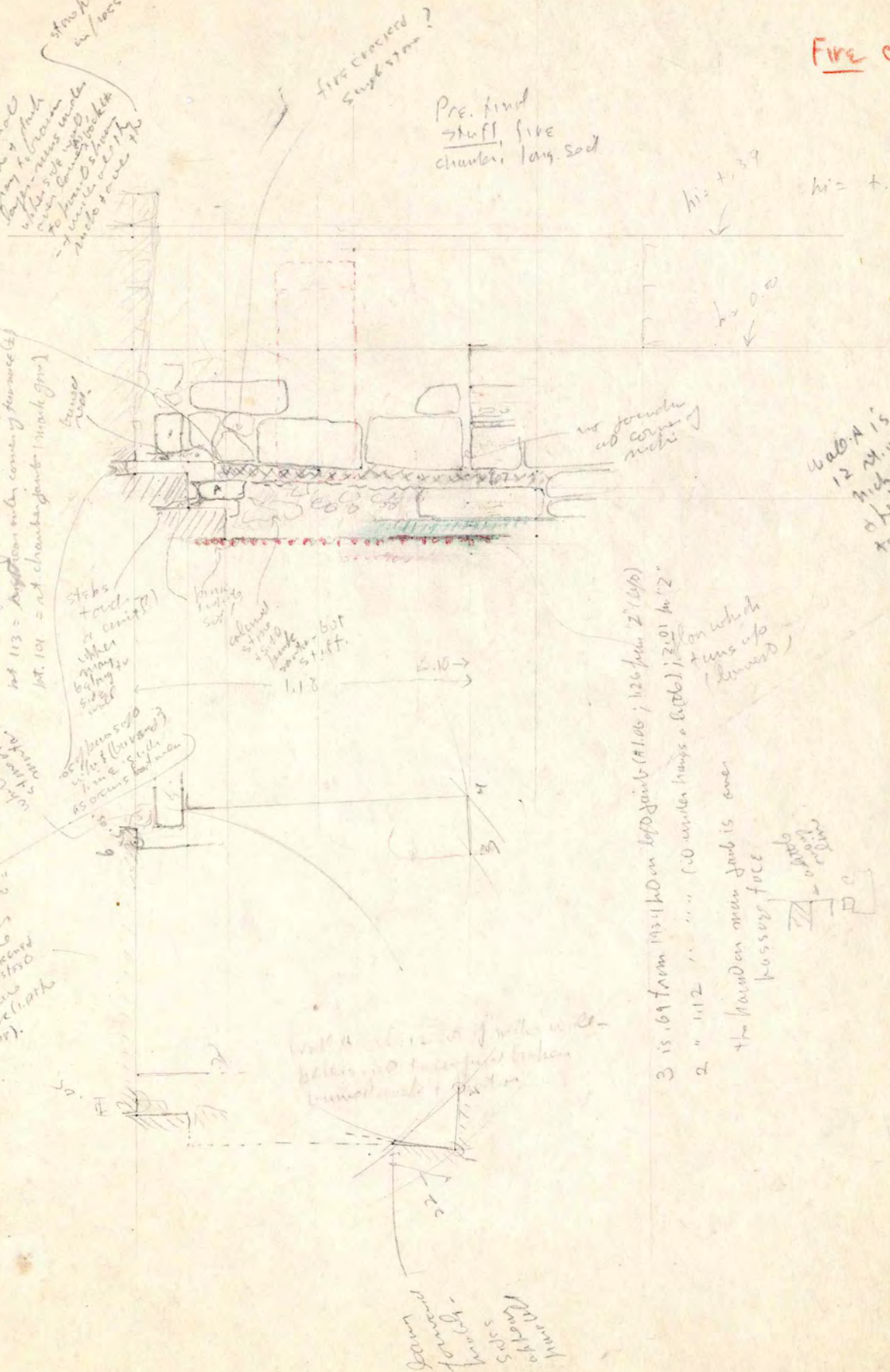
Scab mud
b .05 = 1.00

R7 35/18

R7
1935

(A)

Fire chamber



R7 55-19.
1935

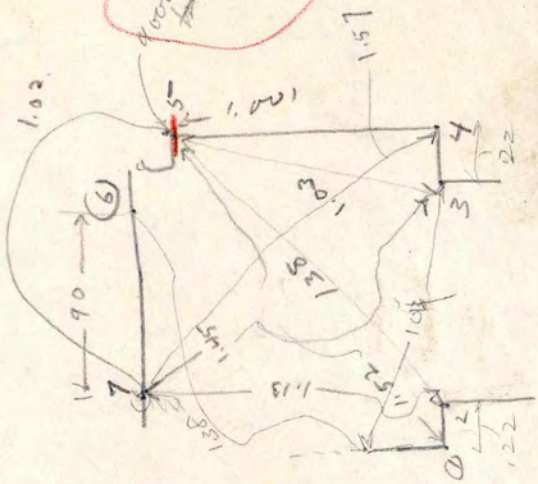
Fire Chamber

D-7

P+6 = .04 [illegible] of plinth from left hand corner of [illegible] furnace, & top.

6-4 = 1.17
6-3 1.18
6-2 1.47
6-1 1.54

Wood (thick) [illegible] to surface plaster when 12" min. behind side wall = [illegible] scaling (burned)



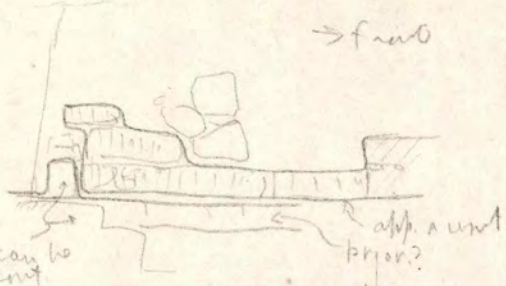
The shaded the tops of heavy wall of niche, hence the hook in all two white flues of corner of doorway is a rubble stone on top.

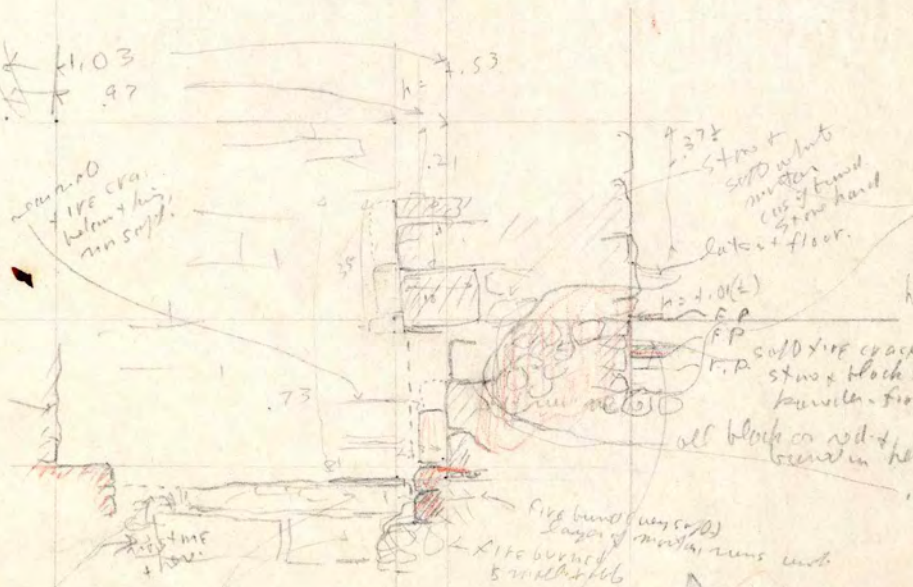
Even when the left wall of flues shows thick soft calcined mortar, that stone may be hand or calcined. Inside early "niche" wall [illegible] higher level is blackened inside

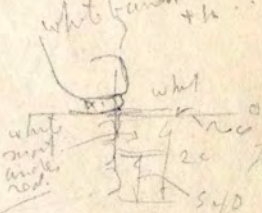
I.P early left wall probably meets with left furnace wall left of about zero, & the early floors.

Sec. 27 [illegible] of curve of top, 37 of bottom. Left near corner of left furnace. 1:2.

Left side of furnace.







Clean this all base chamber floors ended against rubble of left wall of furnace, below razed.

- where left side of wall here, a yard no stone of is block

Red "walls" [illegible] Left side soft. Middle probably 11 inch "brickwork"

Bank with burned over these

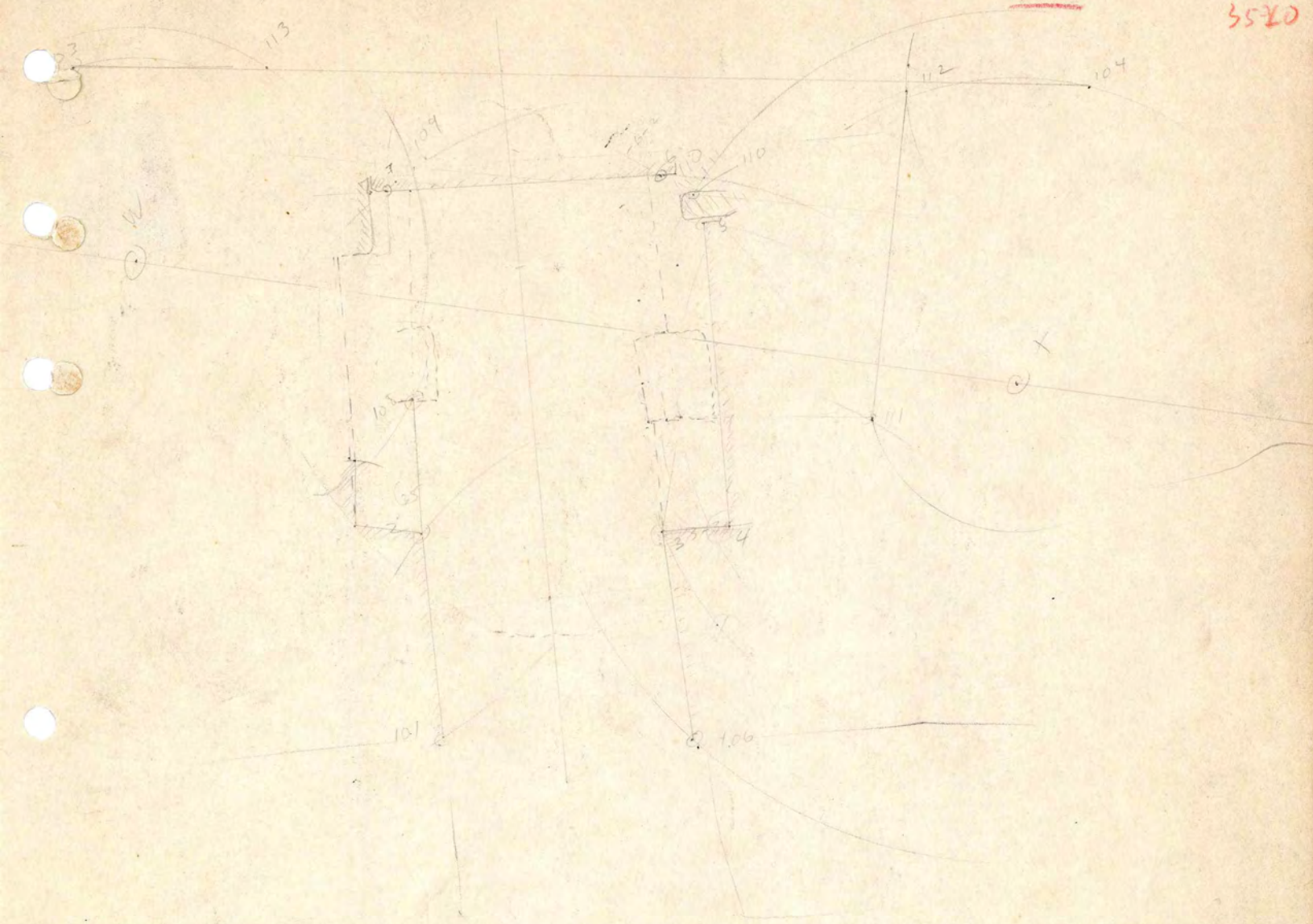
Sab 05 = 1.00

Sab + 1 step

(Scale Used 0.05 = 1.00)

S41 P-7 1935
Early Fire chamber
Plan

3570



.44
220
360
580

5565 L 1.13
55/15 44/69

PIEDRAS NEGRAS 1935 STR. P-7

CP. No. MUSEUM CAT.

SCALE SEE PHOTO Nos.

REMARKS 4531

P-7
1935

35-24

Central Chamber
Cross-Section

ashbin
arch stone
27 x 20 x 16
(hewn)

A2 run under
2 ft of stones
of old wall
of furnace.
The ashes here
had the lower
reduced to powder.
(hand stones of base
+ on both sides of it.

#1 duct above, and (f. p [illegible])
#3 and 3.45
2, ashpit.

1 C-P
4 .03
2 .05
3 f.p blocking spots
.10
white [illegible] f.p
120, f.p
rough surface of sandy subfloor
.01, hard white
.01 + dark brown sandstone
4 Secs, all pre-date sand of all heads shown of passage walls
f.p floor, bad shape. the first floor here
f.p found near stone (4)
See A.B
f.p
white
.015
white mortar strip
white mortar
.03

red floor. Below red. 35 from road
at 70 begins this rock
rocks
like I-7 - but a great deal of ashes
.03 mostly of gentle curve

Long Cross See inside chamber

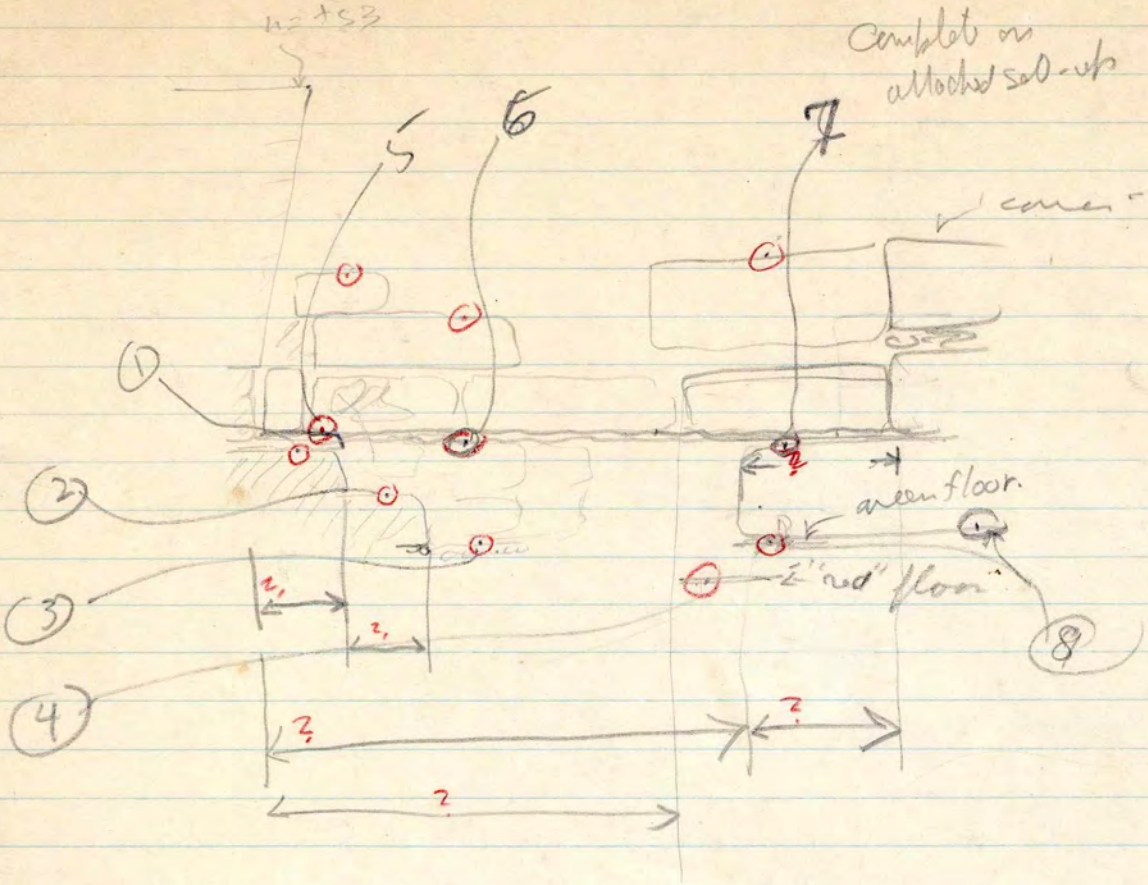
It is clear that floors 1 & 4
run possibly [illegible] and the white on
brickate the final old corner of
furnace. They are all too high to
go with such corner at present height.

1.27
.125
.08
.035
.030
cobble smooth (like on south bench steps of chamber)
reddish, black charcoal-ashy sand not so good as other side.
lower (see notes)
stone removed 1.0
2.05
.05
.01 x .20
.0015
.01
.03
.035
third wall
block
pier for [illegible] of chest
white, rough
new broken by Mayer's
3 great floor
off the chest wall
broke curb stone on new passage line
rock & drop .01 in .70
floors under the red f (wall) fail to reach passage wall & should it. This is very clear on left side.
(harder)
that rock & the cement white floor run under both sides
The white under both fronts.
rock holes inside - see note
both fail to reach passage wall:
the white meets & dies over passage walls on both sides.
The rock does not on left & probably did not on right. It's angle is. Below on step of the bench on left side.

Scale .05 = 1.00

P-7 55-22

1935



h' = +3.9

1	.83	83/39 h=-44
2	.95	95/39 h=-.56
3	1.06	106/39 h=-67
4	1.05	h=-.66
5	.79	79/39 h=-.40
6	.82	82/39 h=-43
7	.89	89/39 h=-.50
8.	.99	99/39 h=-60

Final check

Chamber. Complete Plant Sec of Furnace per sheet A.
- place it in chamber (includes leveling)
- sketch & locate wrinkle in rod floor.
- show which of burner is blocked by it.
- thermo. 05 below

Outside

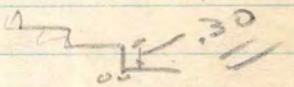
add to passage

- find bottom & level it.
- Cross cent find back

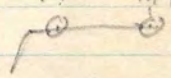
Any signs of leaves bench in ctr room?
None in same position (2 ea)

Look for floor under vaulting on roof.
- Level find any.

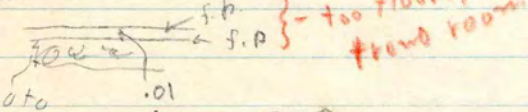
Meas h. of leaves stab. to plug.



Check levels on leaves terrace



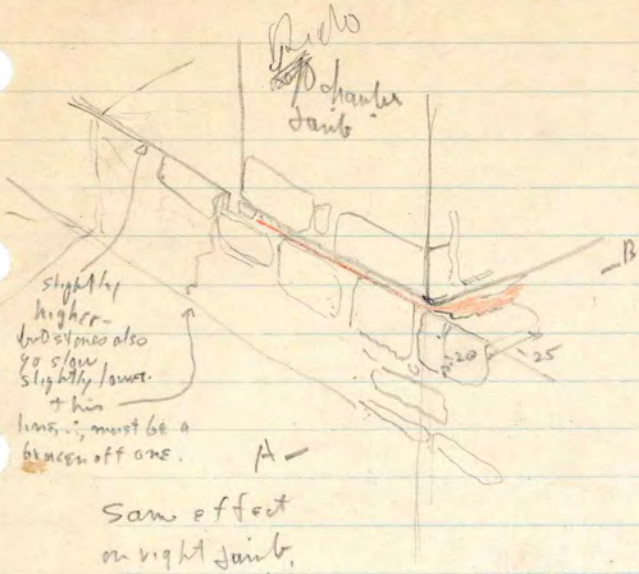
Outside - Pt 130 from chamber, at front room.



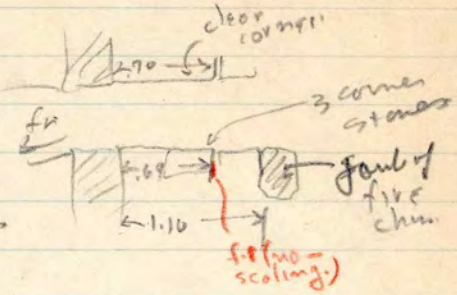
may be now - can't find them & this can now very difficult

P-7-1935 35-03

Passage + Central chamber wall.



Same effect on right jamb, clear to front

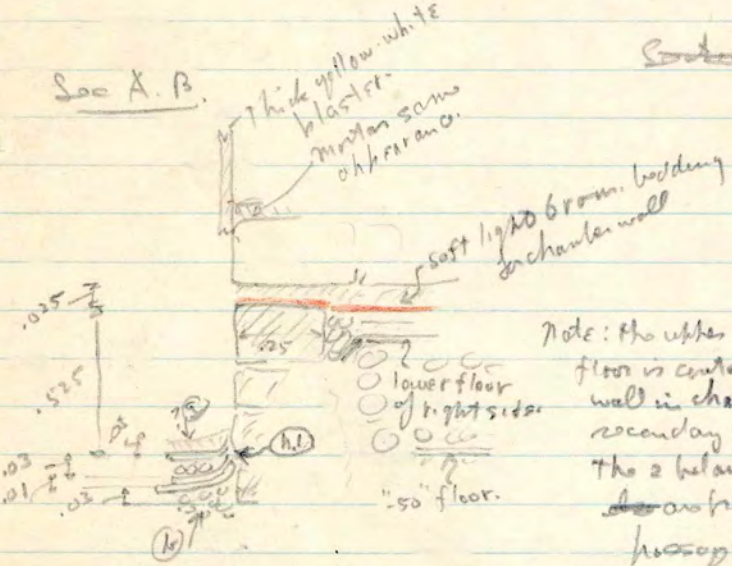


ref = rough surface plaster in place on passage wall inside, horrible in joints all the wall to front on left & within .10 on right jamb. dk under lies soft brown mortar which bedded the chamber wall

This is the highest sub-wall floor of right side, with thin (though not here) shows a secondary white finishing coat. This has (as everywhere) the dark blackish hard surface. under the white (if which shows) dk is white again in body. below the thin surface film of dark. Powdery latter was black hard, bnd possibly in areas dk occurs on the 2 surfaces below. There are below top of passage wall, and just fail to meet it. Apparently they were broken off. (?)

~~Section A-B~~

See A. B.



a = soft brown earth + crushed stone (light packed

b = dark brown to blackish crushed stone + soft earth (very loose

Floors are white; concrete above lowest is crushed stone + white lime

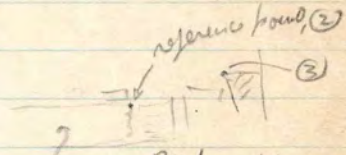
Note: the upper sub-chamber floor is contemp with passage wall in chamber (bottom of the secondary ~~white coat~~ coating. The 2 below preceded it and ~~the~~ are broken at edge, mean passage wall. all four run under chamber wall, the upper, ~~two~~, only, two over passage wall.

Periods here:

1. -50 floor
2. 3 } 2 lower floor surfaces.
3. 4 } 5 } - 2 upper floor surface, passage wall.
4. 5 }
6. - chamber wall.

h1 = +.51

① read 1.035
-.510
h = .575



Read 61
h = +.51

h② = +.10

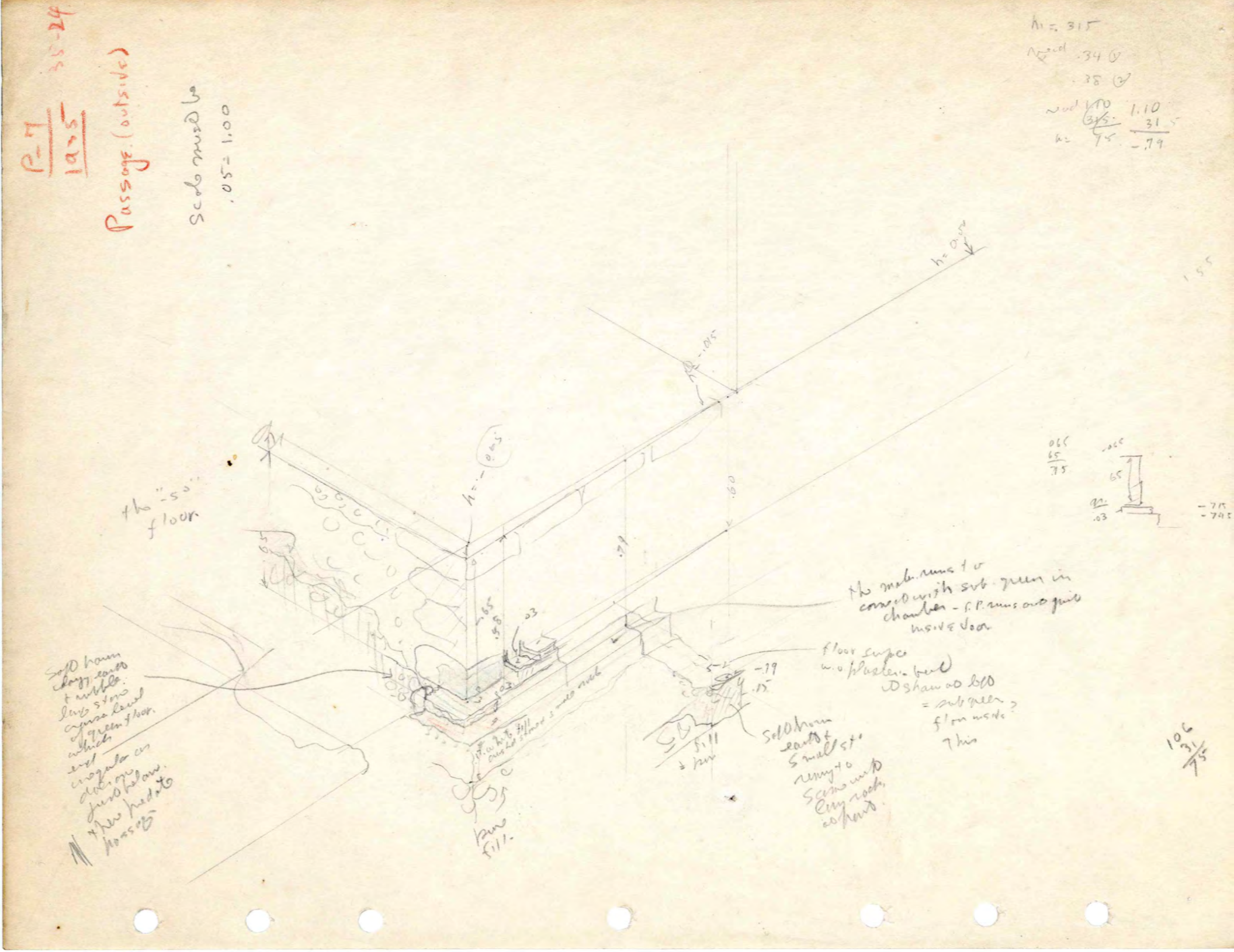
h1 +.51

3 = read .025 below bound.

51
.025
.535

= bottom mean hacked slab on rear passage wall of fire chamber.

IVB there is no escaping conclusion that there was a passage several hours preceding the present chamber, which used same passage.


P-7
19-5
Passage (outside)
Scale used
.05 = 1.00
the "-5" floor
h = -(0.5)
h = 0.5
.65
.55
.03
.60
.31
.15
-.19
Solid loam clayey earth + rubble. Lots stone coarse loam + gravel which crops on declivity just below + NW headto house
Pure fill
Solid loam earth + small st' running to same wall. Lay rock in front.
Floor surface w.o plaster-board
Shaw 00 bld = subsoil floor inside
This
the make runs to connect with sub-green in chamber - S.P. runs and gives inside door
106
31
75